ATTACHMENT B —BASIS OF DESIGN TAXIWAY L AND RUNWAY 4 – 22 SHOULDERS CONSTRUCTION AT ELLINGTON AIRPORT SOLICITATION NO.: HJA-TWYEFD-2022-011

ATTACHMENT B

TAXIWAY L AND RUNWAY 4 – 22 SHOULDERS CONSTRUCTION BASIS FOR DESIGN

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- I. Basis of Design Narrative
- II. Asphalt Shoulder Pavement Design Report
- III. Taxiway L Pavement Design Memorandum
- IV. 30% Drawings (prepared by HNTB)
- V. List of Construction Specifications

I. Basis of Design Narrative

Taxiway L and associated taxiways will follow the 30% Advanced Planning Drawings prepared by HNTB and attached below in Item IV. These drawings were included in the Taxiway L Draft Program Definition Document dated May 2021.

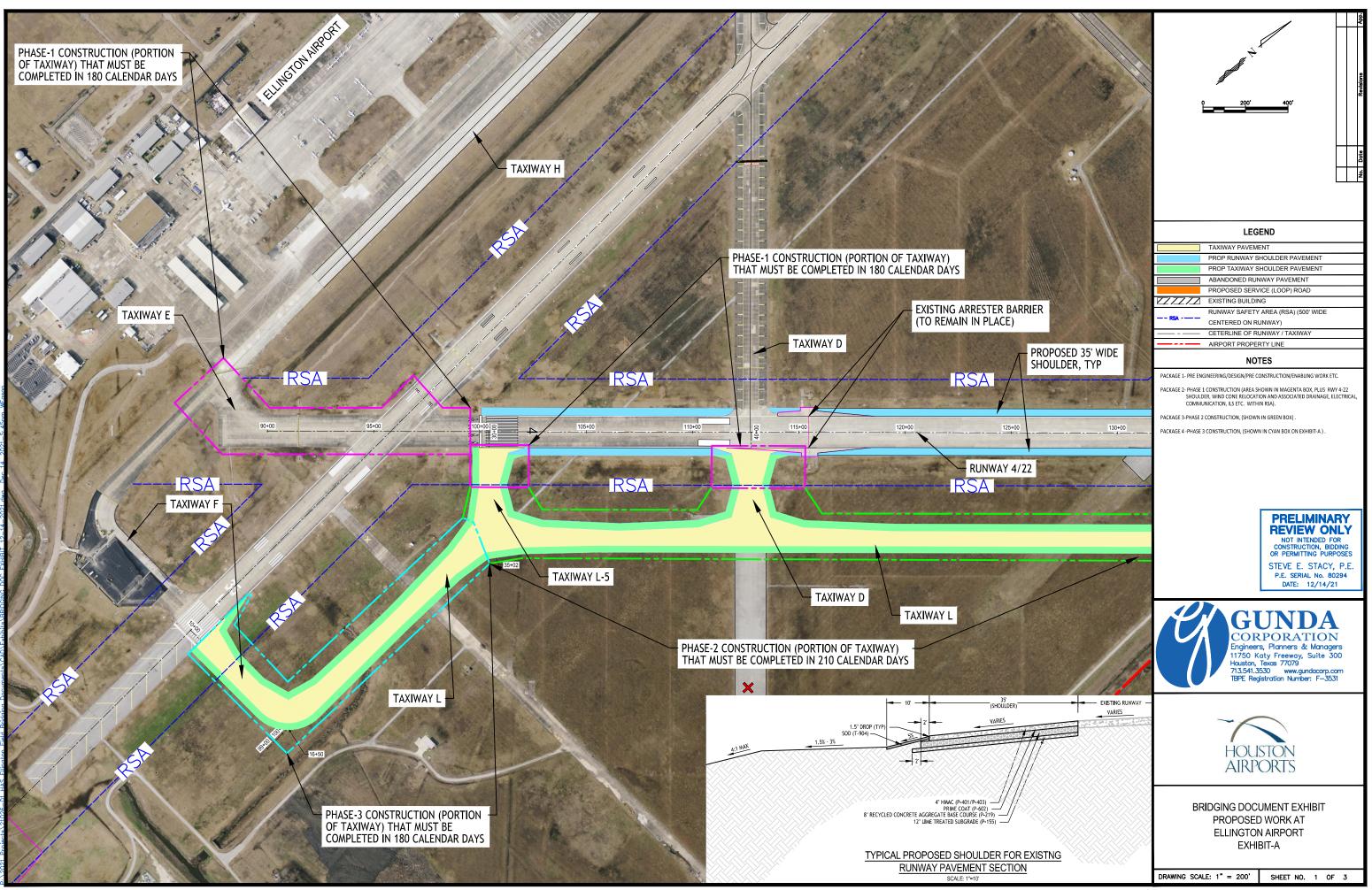
Runway 4-22 improvements will include adding 35 feet wide asphalt shoulders to each side of the runway. The Taxiway L Draft Program Definition Document recommended concrete shoulders. HAS decided asphalt shoulders would be acceptable. The addition of the asphalt shoulder will require the runway edge lights to be replaced and upgraded to LED fixtures to match the recommended fixtures for Taxiway L. Lighting upgrades also be done for the runway end indicator lights. All existing runway edge lights and boxes should be salvaged and delivered to a location determined by HAS. Runway shoulders and lighting upgrades were not part of the 30% Advanced Planning Drawings.

The wind cones for Runway 22, Runway 17R and Runway 35L must be moved outside the Runway Safety Areas. The locations of the relocated wind cones shall meet the requirements for Part 139. These items were noted to not be in compliance during the annual Part 139 inspection.

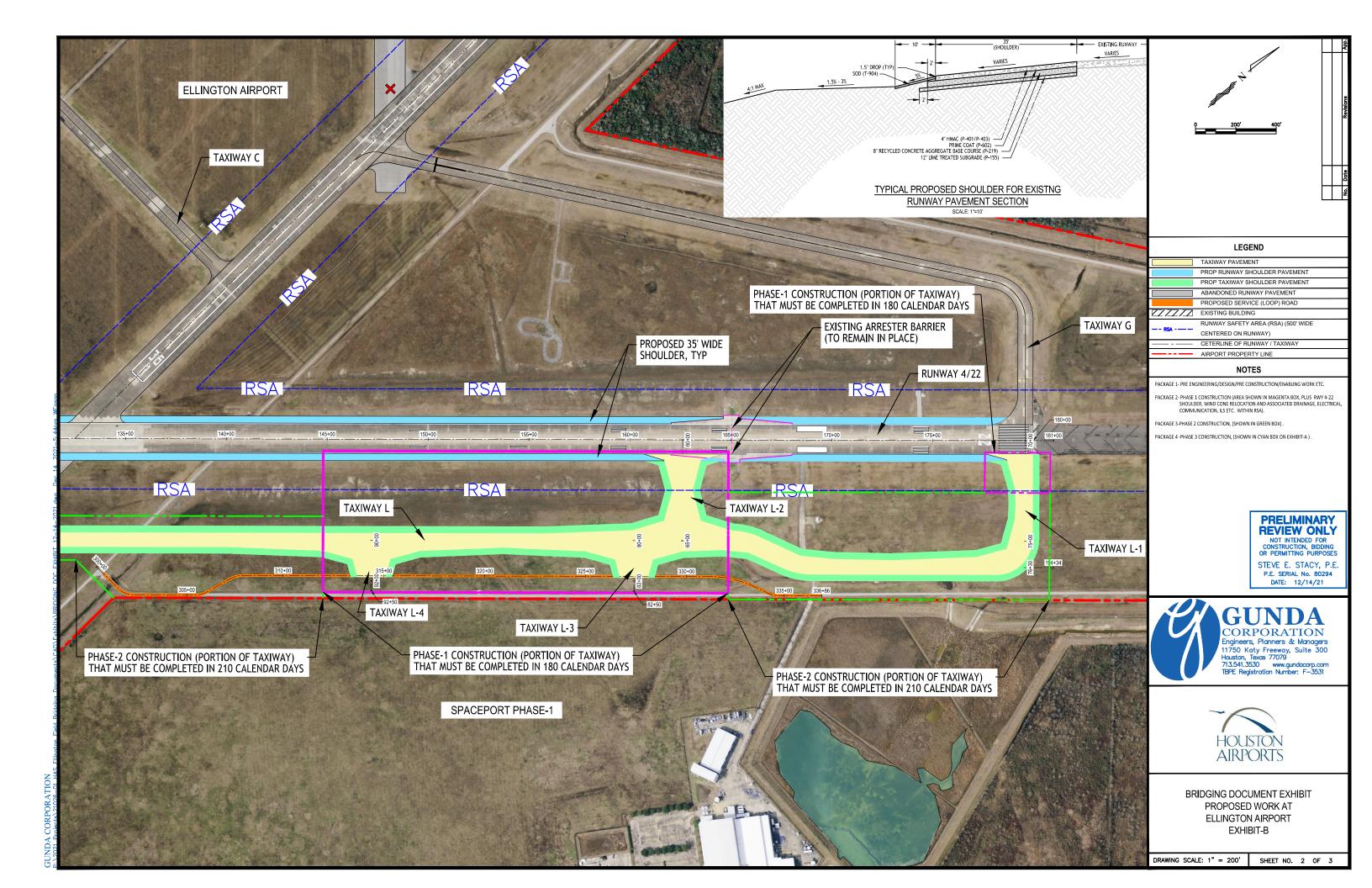
The recommended pavement section for the asphalt shoulder is shown in Section II of this document. Refer to Exhibits A and B for limits of the of the runway shoulders. Exhibits A and B also show the portion of Taxiway L and associated taxiways that must be completed in order to provide access to Spaceport tenants. All work within the RSA for Runway 4-22 must be completed in the same construction phase in order to provide access to Spaceport tenants.

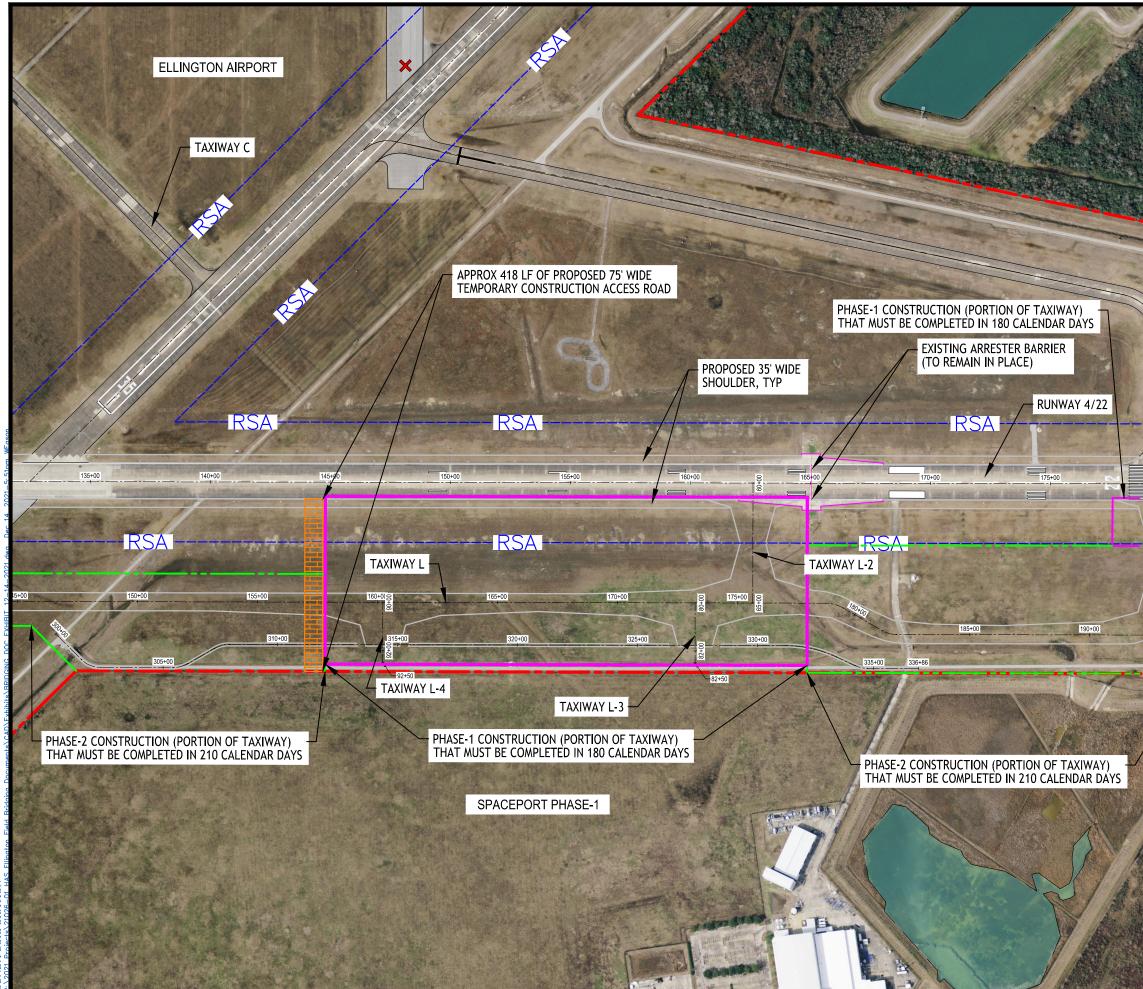
In order to provide access to Runway 4-22 and the portion of taxiways that need to be completed for Spaceport tenants, HAS wants to utilize a wooden/composite mat roadway as a temporary access to the airfield. The temporary roadway shall be 75 feet wide with a length of approximately 418 linear feet. Refer to Exhibit C for the location of the temporary roadway along with applicable notes. The actual location will be as approved by HAS.

The project may be divided into multiple phases/packages depending upon HAS business need and may be discussed during project design development phase.



GUNDA CORPORATION





	LEGEND
TAVINAN	RUNWAY SAFETY AREA (RSA) (500' WIDE CENTERED ON RUNWAY) CETERLINE OF RUNWAY / TAXIWAY AIRPORT PROPERTY LINE
TAXIWAY G	
	NOTES
menter and a second	 THE TEMPORARY CONSTRUCTION ACCESS ROAD SHALL BE COMPOSED OF WOODEN MATS OR OTHER ENGINEER APPROVED MATERIAL.
	2. THE ACCESS ROAD SHALL NOT BLOCK EXISTING STORM WATER DRAINAGE. TEMPORARY
-180+00	CULVERTS MAY BE REQUIRED. 3. THE ACCESS ROAD SHOULD BE ABLE TO WITHSTAND ALL EXPECTED LOADS FROM
82 181+00	CONSTRUCTION EQUIPMENT. 4. ONCE REMOVED, THE ACCESS ROAD AREA MUST BE RESTORED TO ORIGINAL EXISTING
	CONDITION.
A STATE OF THE STATE OF	 REMOVAL OF THE ACCESS ROAD SHALL BE "BACKED" OUT FROM THE RUNWAY TOWARDS THE NEW TAXIWAY.
A Real Trans	THE ACTUAL LOCATION OF THE ACCESS ROAD SHALL BE DETERMINED BY THE CONTRACTOR.
100-52 00-52 00-52 00-52	PRELIMINARY REVIEW ONLY NOT INTENDED FOR CONSTRUCTION, BIDDING OR PERMITTING PURPOSES STEVE E. STACY, P.E. P.E. SERIAL No. 80294 DATE: 12/14/21
	GUNDA CORPORATION Engineers, Planners & Managers 11750 Katy Freeway, Suite 300 Houston, Texas 77079 713.541.3530 www.gundacorp.com TBPE Registration Number: F-3531
	HOUSTON AIRPORTS
	BRIDGING DOCUMENT EXHIBIT PROPOSED WORK AT ELLINGTON AIRPORT EXHIBIT-C
	DRAWING SCALE: 1" = 200' SHEET NO. 3 OF 3

II. Asphalt Shoulder Pavement Design

Refer to next page.

PAVEMENT DESIGN REPORT HOUSTON AIRPORT SYSTEM ELLINGTON FIELD (EFD) RUNWAY 4-22 SHOULDER PAVEMENT DESIGN HOUSTON, TEXAS

SUBMITTED TO GUNDA CORPORATION 11750 KATY FREEWAY, SUITE 300 HOUSTON, TX 77079

BY HVJ ASSOCIATES, INC. 1701 DIRECTORS BLVD, STE. 910 AUSTIN, TX 78744

NOVEMBER 2, 2021

REPORT NO. HG 18 10259.1.1-P



1701 Directors Boulevard, Suite 910 Austin, Texas 78744 737-222-5151 www.hvj.com

November 2, 2021

Mr. Steve Stacy, P.E. Civil Engineering Manager GUNDA CORPORATION 11750 Katy Freeway, Suite 300 Houston, Texas 77079

Subject: Pavement Design Report Shoulder Pavement Design Houston Airport System – Ellington Field (EFD) Owner: Houston Airport System (HAS) – City of Houston, Texas HVJ Report No. HG1810259.1.1-P

Dear Mr. Stacy,

Submitted herein is shoulder pavement design report for the above-referenced project. The investigation was performed in accordance with HVJ's Subcontract with Gunda Corporation (GUNDA) for the On-Call Design Services for Small Projects at George Bush Intercontinental (IAH), William P. Hobby Airport (HOU) and Ellington Airport (EFD)- Contract No. 4600015601-Project No. 925G and is subject to limitations presented in this report.

It has been a pleasure to work for GUNDA on this project and we appreciate the opportunity to be of service. Please read the entire report and notify us if there are questions concerning this report or if we may be of further assistance.

Sincerely,

HVJ ASSOCIATES, INC. Texas Firm No. F-000646

R. F. Camichasta

Robert F. (Frank) Carmichael III, PE Senior Pavement Engineer

Anthony Gibson Graduate Civil Engineer

FC/AG

This document was released for the purpose of interim review under the authority of Robert F. (Frank) Carmichael III, PE 43815 on November 2, 2021. It is not to be used for construction, bidding, or permitting purposes.

The following lists the pages which complete this report:
Main Text - 7 pages
Appendix A - 3 page

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1. INTRODUCTION

HVJ Associates, Inc. was retained by Gunda Corporation (GUNDA) to prepare pavement design engineering as part of HVJ's Subcontract for the On-Call Design Services for Small Projects at George Bush Intercontinental (IAH), William P. Hobby Airport (HOU) and Ellington Airport (EFD)- Contract No. 4600015601-Project No. 925G. HVJ's scope of services is characterized by two main pavement design tasks:

1.1 Review Existing Geotechnical Investigation Report

HVJ is developing the pavement design for new 35 foot wide shoulders on both sides of existing runway Runway 4-22 at EFD. HVJ is using an existing geotechnical report which was completed by Aviles for Atkins on the parallel Taxiway L¹. This report has the necessary soil parameters needed for the proposed Runway 4-22 shoulder pavement design and was provided by GUNDA to HVJ. HVJ reviewed this report to establish the necessary subgrade design strength and stabilization requirements for the subgrade under the new shoulder design

1.2 Develop Runway 4-22 Shoulder Pavement Design

HVJ used the Aircraft Design Group V aircraft was provided by GUNDA and HAS for the pavement design. FAA Standard Construction Material Specifications were assumed by HVJ for establishing the properties of the new pavement materials. HVJ developed a 15-year hot mix asphalt concrete (HMAC) pavement cross section using the FAA FAARFIELD pavement design procedure. Two alternative base types will be considered (HMAC and CTB) with lime stabilized subgrade assumed to be required.

2. ANALYSIS AND DESIGN

2.1 Task 1 Review of Existing Geotechnical Report

The Taxiway L boring map provided in Appendix A (Plate A-2 of the Aviles report) shows the boring locations for taken for the parallel Taxiway L project. HVJ used the results from Borings B-51, B-53, B-56, B-58, B-60, B-63, and B-64, which were collected at the edge of Runway 4-22, where the connecting taxiways from Taxiway L intersect Runway 4-22. Based on a review of the recommend subgrade California Bearing Ratio (CBR) strength test values in Table 4-1 of the Aviles report, HVJ summarized the values shown in Table 1 below for this project.

Boring	CBR
B-51 5	
B-53	5.0
B-56	8.0
B-58	8.0
B-60	2.0

Table 1 Recommended CBRs Based on DCP results

¹ AVILES Engineering Corporation, "Geotechnical Investigation Report – Houston Airport System (HAS) Taxiway L at Ellington Field (EFD)," Report No G103-21, September 2021.

Boring	CBR	
B-63/CORE	5.0	
B-64	5.0	
AVERAGE	5.4	

The subgrade elastic modulus used for the shoulde pavement design was estimated to 8,100 psi based on the CBR of 5.4 and the following relationship of

$E = CBR \ge 1500$

Consideration of Swelling Soil. The soil types that were encountered in the Aviles borings along the taxiway alignments as summarized in Appendix A generally consist of fat/lean clay (CH/CL) with medium to very high plasticity. Subgrades with high plasticity indexes are capable of swelling beneath pavement structures, so treatment of the soil is necessary to mitigate any swelling effects. According to Section 2.16.12 of the 2015 Houston Airport System (HAS) Design Criteria Manual², all subgrades should be lime/fly ash-treated or cement/fly ash-treated. However, Aviles Engineering Corporation (AEC) recommends using lime stabilization to treat the subgrade. Based on the soil conditions, AEC suggests that a minimum of 8 inches of subgrade soils beneath the proposed pavement be stabilized with a minimum of 8 percent lime (by dry soil weight).

Sulfate content of the subgrade can present an adverse reaction with lime stabilization, so the sulfate levels of the soil were checked. The existing subgrade along the taxiway alignment had sulfate contents less than 3,000 ppm, so traditional treatment is acceptable.

PVR (Potential Vertical Rise) is a soil's potential to swell beyond its existing state if moisture is introduced. AEC selected 15 borings to determine PVR. The results are summarized Table 2.

Boring	PVR (in), based on in-situ
Doring	moisture conditions
B-1	4.03
B-6	1.55
B-11	4.72
B-17	3.03
B-22	2.90
B-26	2.12
B-33	3.21
B-37	2.23
B-41	1.64
B-47	3.46
B-50	3.44
B-56	2.11
B-64	3.26
B-67	2.22
B-74	2.81

Table 2 AEC's Potential Vertical Rise Results

² Houston Airport System (HAS) Design Manual, "Section 2.16.12.5 – Subbase and Base Course", April, 2015.

For reference, the TxDOT 2019 Pavement Design Manual³ requires a maximum allowable PVR of 2.0 inches for highway main lanes. Of the select borings in Table 2, the PVR exceeds 2 inches in 13 of the 15 borings. AEC states the following in their geotechnical report: "If HAS decides to reduce the PVR to at least 2 inches, the top 24 inches of highly expansive clay soils along the project alignment should be excavated and either replaced with lean clay soil with low plasticity, or by stabilizing the excavated clay soil with at least 8 percent hydrated lime and then compacting it back in place." The existing proposed pavement design provides 24 inches on nonswelling material and meets this requirement.

2.2 Task 2 Shoulder Pavement Design

HVJ prepared the hot mix asphalt concrete (HMAC) shoulder pavement thickness designs in accordance with the FAA AC 150/5320-6F Airfield Pavement Design and Evaluation and using the FAARFIELD computer software. The design procedure inputs include: insitu subgrade modulus, pavement materials' modulus values, aircraft mix, and number of departures.

New Pavement Material Strength Values. The Hot Mix Asphalt Concrete (HMAC) Item P-401 /P-403 surface design modulus was assigned to be 200,000 psi. The Recycled Concrete Aggregate Base Course (RCAB) Item P-219 base design modulus was assigned to be 75,000 psi.

Lime stabilized subgrade was selected as for all cross sections due to the high PI subgrade soil. Lime stabilized subgrade is not a listed option within the FAARFIELD software, so a "User Defined" layer was used and HVJ assumed a typical lime stabilized subgrade modulus of 30,000 psi. The Aviles report recommended 8% Lime in their report. HVJ also recommends that the contractor confirm a mix design that will achieve a minimum unconfined compressive strength of 150 psi. Finally based on the high PI of the insitu soils, HVJ recommends that the lime stabilization be to a minimum of 8 inches for the shoulder pavement.

A summary of the new pavement material strengths used in designs is shown in Table 3.

Pavement Material	Design Resilient Modulus, psi
Item P-401/P-403 Hot Mix Asphalt Concrete	200,000
Item P-219 Recycled Concrete Aggregate Base Course (RCAB)	75,000
Item P-155 Lime Treated Subgrade (LTS)	30,000

Table 3. New Pavement Material Design Strengths

Design Aircraft Selection. Based on the Aircraft Design Group (ADG) V established by HAS for this runway, the Boeing 777-300ER aircraft was selected by HVJ for the shoulder thickness design.

Runway 4-22 Shoulder Pavement Design. The FAA software FAARFIELD⁴ was used for the pavement thickness design. A hot mix asphalt concrete (HMAC) Item P-401 / P-403 surface was used assumed for the shoulders and the 15-year design life was modeled based on a single annual departure of a Boeing 777-300ER loading. The FAARFIELD models insitu subgrade based on the

³TxDOT Pavement Design Manual, Chapter 3, Section 2 –" Geotechnical Investigation for Pavement Structures", Subsection 2.3.2.2 – "Swell Potential", 2019.

modulus of the subgrade and assumes the layer to be elastic, homogeneous, and infinite in thickness. The recommended FAARFIELD pavement thickness design is summarized below in Table 4 and the software output is provided in Appendix B.

Table 4. Runway 4-22 Shoulder Pavement Design			
15 year Design Life			
4.0" HMAC (Item P-401/P-403)			
Prime Coat (Item P-602)			
8.0" Recycled Concrete Aggregate Base Course (Item P-219)			
12.0" Lime Treated Subgrade (Item P-155)			

3. PAVEMENT SPECIFICATIONS

The following FAA Standard Airport Construction Specifications from AC 150/5370-10F⁵ Standards for Specifying Construction of Airports are applicable and apply the construction materials assumed for these designs.

Item P-152 Excavation, Subgrade, and Embankment Item P-155 Lime-Treated Subgrade Item P-219 Recycled Concrete Aggregate Base Course Item P-401 Asphalt Mix Pavement Item P-602 Emulsified Asphalt Prime Coat

4. **DESIGN REVIEW**

HVJ Associates, Inc. should review the design and construction plans and specifications prior to release to make certain that the geotechnical recommendations and design criteria presented herein have been properly interpreted.

5. LIMITATIONS

The shoulder pavement design was prepared for the exclusive use of GUNDA for the proposed Runway 4-22 shoulder at Ellington Field (EFD) for the Houston Airport System (HAS). The analyses and recommendations contained in this report are based on data obtained from subsurface exploration and laboratory testing prepared by others and provided to HVJ by GUNDA. The subsurface conditions only represent the specific locations where samples were obtained, only at the time they were obtained, and only to the depths penetrated. Samples cannot be relied on to accurately reflect the strata variations that usually exist between sampling locations or on different sites. Should any subsurface conditions other than those described in the boring logs be encountered, HVJ Associates, Inc. should be immediately notified so that further investigation and supplemental recommendations can be provided.

⁴ FAA, "Airport Pavement Design and Evaluation", Advisory Circular No. 150/5320-6F – FAARFIELD Software, November 10, 2016.

⁵ FAA, "Standards for Specifying Construction of Airports", Advisory Circular No. 150/5370-10G, July 21, 2014.

III. Taxiway L Pavement Design Memorandum





Technical Memorandum

То:	Dev Pokhrel, PE		
From:	Edmond Woods, PE	Email:	Edmond.woods@atkinsglobal.com
Date:	29 October 2021	Phone:	
Ref:	EFD Taxiway L Construction	cc:	John.verburg@atkinsglobal.com

Subject: Preliminary Pavement Design

1. Introduction

This technical memorandum summarizes the preliminary pavement design for the construction of Taxiway L at Ellington Field Airport (EFD). An overview of the proposed geometry is shown in Figure 1-1.

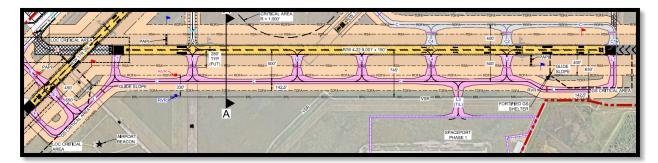


Figure 1-1 – Proposed Draft Geometry

2. Existing Conditions

In general, the proposed Taxiway L is proposed to be located to the east and parallel to existing Runway 4-22. The project area is primarily flat and covered with grass.



2.1. Document Review

TBD. At this time, no information has been provided regarding the area in which the proposed Taxiway L lies within or related to the existing, parallel Runway 4-22.

2.1.1. Taxiway L As-Built Drawings

Not applicable.

3. Geotechnical Investigation

Geotechnical information pertaining to the proposed EFD Taxiway L pavement design is available from the current geotechnical investigation for this project provided by Aviles. The Interim Geotechnical Report was provided on September 23, 2021.

The geotechnical investigation for this project was conducted during the period of 4 through 8 March 2021. The investigation consisted of drilling and sampling seventy-four (74) soil borings to a depth of 16 feet below the existing grade, performing thirty-seven (37) Dynamic Cone Penetrometer (DCP) tests along the proposed taxiways to estimate the field California Bearing Ratio (CBR) values, performing soil laboratory testing on selected soil samples to determine the index and strength properties of the subgrade soils, and performing solid laboratory testing on soil samples collected from sample pits to determine maximum dry density and moisture content of subgrade soils and subgrade CBR. At the time of this memo, the interim geotechnical report has been received which includes boring logs and initial laboratory testing. The interim geotechnical report is provided in Appendix A.

Fieldwork for this project's geotechnical investigation is complete and laboratory testing is ongoing. An interim geotechnical report has been issued to include boring logs and initial laboratory testing. Outstanding laboratory testing includes moisture-density relationship, soaked CBR, and soil-lime mix design series of the bulk samples. Boring locations are shown in Figure 3-1. This section will be updated, and the preliminary pavement designs will be reviewed upon receipt of the final geotechnical report.

Clay soils in the Greater Houston area typically have secondary features such as slickensides, calcareous/ferrous nodules, and contain sand/silt seams/lenses/layers/pockets. It should be noted that the information in the boring logs is based on 3-inch diameter soil samples which were generally obtained from the borings at intervals of 2 feet continuously from the ground surface to a depth of 16 feet below the existing grade. A detailed description of the soil secondary features may not have been obtained due to the small sample size and sampling interval between the samples.

The subgrade soils beneath the pavement that were encountered in the borings along the taxiway alignments generally consist of fat/lean clay (CH/CL) with medium to very high plasticity. For the construction of the taxiways, it is of the opinion that it will be sound engineering practice for the subgrade soils beneath the pavement to be stabilized to provide uniform and long-lasting subgrade support of the pavement, as well as provide a weather-resistant work platform during construction.





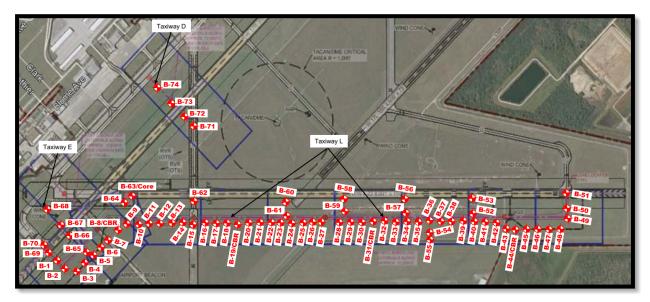


Figure 3-1 – Borings and Coring Location Plan

4. FAA Standard Design Criteria

4.1. Design Considerations

The FAA computer program, FAARFIELD, was used for all pavement thickness designs regardless of aircraft gross weight. FAARFIELD uses layered elastic and three-dimensional finite element-based design procedures for new and overlay designs of flexible and rigid pavements respectively. For rigid pavement design, FAARFIELD uses the horizontal stress at the bottom of the concrete panel as the predictor of the pavement structural life. The maximum horizontal stress for design is determined considering both edge and interior loading conditions. FAARFIELD provides the required thickness of the rigid pavement panel required to support a given aircraft traffic mix for the structural design life over a given base/subbase/subgrade.

4.2. Rigid Pavement Design

Rigid pavements for airports are composed of concrete placed on a granular or stabilized base course supported on a compacted subgrade. The FAARFIELD design process currently considers only one mode of failure for rigid pavement, bottom-up cracking of the concrete panel. Cracking is controlled by limiting the horizontal stress at the bottom of the concrete panel. Rigid pavement design is as referenced in Chapter 3 – Pavement Design, of AC 150/5320-6G.

The concrete surface provides a nonskid texture, minimizes the infiltration of surface water into the subgrade, and provides structural support for aircraft loading. The quality of the concrete, acceptance and control tests, methods of construction and handling, and quality of workmanship is covered in Item P-501Cement Concrete Pavement. See AC 150/5370-10, Item P-501 for concrete pavement specifications.



For pavement design, since the primary action and failure mode of concrete pavement is in flexure the critical strength of the concrete is the flexural strength. A design flexural strength between 600 and 750 psi (4.14 to 5.17 MPa) is recommended for most airfield applications. HAS requires the design flexural strength of 700 psi to be used in the design of airfield pavement.

4.3. Jointing of Concrete Pavement

Variations in temperature and moisture content can cause volume changes and warping of panels which may cause significant stresses. Joints are used to divide the pavement into a series of panels of predetermined dimensions to reduce the detrimental effects of these stresses and to minimize random cracking. Refer to Table 4-1 for recommended maximum joint spacing, according to AC 150/5320-6G, Section 3.16.13 – Joint Spacing. Note that the panel thickness controls the joint spacing, not vice-versa. Table 4-1 is not intended to be used to establish panel thickness based on a predetermined joint spacing. In general, smaller panels have better long-term performance. All joints should be sealed with appropriate joint sealant, using appropriate detail for sizing of joint. See AC 150/5370-10G for standard joint specifications, Item P-604 Compressive Joint Seals for Concrete Pavements, and Item P-605 Joint Sealants for Pavements.

Panel Thickness	Joint Spacing	
8-10 inches (203-254 mm)	12.5 feet (3.8 m)	
10.5-13 inches (267-330 mm)	15 feet (4.6 m)	
13.5-16 inches (343-406 mm)	17.5 feet (5.3 m)	
>16 inches (>406 mm)	20 feet (6.1 m) ^{2,3}	

Table 4-1 – Recommended Maximum Joint Spacing (Rigid Pavement)

4.3.1. Joint Type Categories and Details

Pavement joints are categorized according to the function that the joint is intended to perform. Joint types and their uses are as described in Table 4-2 and below. Pavement joint details are shown in Figure 4-1, Figure 4-2, and Figure 4-3, as referenced in AC 15/5320-6G. The categories of joints are:

- → Isolation.
- → Construction.
- → Contraction.





Туре	Description	Longitudinal	Transverse	
A	Thickened Edge Isolation Joint	Use at: -Pavement Intersections -Free edge that is location of future expansion -edge of structures	Use at: -pavement feature intersections when the pavement intersects atan angle. -free edge that is location of future expansion, -where pavement abuts a structure.	
A-1	Reinforced Isolation Joint	For concrete panels > 9 in (230 mm). Use at: -Pavement Intersections -Free edge that is location of future expansion - edge of structures	For concrete panels > 9 in (230 mm). Use at: -Pavement Intersections -Free edge that is location of future expansion - edge of structures	
В	Hinged Contraction Joint	Longitudinal contraction jointin panels < 9 in (230 mm) thick; longitudinal contraction joints located 20ft (6m) or less from the pavement free edge in panels < 9 in (230 mm) thick	Not used except for panels < 9" when using 'tension ring'	
С	Doweled Contraction Joint	For use in longitudinal contraction joints 20 ft (6 m) or less from free edge in panels > 9 in (230 mm) thick. Use at other locations with FAA approval, eg. at gate stands.	Use on the last three joints froma free edge, and for two or three joints on either side of isolation joints. Use at other locations with FAA approval, eg. at gate stands.	
D	Dummy Contraction Joint	For all other contraction jointsin pavement.	For all other contraction jointsin pavement.	
E	Doweled Construction Joint	All construction joints excluding isolation joints.	Use for construction joints at all locations separating successive paving operations ("headers").	
E1	Tied- Doweled Construction Joint	Construction joints on RW or TW in panels <9 in (230mm) thick (Replace every 3 rd dowel with tie bar)	N/A	
F	Butt Construction Joint	All construction joints for pavement serving aircraft less than 30,000 lbs (13,610 kg) on a stabilized base.	All construction joints for pavements serving aircraft less than 30,000 lbs (13,610 kg) on a stabilized base.	

Table 4-2 – Pavement Joint Types.





Isolation joints are needed:

- \rightarrow Where the pavement abuts a structure.
- ✤ To isolate intersecting pavements where differences in direction of movement of the pavement may occur (e.g., between a connecting taxiway and a runway).

Note: when connecting new pavement to existing pavement it may be necessary to extend the project back into the existing pavement to construct an isolation joint when the existing edge does not already include a Type A or A1 joint.

Type A joints are created by increasing the thickness of the pavement along the edge of the panel (see Figure 4-1). This thickened edge will accommodate the load that otherwise would be transferred with dowels or by aggregate interlock in contraction and construction joints. Type A-1 joints are reinforced to provide equivalent load carrying capacity as a thickened edge, but may only be used for concrete pavements greater than 9 inches (228 mm), that occur where pavement centerlines intersect at approximately 90 degrees. The joint between the runway and connector, crossover, and exit taxiways are locations where the Type A-1 joint may be considered. When intersecting pavements are at acute angles which results in small irregularly shaped panels on one side of the isolation joint, it may not be possible to install the reinforcement steel.





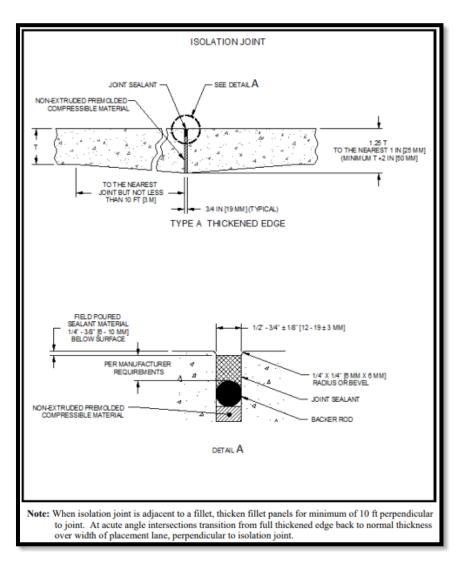


Figure 4-1 – Rigid Pavement Isolation Joint.

Construction joints are required when two abutting panels are placed at different times, such as at the end of a day's placement or between paving lanes. For pavements serving aircraft 30,000 pounds (13,610 kg) or greater, type E construction joints should be used. Type F butt joints may be used for pavements serving aircraft less than 30,000 pounds gross weight, constructed on a stabilized base or for a concrete overlay on a flexible pavement. Details for construction joints are shown in Figure 4-2.

Contraction joints provide controlled cracking of the pavement when the pavement contracts due to a decrease in moisture content or a temperature drop. Contraction joints also decrease stresses caused by panel warping and curling. Details for contraction joints are shown as Types B, C, and D in Figure 4-2. Details for joint sealant are shown in Figure 4-3.





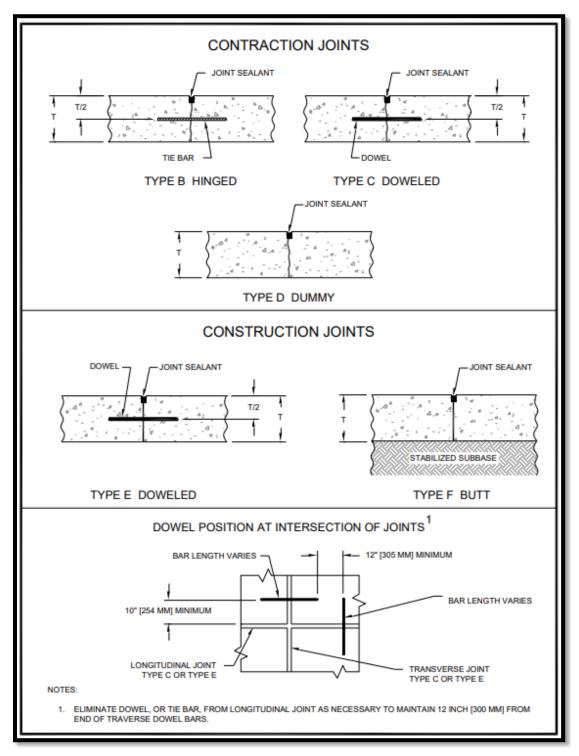


Figure 4-2 – Rigid Pavement Contraction and Construction Joints.





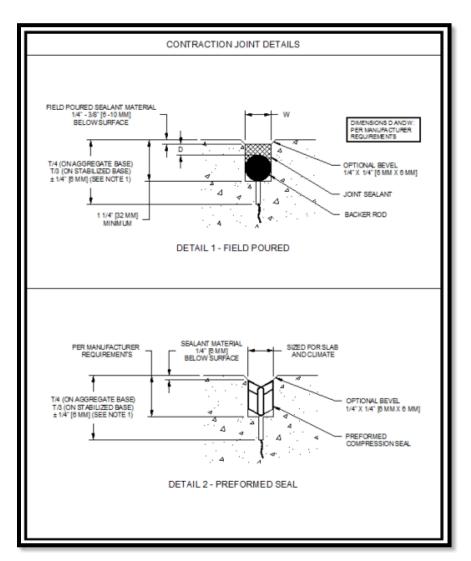


Figure 4-3 – Rigid Pavement Joint Sealant Details.

4.3.2. Dowels

Dowels provide load transfer across the joint and prevent relative vertical displacement of adjacent panel ends. Provide dowels in the last three transverse contraction joints from a free edge. Research indicates that when a stabilized base is included in the pavement section, the stabilized base will provide panel support assisting with load transfer. There is little benefit to providing more than a minimum of dowels in the last three joints from a free edge when the pavement section includes a stabilized base. Dowels are required in all construction joints regardless of if they are longitudinal or transverse, unless a thickened or reinforced edge is provided. Size dowels to resist the shearing and bending stresses produced by the loads on the pavement. Use dowel length and spacing sufficient to prevent failure of the concrete panel due to the bearing stresses exerted on the concrete. Table 4-3 gives dowel dimensions and spacing for various pavement thicknesses, as detailed in AC 150/5320-6G, Section 3.16.10.2.





Thickness of Panel	Diameter	Length	Spacing
5-7 in (125-178 mm)	3¼ in (20 mm)	18 in (460 mm)	12 in (305 mm)
7.5-12 in (191-305 mm)	1 in (25 mm)	18 in (460 mm)	12 in (305 mm)
12.5-16 in (318-406 mm)	1 ¼ in (30 mm)	20 in (510 mm)	15 in (380 mm)
16.5-20 in (419-508 mm)	1 ½ in (40 mm)	20 in (510 mm)	18 in (460 mm)
20.5-24 in (521-610 mm)	2 in (50 mm)	24 in (610 mm)	18 in (460 mm)

Table 4-3 – Dimensions and Spacing of Steel Dowels.

4.3.3. Transition Between Concrete and Asphalt

When rigid pavement abuts a flexible pavement section at a location that will be subjected to regular aircraft loading, provide a transition using a detail similar to Figure 4-4, as referenced in AC 150/8320-6G, Section 3.16.2 – Transition Between Concrete and Asphalt.

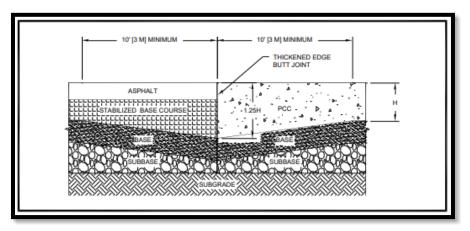


Figure 4-4 – Transition between Rigid and Flexible Pavement Sections.

4.4. Steel Reinforcement

Locations and sizes of reinforcement for crack control of irregularly shaped slabs shall be as detailed in FAA AC 150/5320-6G Section 3.16.12.2. Additional steel may be required at the Owner's direction.





5. Pavement Design

5.1. Traffic

Traffic used for design is derived from the airport's fleet mix provided in Appendix B. Sensitivity analyses were conducted for 1) the entire fleet mix, 2) only those aircraft contributing to the cumulative damage factor, and 3) only those aircraft with greater than 250 departures per year. No difference was noted between the first two options; however, removing aircraft with less than 250 departures per year reduces the P-501 thickness by one inch. Therefore, aircraft with less than 250 departures per year have an impact on the design and are included. The design life provided for FAARFIELD analysis and design was 20 years. The sensitivity analyses are included with the FAARFIELD reports in Appendix C.

5.2. Subgrade Support Conditions

According to Section 2.16.12 of the HAS Design Criteria Manual, all subgrades should be lime/fly ashtreated or cement/fly ash-treated. However, based on the cohesive soils encountered in the borings, it is the geotechnical engineer's opinion that using fly ash or cement will not be effective for subgrade stabilization along the taxiway alignments. It is recommended that lime stabilized subgrade be used alone for the construction of the taxiways. Based on the soil conditions, the geotechnical engineer suggests that a minimum of 12 inches of subgrade soils beneath the proposed pavement be stabilized with a minimum of 8 percent lime (by dry soil weight). Determination of the subgrade resilient modulus, E, the foundation modulus, k, and CBR is required for rigid pavement design. Based on the DCP test results, the interim geotechnical report recommends CBR values of 1 and 5 for the natural subgrade soils along the different alignments of the taxiways. The recommended CBR values were derived from and based on DCP test results are presented in Table 4-1.

Taxiway Alignment	Nearby Borings	Recommended CBR
Taxiway L/ Connector	B-1 through B-7	5
Taxiway L	B-8	20
Taxiway L	B-9 through B-29	7
Taxiway L	B-30 to B-32	20
Taxiway L	B-33 to B-39	3
Taxiway L	B-40	15
Taxiway L	B-41 to B-43	1
Taxiway L	B-44	9
Taxiway L	B-45 to B-47	2
Taxiway L/ Connectors	B-48 to B-51, B-52, B-53, B-63, B-64	5
Connector	B-54, B-55	20
Connectors	B-56 through B-59	8
Connector	B-60, B-61	2
Taxiway E	B-65 through B-68	5
Taxiway D	B-71 to B-74	8





The stabilized soils should be compacted to 95 percent of their ASTM D 1557 (Modified Proctor) dry density at a moisture content ranging from optimum to 3 percent above optimum. Lime stabilization shall be performed in accordance with Item P-155 of the FAA AC 150/5370-10G Airport Construction Standards.

The geotechnical firm estimated the Potential Vertical Rise (PVR) of soils within the proposed paved areas. However, it is the geotechnical engineer's experience with similar HAS projects that excavation of existing soil for PVR mitigation is not typically performed for taxiway projects. The geotechnical engineer should be notified if PVR mitigation is required so that our recommendations can be updated as necessary.

PVR is an estimate of the potential of an expansive soil to swell from its current state. Expansive clays exhibit a potential to shrink and swell with changes in their moisture contents. The changes in the soil moisture content are usually caused by variations in the seasonal amount of rainfall and evaporation rates or other localized factors like the moisture withdrawal by nearby trees. The geotechnical engineer determined PVR within the zone of seasonal moisture variation, which is typically considered to be 10 feet deep in the Greater Houston area.

Boring	PVR (in), based on in-situ moisture conditions	
B-1	4.03	
B-6	1.55	
B-11	4.72	
B-17	3.03	
B-22	2.90	
B-26	2.12	
B-33	3.21	
B-37	2.23	
B-41	1.64	
B-47	3.46	
B-50	3.44	
B-56	2.11	
B-64	3.26	
B-67	2.22	
B-74	2.81	

Table 5-2 – Estimated PVR

Based on Table 5-2, the PVR exceeds 2 inches in Borings B-1, B-11, B-17, B-22, B-26, B-33, B-37, B-47, B-50, B-56, B-64, B-67, and B-74. If HAS decides to reduce the PVR to at least 2 inches, the top 24 inches of highly expansive clay soils along the project alignments should be excavated and either replaced with lean clay soil with low plasticity or by stabilizing the excavated clay soil with at least 8 percent hydrated lime and then compacting it back in place. Compacted soil (whether embankment fill imported from offsite, or existing onsite soil stabilized with lime) should be placed in accordance with Section 3.4.1 (Ordinary Compaction) of Item 132 of the 2014 TxDOT Standard Specifications. Other



methods for reducing PVR, such as horizontal or vertical moisture barriers, geosynthetic reinforcement, subgrade drainage, etc. can also be considered if allowed by HAS. However, as noted above, it is the geotechnical engineer's opinion that the PVR mitigation strategies presented above would be costexcessive and ultimately unnecessary for this category of taxiway project. However, the decision to include PVR mitigation should ultimately be decided by HAS.

At the time of publication of this technical memo, the geotechnical firm was in the process of performing lime-stabilized soil testing to determine the CBRs for the stabilized base material. Per the FAA standards, this value must be greater than 35. The geotechnical firm stated that an updated final report or addendum letter will be provided once the lime-stabilized tests have concluded. Along with the updated final report or addendum letter, the geotechnical firm will provide the corrosion test results.

5.3. Thickness Design

Thickness designs were conducted in accordance with FAA AC 150/5320-6G using FAARFIELD v2.0.3. Outputs from FAARFIELD are provided in Appendix C. The design life used to calculate the Pavement thickness is 30 years, with a flexural strength of 700 psi.

5.3.1. Taxiway L

In order to account for the varying soil conditions presented in the Interim Geotechnical Report, a conservative approach with the soil conditions was taken. To mitigate any detrimental volume change and provide a working platform for construction, the existing infield soils will be lime treated. The lime percent will vary depending on the soil conditions in order to stabilize the first layer and bring it up to a uniform value. Due to the varying CBR calculations, the pavement design was developed using pavement designs with a CBR of 1 for the worst areas, and then a CBR of 5 for the areas with a higher CBR as shown in Table 4-1. Using the equations presented in Figure 4-1, the calculated k-value using a CBR of 1 is 23.53. The calculated E-value using a CBR of 1 is 1500. The calculated k-value using a CBR of 5 is 82.4. The calculated E-value using a CBR of 5 is 7500.

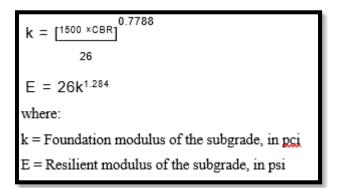


Figure 5-1 – Foundation modulus (k) and resilient modulus (E) of the subgrade soil according to FAA AC 150/5360-6E.

According to the Houston Airport System Design Manual, Section 2.16.12.5 – Subbase and Base Course, all full-strength pavements shall include a nine (9) inch Cement Treated Base course as a minimum. A new lift of Cement Treated Base (CTB) shall be installed full width of the pavement. This will provide





uniform support to the overlying cement concrete pavement (CCP). The preliminary typical pavement section options are shown in Figure 4-2 through Figure 5-9, as well as located in Appendix D.

Two pavement options were developed for the worst-case soil conditions and the best-case soil conditions, according to the geotechnical report. The worst-case soil conditions have a CBR of 1. The best-case soil conditions have a CBR of 5. Option 1 with a design using CBR of 1 consists of 17.5 inches of P-501 CCP, 6 inches of P-307 Cement-Treated Permeable Base Course (Drainage layer), 12 inches of P-304 CTB, and 12 inches of P-155 lime-treated subgrade (LTS). Option 1 with a design using CBR of 5 consists of 14 inches of P-501 CCP, 6 inches of P-307 Cement-Treated Permeable Base (Drainage layer), 12 inches of P-304 CTB, and 12 inches of P-155 lime-treated subgrade (LTS). Option 2 with a design using CBR of 1 consists of 17 inches of P-501 CCP, 6 inches of P-307 Cement-Treated Permeable Base (Drainage layer), 12 inches of 17 inches of P-501 CCP, 6 inches of P-307 Cement-Treated Permeable Base (Drainage layer), 12 inches of 17 inches of P-501 CCP, 6 inches of P-307 Cement-Treated Permeable Base (Drainage layer), 16 inches of P-304 CTB, and 12 inches of P-307 Cement-Treated Permeable (LTS). Option 2 with a design using CBR of 5 consists of 12.5 inches of P-501 CCP, 6 inches of P-307 Cement-Treated Subgrade (LTS). Option 2 with a design using CBR of 5 consists of 12.5 inches of P-304 CTB, and 12 inches of P-307 Cement-Treated Subgrade (LTS). Option 2 with a design using CBR of 5 consists of 12.5 inches of P-304 CTB, and 12 inches of P-307 Cement-Treated Permeable Base Course (Drainage layer), 16 inches of P-304 CTB, and 12 inches of P-304 CTB, and 12 inches of P-307 Cement-Treated Permeable Base Course (Drainage layer), 16 inches of P-304 CTB, and 12 inches of P-307 Cement-Treated Permeable Base Course (Drainage layer), 16 inches of P-304 CTB, and 12 inches of P-307 Cement-Treated Subgrade (LTS).

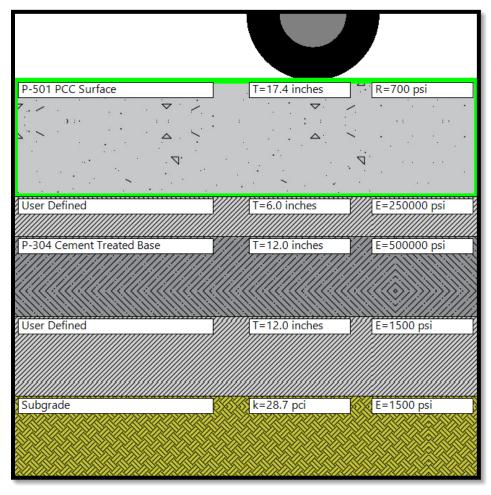


Figure 5-2 – Taxiway Pavement FAARFIELD Output – Option 1 – CBR = 1.





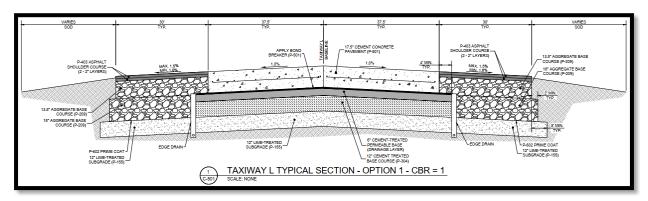


Figure 5-3 – Typical Taxiway and Paved Shoulder Section – Option 1 – CBR = 1.

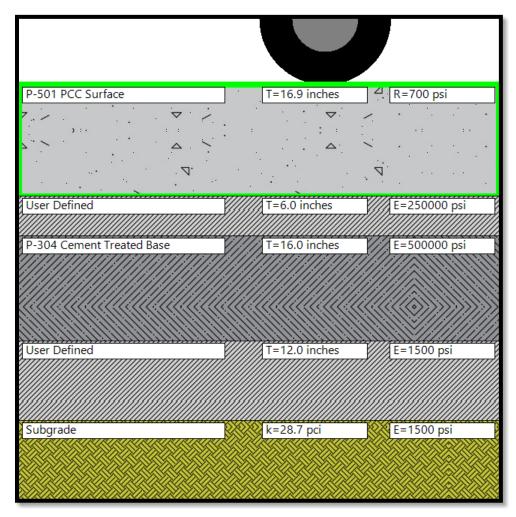


Figure 5-4 – Taxiway Pavement FAARFIELD Output – Option 2 – CBR = 1.





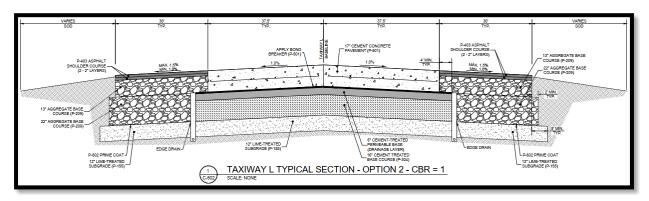


Figure 5-5 – Typical Taxiway and Paved Shoulder Section – Option 2 – CBR = 1.

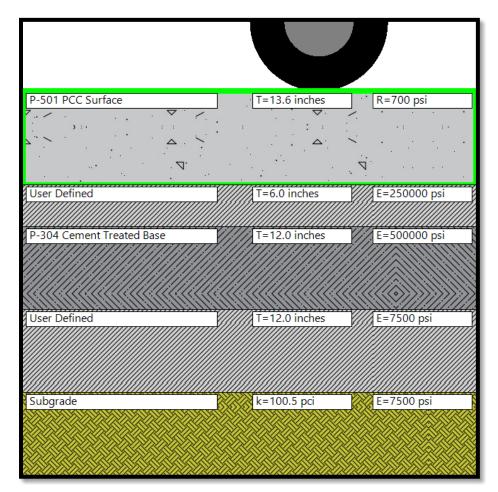


Figure 5-6 – Taxiway Pavement FAARFIELD Output – Option 1 – CBR = 5.





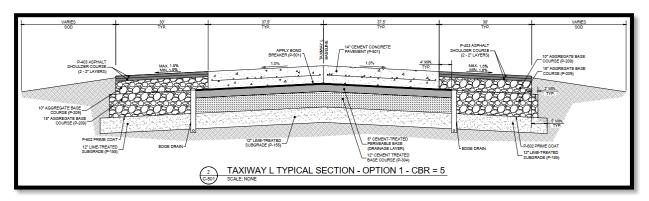


Figure 5-7 – Typical Taxiway and Paved Shoulder Section – Option 1 – CBR = 5.

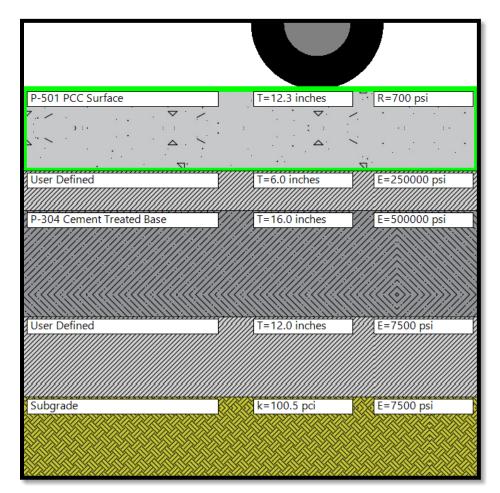


Figure 5-8 – Taxiway Pavement FAARFIELD Output – Option 2 – CBR = 5.





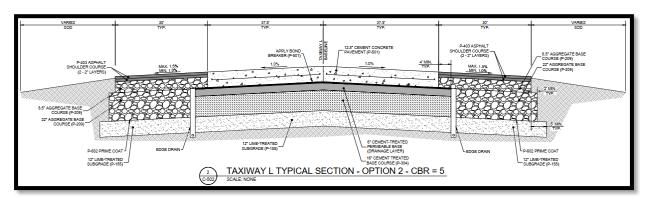


Figure 5-9 – Typical Taxiway and Paved Shoulder Section – Option 2 – CBR = 5.

5.3.2. Paved Shoulder

Similar to the full-strength taxiway pavement, the paved shoulder is constructed on existing infield soils. The proposed shoulder will also utilize a lime-treated subgrade to provide a working platform. The proposed shoulder typical pavement section consists of 4 inches of P-403 Hot Mix Asphalt (HMA), 31.5 inches of P-209 aggregate base course, and 12 inches of Lime Treated Subgrade (LTS).

6. Materials and Construction Recommendations

6.1. Pavement Specifications

6.1.1. P-155 Lime-Treated Subgrade

The lime-treated subgrade is used to provide a working platform not susceptible to weather impacts and to mitigate the high shrink-swell potential of the in-situ soils. Lime slurry is recommended in lieu of dry lime due to the proximity to open taxiways and the apron. Project-specific edits to the specification will be made upon receipt of the soil-lime test results from the bulk samples obtained during the geotechnical investigation. The lime percent will vary depending on the soil conditions. The stabilized soils should be compacted to 95 percent of their ASTM D 1557 (Modified Proctor) dry density at a moisture content ranging from optimum to 3 percent above optimum. Lime stabilization shall be performed in accordance with Item P-155 of the FAA AC 150/5370-10G Airport Construction Standards.

6.1.2. P-209 Crushed Aggregate Base Course

This item consists of a base course composed of a crushed aggregate base constructed on a prepared course. Another alternative to P-209 is the use of P-219, Recycled Aggregate Base Course. This alternative will allow the airport to use material that may already be stockpiled on-site, thus, reducing the cost of this base course overall. This may also be a candidate for a bid alternative.

6.1.3. P-304 Cement-Treated Aggregate Base Course

The cement-treated aggregate base course (CTB) is used as a stabilized base under the taxiway concrete pavement. The mix design will be developed by the contractor and will require a minimum compressive





strength of 300 psi at 7 days. Considering reflective cracking can be a concern with P-304 the following measures are taken to mitigate this risk:

- → Compact on the dry side of optimum moisture content and to 100 percent maximum density.
- → Provide an upper limit on 7-day compressive strength of 500 psi.
- → Under asphalt pavement, microcrack the CTB after minimum 24 hours of curing. Under the concrete pavement, apply a double application of curing compound prior to concrete paving.

6.1.4. P-403 Asphalt Mix Pavement

The paved shoulder will be constructed with two 2-inch lifts of P-403. Based on the lift thickness, gradation 2 is recommended. The base asphalt grade for Harris County is PG 64-16 per TxDOT. PG 64-22 is recommended for use as it is more commonly available and will provide additional resistance to low-temperature cracking. Specifying 50 gyrations is recommended to provide a greater asphalt content and, therefore, more durability against environmental distresses such as oxidation.

6.1.5. P-501 Cement Concrete Pavement

Concrete pavement will be provided in accordance with P-501. The minimum flexural strength to be used for acceptance during construction is 650 psi at 28 days. However, during production flexural strength averages are about 5 percent, or more, greater than the minimum specified. Therefore, the flexural strength used for design is 680 psi at 28 days. Use of combined well-graded gradations in accordance with the workability chart guidelines and a 1.5-inch nominal maximum aggregate size is recommended. The 1.5-inch nominal maximum aggregate size is achieved by specifying a concrete mixture using ASTM C33 No. 4 and No. 67, or a No. 467, coarse aggregate. Concrete using these types of gradations is less prone to spalling as compared to previous mixes which were generally high in sand content. As a bond breaker, Fabric shall meet the requirements of AASHTO M 288 Class I woven fabric with elongation less than 50% at the specified strengths. A certificate of compliance (COC) shall be provided by the fabric manufacturer that the material may be used as a bond breaker, or a liquid membrane-forming compound shall be in accordance with paragraph 501-2.7 of FAA Specification P-501, Cement Concrete Pavement. The Engineer will determine the type of bond breaker that is required, and as required at the Owner's direction.

6.1.6. P-307 Cement Treated Permeable Base Course (Drainage Layer)

A stabilized drainage layer should be placed immediately beneath the concrete panel in place of the stabilized base. Drainage layers are recommended for pavements serving aircraft greater than 60,000 pounds, constructed in areas with excessive subsurface moisture and where existing soils have a coefficient of permeability less than 20 ft/day (6 m/day). The use of drainage layers will protect pavements from moisture-related subgrade, subbase, and base failures. Drainage layers facilitate the quick removal of excess moisture from the pavement structure. Construct drainage layers to be free draining, include outlets to ensure that water is not trapped in the layer. Include a geosynthetic separation material when the drainage layer is placed directly above the subgrade. Regularly perform maintenance of drainage outlets to ensure that they are functioning, and that water is not trapped in the drainage layer. The modulus value assigned to the drainage layer for the cement-treated permeable base is 250,000 psi.









Appendix A – Geotechnical Report

EFD Taxiway L - Preliminary Pavement Design Memo



GEOTECHNICAL INVESTIGATION

HOUSTON AIRPORT SYSTEM TAXIWAY L GEOTECHNICAL INVESTIGATION AT ELLINGTON AIRPORT (EFD) HOUSTON, TEXAS

Reported to

Atkins North America, Inc. Houston, Texas

by

Aviles Engineering Corporation 5790 Windfern Houston, Texas 77041 713-895-7645

REPORT NO. G103-21

October 2021



October 22, 2021

Mr. John Verburg, P.E. Sr. Technical Manager, Aviation Atkins North America, Inc. 200 Westlake Park Blvd, Suite 1100 Houston, TX 77079

Reference: Geotechnical Investigation Houston Airport System Taxiway L Geotechnical Investigation At Ellington Airport (EFD) Houston, Texas AEC Report No. G103-21

Dear Mr. Verburg,

Aviles Engineering Corporation (AEC) is pleased to present this report of the results of our geotechnical investigation for the above referenced project. This investigation was authorized by Mr. Benedikt Goebel, Division Manager of Atkins North America, Inc. (Atkins) on March 8, 2021, via Task Order No.6 of Subcontract No. 1008665. Project terms and conditions were in accordance with the Master Subcontract Agreement between Atkins and AEC, dated June 24, 2019. The project scope of services is in accordance with AEC Proposal No. G2020-12-12, dated December 30, 2020.

AEC appreciates the opportunity to be of service to you. Please call us if you have any questions or comments concerning this report or when we can be of further assistance.

Respectfully submitted, *Aviles Engineering Corporation* (TBPELS Firm Registration No. F-42)

Wilber L. Wang, P.E. Senior Engineer

10/22/2021

Md. Rakib Hasan, Ph.D., EIT Staff Engineer

Reports Submitted: 1

1 Atkins North America, Inc. (electronic)

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GEOTECHNICAL INVESTIGATION

HOUSTON AIRPORT SYSTEM TAXIWAY L GEOTECHNICAL INVESTIGATION AT ELLINGTON AIRPORT (EFD) HOUSTON, TEXAS

1.0 INTRODUCTION

1.1 Project Description

The report submitted herein presents the results of Aviles Engineering Corporation's (AEC) geotechnical investigation as part of the preliminary engineering services for the Houston Airport System's (HAS) proposed Taxiway L at Ellington Airport (IATA Airport Code: EFD) in Houston, Texas (Houston/Harris County Key Map 577U, V, Y & Z, 578S, and 617C). A vicinity map is presented on Plate A-1, in Appendix A.

According to information provided by Atkins North America, Inc. (Atkins), the project consists of design and construction of (i) an approximately 10,000 feet long Taxiway L parallel to Runway 4-22, (ii) Taxiways E and D with approximately 1,200 feet length each, and (iii) additional connector taxiways.

1.2 Purpose and Scope

The purpose of this geotechnical investigation is to evaluate the subsurface soil and groundwater conditions along the proposed taxiways, and to develop geotechnical engineering recommendations for design and construction of the taxiways. The scope of this geotechnical investigation is summarized below:

- 1. Drilling and sampling seventy-four (74) soil borings to a depth of 16 feet below existing grade.
- 2. Perform thirty-seven (37) Dynamic Cone Penetrometer (DCP) tests along the proposed taxiways to estimate field California Bearing Ratio (CBR) values.
- 3. Performing soil laboratory testing on selected soil samples to determine the index and strength properties of the subgrade soils.
- 4. Soil laboratory testing on soil samples collected from four (4) sample pits to determine maximum dry density and moisture content of subgrade soils and subgrade CBR.
- 5. Engineering analyses and recommendations for subgrade preparation of the proposed taxiways.

2.0 <u>SUBSURFACE EXPLORATION</u>

Subsurface conditions at the site were investigated by drilling seventy-four soil borings to a depth of 16 feet below existing grade. The total drilling footage was 1,184 feet. Boring locations were marked in the field by



Landtech, Inc. The boring locations were surveyed as they were marked. Boring survey data (in State Plane Grid Coordinates, Texas South Central Zone, US Survey Feet) is presented on the representative boring logs and is also summarized on Table 1. The boring locations are presented on the Boring Location Plan on Plate A-2, in Appendix A.

Boring No.	Northing (Grid, ft)	Easting (Grid, ft)	Boring Surface Elevation (ft)	
B-1	13783415.92	3187660.15	23.74	
B-2	13783422.56	3187859.09	22.68	
B-3	13783566.78	3188038.56	22.35	
B-4	13783767.15	3188032.25	22.64	
B-5	13783960.47	3188025.19	17.12	
B-6	13784137.34	3188019.81	24.15	
B-7	13784336.88	3188011.52	24.86	
B-8	13784585.23	3188001.57	23.67	
B-9	13784766.46	3188046.14	23.64	
B-10	13784911.62	3188178.70	23.85	
B-11	13785057.8	3188312.01	23.51	
B-12	13785200.94	3188442.08	24.02	
B-13	13785353.95	3188580.17	23.97	
B-14	13785502.17	3188713.71	24.50	
B-15	13785649.47	3188846.78	26.53	
B-16	13785797.47	3188978.40	25.42	
B-17	13785943.43	3189107.23	26.76	
B-18	13786090.78	3189237.78	27.16	
B-19	13786238.83	3189368.77	27.62	
B-20	13786382.46	3189495.76	27.49	
B-21	13786530.17	3189626.79	27.49	
B-22	13786676.7	3189756.41	27.61	
B-23	13786826.68	3189888.87	28.40	
B-24	13786974.37	3190019.68	27.73	
B-25	13787123.06	3190150.63	27.80	
B-26	13787273.58	3190283.37	27.76	

Table 1. Boring Survey Data



Boring	Northing	Easting	Boring Surface
No.	(Grid, ft)	(Grid, ft)	Elevation (ft)
B-27	13787345.15	3190347.65	28.98
B-28	13787613.52	3190587.56	25.94
B-29	13787763.75	3190722.18	26.82
B-30	13787912.42	3190855.46	28.36
B-31	13788062.33	3190990.08	28.64
B-32	13788214.86	3191126.90	28.58
B-33	13788359.82	3191256.90	28.56
B-34	13788508.18	3191389.97	28.52
B-35	13788656.52	3191523.83	28.58
B-36	13788805.19	3191657.43	28.03
B-37	13788954.42	3191791.89	28.03
B-38	13789103.1	3191927.79	28.23
B-39	13789250.49	3192064.15	27.96
B-40	13789396.53	3192199.30	27.42
B-41	13789546.63	3192338.75	25.39
B-42	13789691.68	3192474.48	26.34
B-43	13789743.19	3192701.02	25.75
B-44	13789860.64	3192800.73	24.91
B-45	13790012.28	3192932.66	25.35
B-46	13790165.72	3193066.91	24.87
B-47	13790317.36	3193199.53	24.87
B-48	13790468.75	3193332.02	24.48
B-49	13790676.93	3193277.37	25.90
B-50	13790781.27	3193142.56	27.33
B-51	13790936.77	3192959.63	29.51
B-52	13789469.79	3192085.20	22.99
B-53	13789619.01	3191884.44	28.80
B-54	13788678.98	3191813.56	28.57
B-55	13788625.07	3191889.04	28.99
B-56	13788726.98	3191085.93	28.61
B-57	13788581.1	3191288.79	24.88
B-58	13787913.22	3190355.29	28.76



Boring No.	Northing (Grid, ft)	Easting (Grid, ft)	Boring Surface Elevation (ft)
B-59	13787800.88	3190514.38	23.57
B-60	13787134.39	3189680.18	28.36
B-61	13786976.9	3189874.38	28.74
B-62	13785900.00	3188564.99	26.27
B-63	13785144.79	3187757.15	25.59
B-64	13784963.94	3187758.98	23.56
B-65	13783900.36	3187914.00	24.07
B-66	13783873.31	3187503.54	25.36
B-67	13783866.81	3187265.19	24.99
B-68	13783851.5	3186896.05	23.83
B-69	13783412.24	3187467.24	26.71
B-70	13783417.81	3187314.31	26.16
B-71	13786754.06	3187613.52	26.11
B-72	13786733.82	3187389.62	24.12
B-73	13786711.34	3187069.64	24.70
B-74	13786699.81	3186704.33	20.79

<u>Soil Borings:</u> The field drilling was performed using a truck-mounted drill rig. Prior to drilling, existing concrete pavement at Borings B-7, B-15, B-27, B-43, B-51, B-62, B-63, and B-69 through B-71 was cut with a core barrel. Existing asphalt pavement and base at Borings B-23, B-55, and B-61 were augered through during drilling. The borings were advanced using dry auger method. Undisturbed samples of cohesive soils were obtained from the borings by pushing 3-inch diameter thin-wall, seamless steel Shelby tube samplers in accordance with ASTM D 1587. Granular soils were sampled with a 2-inch split-barrel sampler in accordance with ASTM D1586. In addition, the 2-inch split-barrel sampler was also used at 5 feet intervals on selected borings (regardless of the soil type encountered) as requested by Atkins. Standard Penetration Test (SPT) resistance value for this sample was recorded as "Blows per foot" and is shown on the representative boring log. Strength of the cohesive soils was estimated in the field using a hand penetrometer. The undisturbed samples of cohesive soils were sealed in plastic bags to reduce moisture loss and disturbance. The samples were then placed in core boxes and transported to the AEC laboratory for testing and further study. Groundwater readings were obtained during drilling and upon completion of drilling. The boreholes were then grouted with cement-bentonite upon completion of drilling, and existing pavement (where present) was patched with high strength non-shrink



grout. Details of the soils encountered in our borings are presented on Plates A-3 through A-76, in Appendix A. A key to symbols for the boring logs is presented on Plate A-77, in Appendix A.

<u>Sample Pits:</u> In addition to soil borings, four sample pits were excavated in the vicinity of Borings B-8, B-19, B-31, and B-44 to collect subgrade materials for Modified Proctor (ASTM D 1557) and CBR (ASTM D 1883) testing (see Section 3.0 of this report). AEC used a drill rig with a continuous flight auger to collect samples continuously from a depth of 0 to 4 feet below grade. The samples were then bagged and transported to the AEC laboratory for testing. The pits were backfilled with bentonite chips upon completion of field work.

Dynamic Cone Penetrometer (DCP) Tests: Thirty-seven (37) DCP tests were performed in accordance with ASTM D 6951 adjacent to the locations of Borings B-2, B-4, B-6 through B-8, B-10, B-12, B-14, B-16, B-18, B-20, B-22, B-26, B-28, B-30, B-32, B-34, B-36, B-38, B-40, B-42, B-44, B-46, B-48, B-50, B-53, B-55, B-56, B-58, B-60, B-64, B-66 through B-68, and B-72 through B-74. AEC used the DCP test data to estimate CBR versus penetration depth. CBR values versus penetration depth for each DCP test are presented on Plates B-13 through B-49, in Appendix B.

3.0 LABORATORY TESTING

Soil laboratory testing was performed by AEC personnel. Samples from the borings were examined and classified in the laboratory by a geotechnical technician under supervision of a geotechnical engineer. Laboratory tests were performed on selected soil samples to evaluate the engineering properties of the foundation soils in accordance with applicable ASTM Standards. Atterberg limits, moisture contents, percent passing a No. 200 sieve, grain size analysis, and dry unit weight tests were performed on selected samples to establish the index properties and confirm field classification of the subsurface soils. Strength properties of cohesive soils were estimated by means of torvane (TV), unconfined compression (UC), and unconsolidated-undrained (UU) triaxial tests performed on undisturbed samples. The test results are presented on the representative boring logs. Classification of soils for engineering purposes, terms used on boring logs, and reference ASTM Standards for laboratory testing are presented on Plates A-78 through A-80, in Appendix A. The results of grain size analyses are presented on Plate A-81, in Appendix A.

<u>Sulfate Content Tests</u>: AEC performed sulfate content tests on selected soil samples in accordance with Texas Department of Transportation (TxDOT) test method Tex-145-E to determine if the onsite soils have a potential for sulfate attack on lime-stabilized subgrade for pavements. Sulfate content test results are presented on Table



2.

Sample ID and Description	Sulfate Content (mg/kg)	Treatment Level for Roadway Subgrade ⁽¹⁾
B-1, 6'-8', Fat Clay (CH)	20	Level 1
B-2, 4'-6', Fat Clay (CH)	13	Level 1
B-3, 4'-6', Fat Clay (CH)	20	Level 1
B-4, 2'-4', Fat Clay (CH)	80	Level 1
B-5, 0'-2', Fill: Fat Clay (CH)	20	Level 1
B-6, 2'-4', Fat Clay (CH)	42	Level 1
B-7, 4'-6', Fat Clay with Sand (CH)	47	Level 1
B-8, 0'-2', Fat Clay (CH)	20	Level 1
B-9, 2'-4', Fat Clay (CH)	42	Level 1
B-10, 4'-6', Fat Clay (CH)	40	Level 1
B-11, 0'-2', Fat Clay (CH)	40	Level 1
B-12, 4'-6', Fat Clay (CH)	51	Level 1
B-13, 0'-2', Fat Clay (CH)	22	Level 1
B-14, 4'-6', Fat Clay (CH)	33	Level 1
B-15, 2'-4', Fat Clay (CH)	13	Level 1
B-16, 0'-2', Fat Clay (CH)	20	Level 1
B-17, 4'-6', Fat Clay (CH)	60	Level 1
B-18, 6'-8', Fat Clay (CH)	20	Level 1
B-19, 0'-2', Fat Clay with Sand (CH)	0	Level 1
B-20, 4'-6', Fat Clay (CH)	20	Level 1
B-21, 4'-6', Fat Clay (CH)	20	Level 1
B-22, 0'-2', Fat Clay (CH)	40	Level 1
B-23, 6'-8', Fat Clay (CH)	40	Level 1
B-24, 0'-2', Fat Clay (CH)	60	Level 1
B-25, 4'-6', Fat Clay with Sand (CH)	60	Level 1
B-26, 6'-8', Fat Clay (CH)	40	Level 1
B-27, 4'-6', Fat Clay (CH)	40	Level 1

Table 2. Sulfate Content Test Results



Sample ID and Description	Sulfate Content (mg/kg)	Treatment Level for Roadway Subgrade ⁽¹⁾
B-28, 4'-6', Lean Clay (CL)	33	Level 1
B-29, 6'-8', Fat Clay (CH)	9	Level 1
B-30, 0'-2', Lean Clay (CL)	7	Level 1
B-31, 2'-4', Fat Clay (CH)	47	Level 1
B-32, 4'-6', Fat Clay (CH)	80	Level 1
B-33, 0'-2', Fill: Fat Clay (CH)	20	Level 1
B-34, 4'-6', Lean Clay with Sand (CL)	33	Level 1
B-35, 0'-2', Lean Clay (CL)	13	Level 1
B-36, 6'-8', Fat Clay (CH)	40	Level 1
B-37, 2'-4', Lean Clay (CL)	47	Level 1
B-38, 2'-4', Fat Clay (CH)	22	Level 1
B-39, 0'-2', Fill: Fat Clay (CH)	18	Level 1
B-40, 4'-6', Fat Clay (CH)	49	Level 1
B-41, 4'-6', Lean Clay with Sand (CL)	27	Level 1
B-42, 2'-4', Fill: Lean Clay (CL)	40	Level 1
B-43, 4'-6', Fat Clay (CH)	20	Level 1
B-44, 4'-6', Fat Clay (CH)	40	Level 1
B-45, 4'-6', Fat Clay (CH)	47	Level 1
B-46, 6'-8', Lean Clay (CL)	20	Level 1
B-47, 0'-2', Fill: Fat Clay (CH)	27	Level 1
B-48, 4'-6', Lean Clay with Sand (CL)	20	Level 1
B-49, 4'-6', Fill: Fat Clay (CH)	60	Level 1
B-50, 6'-8', Fat Clay (CH)	20	Level 1
B-51, 4'-6', Fill: Fat Clay with Sand (CH)	40	Level 1
B-52, 2'-4', Fat Clay (CH)	40	Level 1
B-53, 0'-2', Fill: Fat Clay (CH)	20	Level 1
B-54, 6'-8', Fat Clay (CH)	60	Level 1
B-55, 1'-2', Fat Clay (CH)	60	Level 1
B-56, 4'-6', Fat Clay (CH)	20	Level 1
B-57, 4'-6', Fat Clay (CH)	20	Level 1



Sample ID and Description	Sulfate Content (mg/kg)	Treatment Level for Roadway Subgrade ⁽¹⁾
B-58, 0'-2', Fill: Fat Clay (CH)	20	Level 1
B-59, 6'-8', Fat Clay (CH)	40	Level 1
B-60, 4'-6', Fat Clay (CH)	20	Level 1
B-61, 4'-6', Fat Clay (CH)	120	Level 1
B-62, 4'-6', Fat Clay (CH)	40	Level 1
B-63, 6'-8', Fat Clay (CH)	7	Level 1
B-64, 4'-6', Fill: Fat Clay (CH)	40	Level 1
B-65, 6'-8', Fat Clay (CH)	0	Level 1
B-66, 0'-2', Fill: Lean Clay	20	Level 1
B-67, 4'-6', Fat Clay (CH)	60	Level 1
B-68, 6'-8', Fat Clay (CH)	40	Level 1
B-69, 8'-10', Fat Clay (CH)	60	Level 1
B-70, 3'-4', Fill: Fat Clay (CH)	60	Level 1
B-71, 1'-2', Fill: Silty Sand	0	Level 1
B-72, 4'-6', Fat Clay (CH)	20	Level 1
B-73, 2'-4', Fat Clay (CH)	40	Level 1
B-74, 4'-6', Lean Clay (CL)	20	Level 1

Notes: (1) Evaluation of sulfate attack on stabilized subgrade for roadways is based on TxDOT's "Guidelines for Treatment of Sulfate-Rich Soils and Bases in Pavement Structures" criteria.

According to TxDOT's "Guidelines for Treatment of Sulfate-Rich Soils and Bases in Pavement Structures", different levels of treatment are required if roadway subgrade will be stabilized. As defined by TxDOT's document: (i) Level 1 treatment (Traditional Treatment) can be used for roadway subgrades that have a sulfate content of 3,000 ppm or less; (ii) Level 2 treatment (Modified Treatment) can be used for roadway subgrades that have a sulfate content between 3,000 ppm and 8,000 ppm; and (iii) Level 3 treatment (Alternative Treatment) is required when the sulfate content is greater than 8,000 ppm. Based on Table 2, the existing soils along the alignment have very low sulfate contents (i.e. significantly less than 3,000 ppm). Based on the results presented in Table 2, Level 1 treatment (Traditional Treatment) can be used for roadway subgrade stabilization.

<u>Chemical Tests</u>: To evaluate the potential for chloride attack on pavements, AEC selected nineteen soil samples for chemical analyses. Chemical testing included pH, resistivity, and chloride content. AEC used TxDOT test



methods for each test type, Tex-128-E, Tex-129-E, and Tex-620-J, respectively. A summary of the chemical test results are presented on Table 3 below.

Sample ID	Resistivity (ohm/cm)	Chloride (mg/kg)	рН	Aggressive Environment
B-1, 0'-2'	992	197	7.94	Yes
B-5, 2'-4'	830	99	8.01	Yes
B-9, 6'-8'	738	329	8.09	Yes
B-13, 4'-6'	821	165	8.08	Yes
B-17, 0'-2'	747	395	6.01	Yes
B-21, 0'-2'	2633	99	5.45	Yes
B-25, 0'-2'	968	148	7.27	Yes
B-31, 2'-4'	632	329	8.02	Yes
B-33, 4'-6'	840	99	8.28	Yes
B-37, 0'-2'	1140	329	8.39	Yes
B-41, 2'-4'	1031	329	8.73	Yes
B-45, 4'-6'	946	329	8.84	Yes
B-49, 0'-2'	1123	197	8.10	Yes
B-53, 4'-6'	747	148	8.23	Yes
B-57, 0'-2'	1390	99	8.51	Yes
B-61, 2'-4'	798	99	7.32	Yes
B-65, 0'-2'	1005	197	7.87	Yes
B-69, 4'-6'	463	296	7.79	Yes
B-73, 4'-6'	1089	99	8.70	Yes

Table 3. Resistivity, Chloride, and pH Analysis Results

According to the Federal Highway Administration (FHWA) Design Manual "Design and Construction of Driven Pile Foundations", concrete design (AEC recommends that the FHWA foundation design concept also be applied to reinforcing steel for concrete pavement design) should be based on an aggressive subsurface environment whenever the pH value is 4.5 or less. Alternately, if the resistivity is less than 2,000 ohms/cm, the soils should be treated as an aggressive environment. If the soil resistivity is between 2,000 and 5,000 ohms/cm, and the chloride ion content is greater than 100 parts per million (ppm), the pavement design should be based on an aggressive subsurface environment. Resistivity values greater than 5,000 ohms/cm can be considered non-aggressive environments.



Based on the test results in Table 3 and FHWA criteria, the tested soil samples are considered an aggressive environment for reinforcing steel.

<u>Organic Matter Content:</u> AEC performed organic matter content tests on selected soil samples in accordance with ASTM D 2974. Organic content test results are summarized on Table 4 and presented on Plates A-82 and A-83, in Appendix A.

Sample ID and Description	Organic Content (%)
B-1, 6'-8', Fat Clay (CH)	4.6
B-5, 0'-2', Fill: Fat Clay (CH)	5.0
B-9, 2'-4', Fat Clay (CH)	5.5
B-13, 0'-2', Fat Clay (CH)	5.7
B-17, 0'-2', Fat Clay (CH)	5.7
B-21, 0'-2', Lean Clay (CL)	5.3
B-25, 4'-6', Fat Clay with Sand (CH)	3.0
B-31, 0'-2', Lean Clay with Sand (CL)	3.8
B-33, 0'-2', Fill: Fat Clay (CH)	6.2
B-37, 0'-2', Fat Clay (CH)	5.8
B-41, 0'-2', Fill: Fat Clay (CH)	5.2
B-45, 4'-6', Fat Clay (CH)	3.1
B-49, 2'-4', Fill: Fat Clay (CH)	2.5
B-53, 0'-2', Fill: Fat Clay (CH)	4.1
B-57, 2'-4', Fat Clay (CH)	3.1
B-61, 6'-8', Sandy Lean Clay (CL)	2.5
B-65, 6'-8', Fat Clay (CH)	4.5

 Table 4. Organic Matter Content Test Results (ASTM D 2974)



Sample ID and Description	Organic Content (%)
B-69, 6'-8', Fat Clay (CH)	5.9
B-73, 0'-2', Fill: Fat Clay with Sand (CH)	3.9

<u>Compaction and CBR</u>: Soil (from the ground surface to a depth of 4 feet below grade) recovered from the sample pits were mixed and split in general accordance with ASTM C 702. After splitting, Atterberg limits and a Percent Passing a 200-sieve analysis were performed to determine the index properties and grain size distribution of the samples. The samples were molded and compacted in accordance with ASTM D 1557 (Modified Proctor). After the samples were compacted, it is soaked for a period of 96 hours and a CBR (ASTM D 1883) test was performed. AEC will perform additional Modified Proctor and CBR tests on lime stabilized soil samples, which will be presented on a separate addendum letter.

Modified Proctor compaction test results on natural soils are presented on Plates B-1 through B-4, in Appendix B. CBR test results are presented on Plates B-5 through B-12, in Appendix B. A summary of sample pit index properties and CBR test results are presented on Table 5 and Table 6.

Sample ID and Description	Liquid Limit (%)	Plasticity Index (%)	Percent Passing #200 Sieve (%)	ASTM D 1557 Maximum Dry Density (pcf)	ASTM D 1557 Optimum Moisture Content (%)
B-8, 0'-4', Fat Clay (CH)	73	51	95.4	107.1	19.8
B-19, 0'-4', Fat Clay (CH)	59	42	90.4	116.3	14.5
B-31, 0'-4', Lean Clay with Sand (CL)	44	30	76.2	125.6	11.1
B-44, 0'-4', Lean Clay (CL)	45	29	91.5	119.8	12.8

Table 5. Sample Pit Soil Properties

Table 6. California Bearing Ratio Test Results (ASTM D 1883)

Sample ID	Percent Compaction (%), ASTM D 1557	Dry Density (pcf)	CBR (%)
B-8, 0'-4', Fat Clay (CH)	100	107.1	1.77
	95	101.7	1.54
	90	96.4	1.32
	85	91.0	1.13



Sample ID	Percent Compaction (%), ASTM D 1557	Dry Density (pcf)	CBR (%)
	100	116.3	3.10
D 10 0' 4' Est Class (CID	95	110.5	2.10
B-19, 0'-4', Fat Clay (CH)	90	104.7	1.75
	85	98.9	1.42
	100	125.6	3.36
B-31, 0'-4', Lean Clay with	95	119.3	2.98
Sand (CL)	90	113.0	2.13
	85	106.8	1.26
	100	119.8	2.48
\mathbf{D} 44 0' 4' Loop Clay (CL)	95	113.8	2.45
B-44, 0'-4', Lean Clay (CL)	90	107.8	2.05
	85	101.8	1.60

4.0 <u>SITE CONDITIONS</u>

In general, Taxiway L is to be located to the east and parallel to existing Runway 4-22. The project area is primarily flat and covered with moved grass. AEC notes that the site experienced greater than normal seasonal rainfall in the period when our field work was taking place (from June 2021 to August 2021). Most of our fieldwork (i.e., soil borings and field DCP tests) was performed when the ground surface was moist or wet.

A summary of pavement sections encountered in AEC's borings is presented on Table 7. Photographs of concrete core sections are presented on Plates 1 through 4, in the Illustrations.

Boring No.	Core Location	Pavement Thickness
B-7	Access Road	6.5" concrete
B-15	Taxiway X	6" concrete
В-23	Runway 35R Extension (demolished)	12" stabilized sand base
B-27	Access Road	2.5" asphalt, 8.25" concrete
B-43	Access Road	17.75" concrete, 7.25" stabilized soil base
B-51	Runway 22	28" concrete, 5.25" stabilized soil base
B-55	Access Road	2" asphalt, 6" sand and gravel base
B-61	Runway 35R	12" sand with shell base

Table 7. Existing Pavement Encountered at Borings



Boring No.	Core Location	Pavement Thickness
	Extension (demolished)	
B-62	Taxiway X	12.5" concrete, 3" asphalt, 7.8" concrete, 13.1" stabilized soil base
B-63	Runway 4	15" concrete, 11.5" cement stabilized base, 10.5" stabilized soil subbase
B-69	Runway 35L	16.25" concrete, 7.75" cement stabilized base, 9.75" stabilized soil subbase
B-70	Taxiway F	15.5" concrete, 8" cement stabilized base, 12" stabilized soil subbase
B-71	Taxiway D	13" concrete

4.1 Subsurface Conditions

Details of the soils encountered during drilling are presented in the boring logs on Plates A-3 through A-76, in Appendix A. Soil strata encountered in our borings are summarized below.

<u>Boring</u> B-1	<u>Depth (ft)</u> 0 - 4 4 - 8 8 - 12 12 - 16	<u>Description of Stratum</u> Fill: very stiff to hard, Fat Clay (CH), with calcareous nodules Firm to stiff, Fat Clay (CH), with slickensides and ferrous nodules Stiff to very stiff, Lean Clay (CL), with slickensides and ferrous nodules Stiff to very stiff, Fat Clay (CH), with slickensides, calcareous nodules, and lean clay seams
B-2	0 - 8 8 - 10 10 - 16	Soft to very stiff, Fat Clay (CH), with slickensides Firm to stiff, Lean Clay (CL), with fat clay pockets Firm to very stiff, Fat Clay (CH), with slickensides and calcareous nodules
B-3	0 - 2 2 - 16	Fill: very stiff, Fat Clay (CH), with roots and shell fragments Firm to very stiff, Fat Clay (CH), with slickensides
B-4	0 - 16	Firm to hard, Fat Clay (CH), with slickensides
B-5	0 - 2 2 - 8 8 - 16	Fill: very stiff, Fat Clay (CH), with calcareous and ferrous nodules Stiff to very stiff, Fat Clay (CH), with slickensides and ferrous nodules Very stiff to hard, Lean Clay (CL), with fat clay seams and pockets
B-6	0 - 2 2 - 14 14 - 16	Fill: stiff, Fat Clay (CH), with sandy lean clay seams, shell fragments, and roots Soft to very stiff, Fat Clay (CH), with slickensides Very stiff, Lean Clay (CL), with calcareous nodules, silty clay seams, and fat clay pockets
B-7	0 - 0.54 0.54 - 2 2 - 10	Pavement: see Table 7 in Section 4.0 of this report Fill: stiff to very stiff, Fat Clay with Sand (CH), with silty sand seams and ferrous nodules Firm to very stiff, Fat Clay with Sand (CH)



Boring B-7 (cont.)	<u>Depth (ft)</u> 10 - 14 14 - 16	<u>Description of Stratum</u> Stiff to very stiff, Lean Clay (CL), with ferrous stains Stiff to very stiff, brown Fat Clay (CH), with calcareous nodules
B-8	0 - 16	Firm to very stiff, Fat Clay (CH), with slickensides
B-9	0 - 16	Firm to very stiff, Fat Clay (CH), with slickensides
B-10	0 - 10 10 - 16	Soft to very stiff, Fat Clay (CH) Stiff to very stiff, Lean Clay (CL)
B-11	0 - 10 10 - 16	Firm to very stiff, Fat Clay (CH), with slickensides Stiff to hard, Lean Clay (CL)
B-12	0 - 16	Firm to very stiff, Fat Clay (CH), with slickensides
B-13	0 - 16	Stiff to very stiff, Fat Clay (CH), with slickensides
B-14	0 - 2 2 - 16	Very stiff, Fat Clay with Sand (CH), with calcareous nodules and roots Firm to hard, Fat Clay (CH), with slickensides
B-15	0 - 0.5 0.5 - 2 2 - 14 14 - 16	Pavement: see Table 7 in Section 4.0 of this report Fill: stiff, Lean Clay (CL), with sandy lean clay pockets Firm to very stiff, Fat Clay (CH), with slickensides Stiff to very stiff, Lean Clay (CL)
B-16	0 - 10 10 - 14 14 - 16	Soft to hard, Fat Clay (CH) Stiff to very stiff, Lean Clay (CL) Hard, Silty Clay (CL-ML), with silt seams
B-17	0 - 10 10 - 16	Stiff to very stiff, Fat Clay (CH), with calcareous nodules Stiff to very stiff, Lean Clay (CL), with slickensides
B-18	0 - 16	Firm to hard, Fat Clay (CH), with slickensides
B-19	0 - 6 6 - 16	Firm to hard, Fat Clay with Sand (CH) Stiff to hard, Fat Clay (CH), with slickensides
B-20	0 - 16	Firm to hard, Fat Clay (CH)
B-21	0 - 2 2 - 6 6 - 8 8 - 10 10 - 16	Hard, Lean Clay (CL), with roots Stiff, Fat Clay (CH) Very stiff, Fat Clay with Sand (CH), with lean clay seams, and calcareous and ferrous nodules Very stiff, Fat Clay (CH), with slickensides and calcareous nodules Firm to very stiff, Lean Clay (CL), with fat clay seams and pockets
B-22	0 - 8 8 - 12 12 - 14	Stiff to very stiff, Fat Clay (CH) Firm to stiff, Lean Clay (CL) Silt (ML), with sand pockets and lean clay seams, wet



Boring B-22 (cont.)	<u>Depth (ft)</u> 14 - 16	Description of Stratum Medium dense, Silty Clayey Sand (SC-SM), with lean clay pockets and calcareous nodules, wet
B-23	0 - 1 1 - 10 10 - 14 14 - 16	Base: see Table 7 in Section 4.0 of this report Stiff to very stiff, Fat Clay (CH), with slickensides Stiff to very stiff, Lean Clay (CL) Stiff to very stiff, Silty Clay (CL-ML), with sandy lean clay pockets
B-24	0 - 14 14 - 16	Firm to very stiff, Fat Clay (CH), with slickensides Medium dense, Silt (ML), with silty clay seams, wet
B-25	0 - 10 10 - 12 12 - 16	Stiff to very stiff, Fat Clay with Sand (CH) Very stiff, Lean Clay (CL), with calcareous nodules Silt (ML), with sand pockets, wet
B-26	0 - 8 8 - 10 10 -16	Firm to very stiff, Fat Clay (CH), with slickensides Stiff to very stiff, Lean Clay (CL) Loose, Silt with Sand (ML), wet
B-27	0 - 0.9 0.9 - 2 2 - 10 10 - 14 14 - 16	Pavement: see Table 7 in Section 4.0 of this report Fill: hard, Lean Clay with Sand (CL), with gravel Very stiff to hard, Fat Clay (CH), with slickensides Very stiff, Lean Clay (CL), with clayey sand seams and pockets Silt (ML), wet
B-28	0 - 2 2 - 6 6 - 10 10 - 16	Very stiff, Fat Clay (CH) Soft to very stiff, Lean Clay (CL), with sand partings Medium dense, Silty Sand (SM), wet Loose to medium dense, Poorly Graded Sand with Silt (SP-SM), wet
B-29	0 - 2 2 - 4 4 - 8 8 - 14 14 - 16	Very stiff, Fat Clay (CH), with lean clay and silty sand pockets Hard, Lean Clay with Sand (CL), with ferrous nodules Stiff to very stiff, Fat Clay (CH), with slickensides and calcareous nodules Firm to very stiff, Lean Clay (CL) Firm to stiff, Silty Clay (CL-ML), with calcareous nodules
B-30	0 - 2 2 - 10 10 - 16	Very stiff, Lean Clay (CL), with sand partings Stiff to very stiff, Fat Clay with Sand (CH), with slickensides Stiff to very stiff, Lean Clay (CL)
B-31	0 - 2 2 - 14 14 - 16	Very stiff, Lean Clay with Sand (CL), with roots Stiff to very stiff, Fat Clay (CH), with slickensides Very stiff, Lean Clay (CL)
B-32	0 - 16	Firm to hard, Fat Clay (CH), with slickensides
B-33	0 - 2 2 - 8 8 - 16	Fill: very stiff, Fat Clay (CH), with gravel, ferrous nodules, and roots Stiff to very stiff, Fat Clay with Sand (CH), with ferrous and calcareous nodules Very stiff to hard, Fat Clay (CH), with slickensides and calcareous nodules



Boring B-34	<u>Depth (ft)</u> 0 - 6 6 - 16	<u>Description of Stratum</u> Stiff to hard, Lean Clay with Sand (CL) Stiff to hard, Fat Clay (CH), with slickensides
B-35	0 - 2 2 - 6 6 - 10 10 - 16	Hard, Lean Clay (CL), with sand partings and roots Very stiff, Fat Clay (CH), with ferrous nodules Stiff to very stiff, Lean Clay (CL), with fat clay pockets and calcareous nodules Very stiff, Fat Clay (CH), with slickensides
B-36	0 - 2 2 - 16	Very stiff, Lean Clay with Sand (CL) Firm to hard, Fat Clay (CH), with slickensides
B-37	0 - 2 2 - 4 4 - 8 8 - 16	Hard, Fat Clay (CH), with calcareous nodules Very stiff, Lean Clay (CL) Stiff to very stiff, Fat Clay with Sand (CH), with calcareous nodules Stiff to very stiff, Fat Clay (CH), with slickensides, and calcareous nodules and pockets
B-38	0 - 2 2 - 16	Fill: hard, Lean Clay (CL), with fat clay seams, sand partings, and calcareous nodules Stiff to very stiff, Fat Clay (CH), with slickensides
B-39	0 - 2 2 - 4 4 - 16	Fill: stiff, Fat Clay (CH), with slickensides and lean clay seams Stiff to very stiff, Lean Clay (CL) Stiff to hard, Fat Clay (CH), with slickensides
B-40	0 - 2 2 - 8 8 - 10 10 - 16	Fill: very stiff, Fat Clay with Sand (CH), with lean clay seams and roots Stiff to very stiff, Fat Clay (CH) Very stiff, Lean Clay with Sand (CL), with calcareous nodules and pockets Stiff to very stiff, Fat Clay (CH), with slickensides
B-41	0 - 2 2 - 8 8 - 16	Fill: hard, Fat Clay (CH), with calcareous nodules and roots Stiff to very stiff, Lean Clay with Sand (CL), with abundant calcareous nodules Stiff to very stiff, Fat Clay (CH), with slickensides
B-42	0 - 4 4 - 8 8 - 16	Fill: hard, Lean Clay (CL) Stiff to very stiff, Lean Clay (CL) Stiff to hard, Fat Clay (CH), with slickensides
B-43	0 - 2.65 2.65 - 16	Pavement and base: see Table 7 in Section 4.0 of this report Stiff to very stiff, Fat Clay (CH), with slickensides
B-44	0 - 2 2 - 16	Fill: hard, Lean Clay with Sand (CL), with fat clay pockets and roots Stiff to hard, Fat Clay (CH), with slickensides
B-45	0 - 2 2 - 16	Fill: hard, Fat Clay with Sand (CH), with calcareous nodules and gravel Stiff to very stiff, Fat Clay (CH), with slickensides
B-46	0 - 2 2 - 4	Fill: very stiff, Fat Clay (CH), with sandy lean clay pockets and roots Fill: Silty Clayey Sand (SC-SM), with shell fragments



Boring B-46 (cont.)	<u>Depth (ft)</u> 4 - 6 6 - 8	<u>Description of Stratum</u> Fill: firm to stiff, Lean Clay (CL), with sandy lean clay seams and shell fragments Stiff to very stiff, Lean Clay (CL), with ferrous nodules and abundant calcareous nodules
	8 - 16	Firm to very stiff, Fat Clay (CH), with slickensides
B-47	0 - 2 2 - 6 6 - 10 10 - 16	Fill: hard, Fat Clay (CH), with gravel and roots Soft to stiff, Fat Clay (CH), with slickensides Stiff to very stiff, Lean Clay with Sand (CL) Very stiff, Fat Clay (CH)
B-48	0 - 4 4 - 10 10 - 16	Fill: stiff to hard, Fat Clay (CH), with slickensides and calcareous nodules Firm to hard, Lean Clay with Sand (CL) Stiff to very stiff, Fat Clay (CH), with slickensides
B-49	0 - 6 6 - 10 10 - 16	Fill: stiff to very stiff, Fat Clay (CH) Stiff to very stiff, Lean Clay (CL), with ferrous nodules and fat clay seams Stiff to very stiff, Fat Clay (CH), with slickensides
B-50	0 - 2.77 2.77 - 6 6 - 10 10 - 16	Pavement and base: see Table 7 in Section 4.0 of this report Fill: very stiff, Fat Clay with Sand (CH) Fill: very stiff to hard, Fat Clay (CH) Very stiff, Fat Clay (CH), with ferrous nodules
B-51	0 - 2.77 2.77 - 6 6 - 10 10 - 16	Pavement and base: see Table 7 in Section 4.0 of this report Fill: very stiff, Fat Clay with Sand (CH) Fill: very stiff to hard, Fat Clay (CH) Very stiff, Fat Clay (CH), with ferrous nodules
B-52	0 - 2 2 - 16	Fill: very stiff, Fat Clay with Sand (CH), with ferrous and calcareous nodules Stiff to very stiff, Fat Clay (CH), with slickensides
B-53	0 - 2 2 - 8 8 - 10 10 - 16	Fill: very stiff, Fat Clay (CH), with ferrous nodules and roots Stiff to very stiff, Fat Clay (CH), with ferrous nodules Stiff to very stiff, Lean Clay with Sand (CL), with calcareous and ferrous nodules Stiff to hard, Fat Clay (CH), with slickensides
B-54	0 - 2 2 - 16	Hard, Lean Clay with Sand (CL), with silty sand seams and roots Stiff to hard, Fat Clay (CH), with slickensides
B-55	0 - 0.67 0.67 - 16	Pavement and base: see Table 7 in Section 4.0 of this report Firm to hard, Fat Clay (CH), with slickensides
B-56	0 - 2 2 - 16	Fill: very stiff, Fat Clay (CH), with ferrous nodules and roots Firm to hard, Fat Clay (CH), with slickensides
B-57	0 - 10 10 - 16	Stiff to hard, Fat Clay (CH), with slickensides and calcareous nodules Stiff to very stiff, Lean Clay (CL)



Boring B-58	<u>Depth (ft)</u> 0 - 4 4 - 16	<u>Description of Stratum</u> Fill: stiff to very stiff, Fat Clay (CH) Firm to hard, Fat Clay (CH), with slickensides
B-59	0 - 2 2 - 8 8 - 12 12 - 16	Hard, Sandy Lean Clay (CL), with ferrous and calcareous nodules Stiff to hard, Fat Clay (CH), with slickensides Soft to stiff, Lean Clay (CL) Firm to stiff, Silty Clay (CL-ML)
B-60	0 - 2 2 - 16	Very stiff, Lean Clay with Sand (CL), with roots Firm to hard, Fat Clay (CH), with slickensides
B-61	0 - 1 1 - 6 6 - 12 12 - 16	Base: see Table 7 in Section 4.0 of this report Stiff to hard, Fat Clay (CH), with ferrous nodules Very stiff, Sandy Lean Clay (CL), with slickensides and ferrous nodules Sandy Silt (ML)
B-62	0 - 3.03 3.03 - 16	Pavement and base: see Table 7 in Section 4.0 of this report Stiff to very stiff, Fat Clay (CH), with slickensides
B-63	0 - 3.08 3.08 - 12 12 - 16	Pavement and base: see Table 7 in Section 4.0 of this report Stiff to very stiff, Fat Clay (CH), with slickensides Very stiff, Lean Clay (CL), with sand pockets
B-64	0 - 6 6 - 10 10 - 12 12 - 16	Fill: firm to very stiff, Fat Clay (CH), with slickensides Stiff to very stiff, Fat Clay (CH), with slickensides Hard, Lean Clay (CL) Stiff to very stiff, Fat Clay (CH)
B-65	0 - 14 14 - 16	Stiff to hard, Fat Clay (CH), with slickensides Silt (ML), with fat clay seams, wet
B-66	0 - 2 2 - 4 4 - 16	Fill: hard, Lean Clay (CL), with calcareous nodules, shell fragments, and roots Fill: stiff to very stiff, Fat Clay (CH), with slickensides and ferrous nodules Firm to very stiff, Fat Clay (CH), with slickensides
B-67	0 - 2 2 - 16	Fill: stiff to very stiff, Fat Clay with Sand (CH), with calcareous nodules, sand pockets, shell fragments, and roots Firm to very stiff, Fat Clay (CH), with slickensides
B-68	0 - 10 10 - 14 14 - 16	Firm to hard, Fat Clay (CH), with slickensides Stiff to hard, Lean Clay (CL) Stiff to very stiff, Fat Clay (CH)
B-69	0 - 2.81 2.81 - 4	Pavement and base: see Table 7 in Section 4.0 of this report Fill: very stiff, Fat Clay (CH), with calcareous nodules, sandy lean clay pockets, and gravel
	4 - 16	Firm to very stiff, Fat Clay (CH), with slickensides and ferrous nodules



Boring B-70	<u>Depth (ft)</u> 0 - 2.96 2.96 - 8 8 - 16	<u>Description of Stratum</u> Pavement and base: see Table 7 in Section 4.0 of this report Fill: stiff to very stiff, Fat Clay (CH), with slickensides Stiff to very stiff, Fat Clay (CH), with slickensides
B-71	0 - 1.08 1.08 - 2 2 - 14 14 - 16	Pavement: see Table 7 in Section 4.0 of this report Fill: Silty Sand (SM), with fat clay seams and pockets Stiff to very stiff, Fat Clay (CH), with slickensides Stiff to very stiff, Lean Clay (CL), with silt partings
B-72	0 - 2 2 - 12 12 - 16	Fill: hard, Fat Clay (CH), with calcareous nodules and roots Firm to very stiff, Fat Clay (CH), with slickensides Firm to stiff, Lean Clay (CL)
B-73	0 - 2 2 - 16	Fill: hard, Fat Clay with Sand (CH), with ferrous nodules, shell fragments, gravel, and roots Firm to very stiff, Fat Clay (CH), with slickensides
B-74	0 - 2 2 - 4 4 - 6 6 - 10 10 - 16	Fill: very stiff, Fat Clay with Sand (CH), with calcareous nodules Stiff to very stiff, Fat Clay (CH), with calcareous and ferrous nodules Stiff to hard, Lean Clay (CL), with calcareous nodules and pockets Firm to very stiff, Fat Clay (CH), with slickensides Firm to stiff, Silty Clay with Sand (CL-ML)

<u>Subsurface Soil Properties</u>: The cohesive soils encountered in the borings (including fill, excluding silty clayey sand) have slight to very high plasticity (see "Degree of Plasticity of Cohesive Soils" on Plate A-78, in Appendix A), with Liquid Limits (LL) ranging from 29 to 90 and Plasticity Indices (PI) ranging from 10 to 65. The cohesive soils encountered are classified as "CL-ML", "CL", and "CH" type soils while the granular soils are classified as "ML", "SM", "SC-SM", and "SP-SM" type soils in accordance with ASTM D 2487.

Groundwater: Groundwater levels encountered in the borings during drilling are summarized in Table 8.

Boring No.	Date Drilled	Boring Depth (ft)	Groundwater Depth (ft)
B-1	8/17/21	16	Dry (Drilling) Dry (Complete)
B-2	8/4/21	16	12 (Drilling) 12 (Complete)
В-3	8/4/21	16	15 (Drilling) 14 (Complete)
B-4	8/5/21	16	15 (Drilling) 13 (Complete)

 Table 8. Summary of Boring Groundwater Depths



Boring No.	Date Drilled	Boring Depth (ft)	Groundwater Depth (ft)
B-5	8/5/21	16	Dry (Drilling)
			Dry (Complete)
B-6	7/1/21	16	15 (Drilling)
			13 (Complete) Dry (Drilling)
B-7	7/1/21	16	Dry (Complete)
D 0	E /1 /0.1	16	Dry (Drilling)
B-8	7/1/21	16	14 (Complete)
B-9	7/1/21	16	Dry (Drilling)
D-7	// 1/ 2 1	10	Dry (Complete)
B-10	8/3/21	16	4 ⁽¹⁾ (Drilling)
2 10	0,0,21		Dry (Complete)
B-11	6/21/21	16	14 (Drilling)
	-	-	10 (Complete)
B-12	6/21/21	16	Dry (Drilling)
	-	-	Dry (Complete)
B-13	6/21/21	16	Dry (Drilling)
			Dry (Complete)
B-14	6/21/21	16	Dry (Drilling)
	-	-	Dry (Complete)
B-15	7/1/21	16	Dry (Drilling)
_	// 1/ 2 1	10	Dry (Complete)
B-16	8/3/21	16	4.2 (Drilling)
-		-	6.3 (Complete)
B-17	8/3/21	16	Dry (Drilling)
			Dry (Complete)
B-18	8/3/21	16	15 (Drilling)
B-19	8/3/21	16	Dry (Drilling)
-		-	Dry (Complete)
B-20	8/3/21	16	Dry (Drilling)
-		-	Dry (Complete)
B-21	8/2/21	16	Dry (Drilling)
	-	-	Dry (Complete)
B-22	8/2/21	16	10 (Drilling)
			7.9 (15 mins)
B-23	8/2/21	16	14 (Drilling)
			7.1 (15 mins)
B-24	8/2/21	16	15 (Drilling)
	0,2,21		7.7 (Complete)
D 25	0/2/21	17	14 (Drilling)
B-25	8/2/21	16	6.6 (15 mins)
			6.6 (Complete)
B-26	8/2/21	16	14 (Drilling)
		-	7.9 (15 mins)
B-27	7/1/21	16	14 (Drilling)
	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	÷ •	11 (Complete)



Boring No.	Date Drilled	Boring Depth (ft)	Groundwater Depth (ft)
B-28	6/21/21	16	Dry (Drilling) 4 (Complete)
B-29	6/21/21	16	14 (Drilling) 7 (Complete)
B-30	6/21/21	16	14 (Drilling) 11 (Complete)
B-31	6/21/21	16	Dry (Drilling) Dry (Complete)
B-32	8/2/21	16	Dry (Drilling) Dry (Complete)
B-33	8/2/21	16	Dry (Drilling) Dry (Complete)
B-34	6/15/21	16	Dry (Drilling) Dry (Complete)
B-35	6/15/21	16	Dry (Drilling) Dry (Complete)
B-36	6/15/21	16	Dry (Drilling) Dry (Complete)
B-37	6/15/21	16	Dry (Drilling) Dry (Complete)
B-38	6/15/21	16	Dry (Drilling) Dry (Complete)
B-39	6/14/21	16	Dry (Drilling) Dry (Complete)
B-40	6/14/21	16	Dry (Drilling) Dry (Complete)
B-41	6/14/21	16	Dry (Drilling) Dry (Complete)
B-42	6/14/21	16	Dry (Drilling) Dry (Complete)
B-43	7/1/21	16	Dry (Drilling) Dry (Complete)
B-44	6/14/21	16	Dry (Drilling) Dry (Complete)
B-45	6/14/21	16	Dry (Drilling) Dry (Complete)
B-46	6/14/21	16	Dry (Drilling) Dry (Complete)
B-47	6/14/21	16	Dry (Drilling) Dry (Complete)
B-48	6/14/21	16	Dry (Drilling) Dry (Complete)
B-49	6/14/21	16	2 ⁽¹⁾ (Drilling) Dry (Complete)
B-50	8/4/21	16	14 (Drilling) 10 (Complete)



Boring No.	Date Drilled	Boring Depth (ft)	Groundwater Depth (ft)
B-51	8/10/21	16	Dry (Drilling)
D-31	0/10/21	10	Dry (Complete)
B-52	8/10/21	16	Dry (Drilling)
D-32	0/10/21	10	Dry (Complete)
B-53	8/10/21	16	Dry (Drilling)
D -33	0/10/21	10	Dry (Complete)
B-54	6/15/21	16	Dry (Drilling)
D 51	0/10/21	10	Dry (Complete)
B-55	8/3/21	16	Dry (Drilling)
2 33	0, 0, 21	10	Dry (Complete)
B-56	8/10/21	16	Dry (Drilling)
		- •	Dry (Complete)
B-57	8/10/21	16	15 (Drilling)
		-	13 (Complete)
B-58	8/4/21	16	Dry (Drilling)
	-	-	Dry (Complete)
B-59	8/10/21	16	10 (Drilling)
			4 (Complete)
B-60	8/4/21	16	12 (Drilling)
			10 (Complete)
B-61	8/4/21	16	15 (Drilling)
			13 (Complete)
B-62	8/10/21	16	Dry (Drilling)
			Dry (Complete)
B-63	8/10/21	16	Dry (Drilling)
			Dry (Complete)
B-64	8/10/21	16	15 (Drilling) 14 (Complete)
			14 (Drilling)
B-65	8/5/21	16	11 (Complete)
			Dry (Drilling)
B-66	8/17/21	16	Dry (Complete)
			Dry (Drilling)
B-67	8/17/21	16	Dry (Complete)
			Dry (Drilling)
B-68	8/17/21	16	15 (Complete)
			Dry (Drilling)
B-69	8/17/21	16	Dry (Complete)
	- / /		Dry (Drilling)
B-70	8/17/21	16	Dry (Complete)
D 71	8/17/21	16	Dry (Drilling)
B-7 1			Dry (Complete)
D 72	8/17/21	16	Dry (Drilling)
B-72			11 (Complete)
D 72	D 72 0/17/21 16		Dry (Drilling)
B-73	8/17/21	16	10 (Complete)



Boring No.	Date Drilled	Boring Depth (ft)	Groundwater Depth (ft)
B-74	8/17/21	16	10 (Drilling) 8 (5 mins)

Note: (1) Groundwater is likely perched.

The information in this report summarizes conditions found on the dates the borings were drilled. However, it should be noted that our groundwater observations are short term; groundwater depths and subsurface soil moisture contents will vary with environmental variations such as frequency and magnitude of rainfall and the time of year when construction is in progress.

4.2 Hazardous Materials

No signs of visual staining or odors were encountered during field drilling or during processing of the soil samples in the laboratory.

4.3 Subsurface Variations

It should be emphasized that: (i) at any given time, groundwater depths can vary from location to location, and (ii) at any given location, groundwater depths can change with time. Groundwater depths will vary with seasonal rainfall and other climatic/environmental events. Subsurface conditions may vary away from and in between the boring locations.

Clay soils in the Greater Houston area typically have secondary features such as slickensides, calcareous/ferrous nodules, and contain sand/silt seams/lenses/layers/pockets. It should be noted that the information in the boring logs are based on 3-inch diameter soil samples which were generally obtained from the borings at intervals of 2 feet continuously from the ground surface to a depth of 16 feet below existing grade. A detailed description of the soil secondary features may not have been obtained due to the small sample size and sampling interval between the samples. Therefore, while AEC's logs show some soil secondary features, it should not be assumed that the features are absent where not indicated on the logs.



4.4 Geologic Faults

AEC performed a desktop fault study which included a review of public maps, available literature, and aerial photographs. According to the published maps "Principal Active Faults of the Houston Area (after O'Neill and Van Siclen, May 1984)", and "Principal Surface Faults in the Central Houston Metropolitan Area (after O' Neill, Van Siclen, with additions by C. Norman, May 13, 2004)", the project site is located over the Friendswood Salt Dome. An overlay of the street map over the 1984 fault map indicates numerous faults are located near the Taxiway L alignment, but according to the overlay, the 1984 map shows no faults directly crossing the Taxiway L alignment itself. The closest fault to the Taxiway L alignment. The next closest fault, according to the 1984 fault map, is an un-named northeast-southwest oriented fault that is approximately 0.24 miles southwest of the Taxiway L alignment.

A map in the 1975 publication, "Active Faults in Southeastern Harris County, Texas", Geo I, pages 149 - 154, by Clanton, U.S. and Amsbury, D.L., indicate multiple faults in or near the project area. The map indicates at least two or more faults crossing the southern portion of the Taxiway L alignment. According to the article, these faults were associated with structural damages seen in nearby buildings, streets, and runways.

Fifty-two aerial photographs from 1944 to 2021 were reviewed on Google Earth on the internet. No evidence of faults near or crossing the Taxiway L alignment was observed.

If there are no historical Phase I Fault Investigation studies readily available of the Taxiway L alignment, AEC recommends a Phase I Fault Investigation for the project be performed since there are variations in fault locations on different maps and the article by Clanton, U.S. and Amsbury, D.L indicates multiple faults near and or crossing the southern half of the Taxiway L alignment.

<u>Limitations</u>: The desktop fault study provided in this report is limited to a review of available literature, aerial photographs, and maps. Distances are scaled from maps. Faults may exist in, cross, or adjoin the Project Alignment which were not identified in this report due to the following reasons: limitations of the scope of work and cost, no field observations were conducted; lack of documentation in the literature; and faults may have not been visible on the aerial photographs due to clarity of the aerial photographs, the presence of vegetation and environmental features, and modification of the land surface by human activities. Faults may also be present



below ground but do not currently have surface expressions. Identification of these faults is beyond the scope of work for this study.

5.0 ENGINEERING ANALYSIS AND RECOMMENDATIONS

According to information provided by Atkins, the project consists of design and construction of (i) approximately 10,000 feet long Taxiway L parallel to Runway 4-22, (ii) Taxiways E and D with approximately 1,200 feet length each, and (iii) additional connector taxiways.

<u>Construction Specifications</u>: For this report, AEC has referenced construction specifications from the Federal Aviation Administration Advisory Circular (FAA AC), where applicable. AEC should be notified if different construction specifications should be used, so that our recommendations can be updated as necessary. AEC has also referenced the 2015 HAS Design Criteria Manual as necessary.

5.1 Taxiway Pavement Subgrade

For the construction of the taxiways, it is AEC's opinion that it will be sound engineering practice for the subgrade soils beneath the pavement to be stabilized to provide uniform and long-lasting subgrade support of the pavement, as well as provide a weather resistant work platform during construction.

Lime Stabilized Subgrade: The subgrade soils beneath the pavement that were encountered in the borings along the taxiway alignments generally consist of fat/lean clay (CH/CL) with medium to very high plasticity. According to Section 2.16.12 of the 2015 HAS Design Criteria Manual, all subgrades should be lime/fly ash-treated or cement/fly ash-treated. However, based on the cohesive soils encountered in the borings, it is AEC's opinion that using fly ash or cement will not be effective for subgrade stabilization along the taxiway alignments. Instead, **AEC recommends lime stabilized subgrade be used alone for the construction of the taxiways**. Based on the subsurface soil conditions, AEC recommends that a minimum of 12 inches of subgrade soils beneath the proposed pavement be stabilized with a minimum of 8 percent lime by dry soil weight. AEC's preliminary lime series tests indicate that an 8 percent application rate (by dry soil weight) will be necessary; however, the actual percentage of lime should be determined by lime-series or pH method by the construction materials testing (CMT) laboratory prior to construction.



5.1.1 Determination of Rigid Pavement Design Parameters

Determination of the subgrade resilient modulus, E, the foundation modulus, k, and CBR is required for rigid pavement design. Based on the DCP test (see Plates B-13 to B-49, in Appendix B) and laboratory CBR test (Table 6 in Section 3.0) results, average CBR values are presented on Table 9.

Taxiway Alignment	Nearby Borings	Average CBR
Taxiway L/ Connector	B-1 through B-7	5
Taxiway L	B-8 through B-32	8
Taxiway L	B-33 to B-39	3
Taxiway L	B-40	15
Taxiway L	B-41 to B-43	1
Taxiway L	B-44	5
Taxiway L	B-45 to B-47	2
Taxiway L/ Connectors	B-48 to B-51, B-52, B-53, B- 63, B-64	5
Connector	B-54, B-55	20
Connectors	B-56 through B-59	8
Connector	B-60, B-61	2
Taxiway E	B-65 through B-68	5
Taxiway D	B-71 to B-74	8

Table 9. Average CBRs based on DCP and CBR Test Results

Based on DCP and CBR test results, it is AEC's opinion that using a design CBR of 3 (based on the lab CBR results) for the natural subgrade in the pavement design is reasonable. AEC notes that the CBR results derived from the field DCP tests may be affected by the frequent rainfall that occurred (see Section 4.0 of this report) when the field DCP tests were performed. AEC will perform additional modified proctor and CBR tests on lime stabilized test pit soil samples. Recommended design CBR for lime stabilized subgrade will be presented in a separate addendum letter. Preliminary optimum lime series content test results (which will be included in the addendum letter) indicate the optimum lime stabilization rate for the subgrade soils to be 8 percent by dry soil weight. However, the actual percentage of lime should be determined by lime-series or pH method by the CMT laboratory prior to construction.

Foundation modulus (k) and resilient modulus (E_{SG}) of the subgrade soil can be estimated using the following equations according to Item 326 of FAA AC 150/5360-6E.



$$k = \left[\frac{1500 \times CBR}{26}\right]^{0.7788}$$
.....Equation (1)
$$E_{SG} = 26k^{1.284}$$
....Equation (2)

where:

k = Foundation modulus of the subgrade, in pci E_{SG} = Resilient modulus of the subgrade, in psi

5.1.2 Subgrade Preparation

AEC assumes that the pavement will be constructed at or near existing grade. Subgrade preparation should extend to 5 feet beyond the paved area perimeters. The top 6 inches of existing soil and any deleterious materials at the ground surface should be stripped and wasted. In case of the presence of existing pavement and base, removal of existing pavement shall be performed in accordance with Item P-101 of the FAA AC 150/5370-10G Airport Construction Standards. After surface stripping, the subgrade should be cut to grade to accommodate the pavement section. After cutting to grade, we recommend that a competent soil technician inspect the exposed subgrade to determine if there are any unsuitable soils or other deleterious materials. Excavate and dispose of unsuitable soils and other deleterious materials which will not consolidate; the excavation depth should be increased when inspection indicates the presence of organics and deleterious materials to greater depths. The exposed soils should be proof-rolled in accordance with Item 216 of the 2014 TxDOT Standard Specifications for Construction and Maintenance of Highways, Streets, and Bridges to identify and remove any weak, compressible, or other unsuitable materials. Excavation and subgrade preparation shall be performed in accordance with Item P-152 of the FAA AC 150/5370-10G Airport Construction Standards.

Scarify the top 12 inches of the exposed subgrade and stabilize with a minimum of 8 percent hydrated lime (by dry weight). The stabilized soils should be compacted to 95 percent of their ASTM D 1557 (Modified Proctor) dry density at a moisture content ranging from optimum to 3 percent above optimum. Lime stabilization shall be performed in accordance with Items P-155 of the FAA AC 150/5370-10G Airport Construction Standards.

5.1.3 Potential Vertical Rise (PVR)

As required by Atkins, AEC estimated the Potential Vertical Rise (PVR) of soils within the proposed paved areas. However, it is AEC's experience with similar HAS projects that excavation of existing soil for PVR mitigation is not typically performed for taxiway projects. AEC should be notified if PVR mitigation is required, so that our recommendations can be updated as necessary.



<u>Estimated Soil Movements</u>: PVR is an estimate of the potential of an expansive soil to swell from its current state. Expansive clays exhibit a potential to shrink and swell with changes in their moisture contents. The changes in the soil moisture content are usually caused by variations in the seasonal amount of rainfall and evaporation rates or other localized factors like the moisture withdrawal by nearby trees. AEC determined PVR within the zone of seasonal moisture variation, which is typically considered to be 10 feet deep in the Greater Houston area.

PVR was computed for selected borings using TxDOT test method Tex-124-E. PVR results based on in-situ moisture contents are presented on Table 10. As a reference, the TxDOT 2019 Pavement Design manual requires a maximum allowable PVR of 2.0 inches for highway main lanes.

Boring	PVR (in), based on in-situ moisture conditions	
B-1	4.03	
B-6	1.55	
B-11	4.72	
B-17	3.03	
B-22	2.90	
B-26	2.12	
B-33	3.21	
B-37	2.23	
B-41	1.64	
B-47	3.46	
B-50	3.44	
B-56	2.11	
B-64	3.26	
B-67	2.22	
B-74	2.81	

Table 10. Estimated PVR

<u>PVR Mitigation</u>: Based on Table 10, the PVR exceeds 2 inches in Borings B-1, B-11, B-17, B-22, B-26, B-33, B-37, B-47, B-50, B-56, B-64, B-67, and B-74. If HAS decides to reduce the PVR to at least 2 inches, the top 24 inches of highly expansive clay soils along the project alignments should be excavated and either replaced with lean clay soil with low plasticity, or by stabilizing the excavated clay soil with at least 8 percent hydrated lime and then compacting it back in place. If PVR mitigation is performed, the lime-stabilized subgrade recommendations presented in Section 5.1.2 of this report are not required. Compacted soil (whether



embankment fill imported from offsite, or existing onsite soil stabilized with lime) should be placed in accordance with Section 3.4.1 (Ordinary Compaction) of Item 132 of the 2014 TxDOT Standard Specifications. Other methods for reducing PVR, such as horizontal or vertical moisture barriers, geo-synthetic reinforcement, subgrade drainage, etc. can also be considered, if allowed by HAS. However, as noted above, it is AEC's opinion that the PVR mitigation strategies presented above would be cost-excessive and ultimately unnecessary for this category of taxiway project. However, the decision to include PVR mitigation should ultimately be decided by HAS.

6.0 <u>CONSTRUCTION CONSIDERATIONS</u>

6.1 Site Preparation and Grading

To mitigate site problems that may develop following prolonged periods of rainfall, it is essential to have adequate drainage to maintain a relatively dry and firm surface prior to starting any work at the site. Adequate drainage should be maintained throughout the construction period. Methods for controlling surface runoff and ponding include proper site grading, berm construction around exposed areas, and installation of sump pits with pumps.

<u>Pumping Soils:</u> AEC notes that silty sand (SM) fill material was encountered at the ground surface in the vicinity of Boring B-71. Silty soils are prone to pumping when they are saturated after rainfall. Pumping soils are not able to support construction equipment. If rainfall occurs and pumping soils are encountered at the ground surface, methods to mitigate the effect of the pumping soils include: (i) providing positive drainage around the pumping soils area, including cutting drainage swales as necessary; (ii) excavate and replace the pumping soils with competent, compacted clay fill that is free from debris or other deleterious materials; (iii) adding lime or fly ash to the pumping soils in order to dry out the soil, as well as increase soil strength; (iv) using woven geotextiles (such as a Mirafi RS series, or equivalent) to reinforce and separate weak/wet underlying soil layers; or (v) a combination of the above methods.

6.2 Construction Monitoring

Site preparation (including clearing and proof-rolling) and earthwork operations should be monitored by qualified geotechnical professionals to check for compliance with project documents and changed conditions, if encountered.



7.0 <u>GENERAL</u>

The information contained in this report summarizes conditions found on the date the borings were drilled. The attached boring log is a true representation of the soils encountered at the specific boring location on the date of drilling. Reasonable variations from the subsurface information presented in this report should be anticipated. AEC should be notified immediately when conditions encountered during construction are significantly different from those presented in this report.

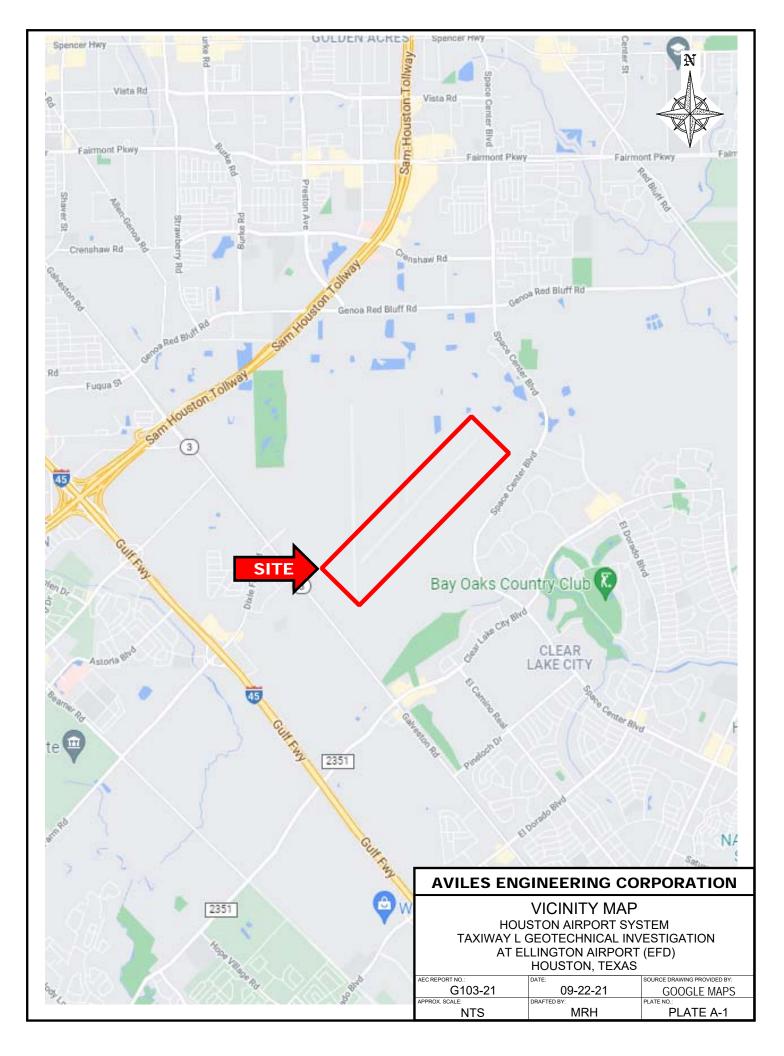
8.0 **LIMITATIONS**

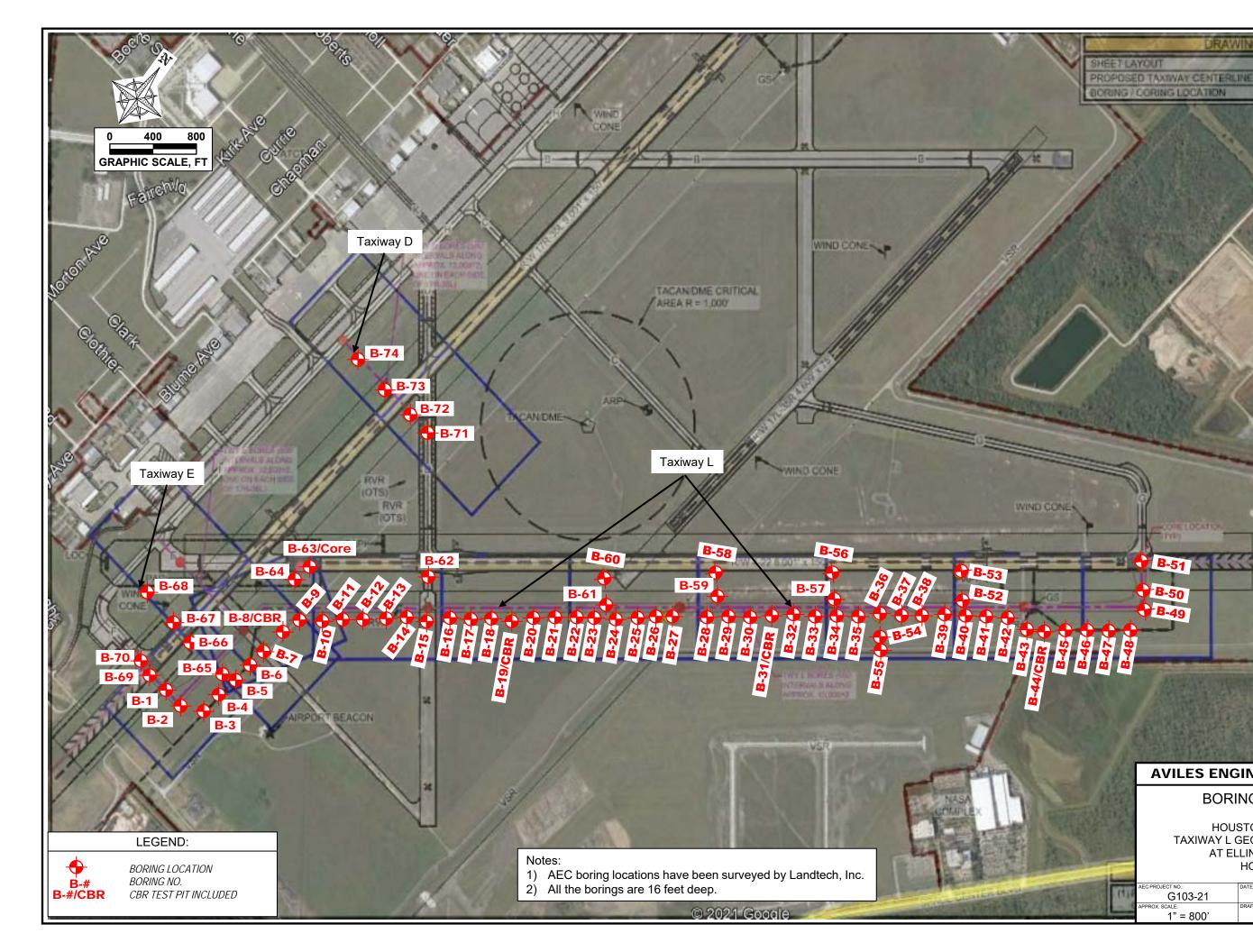
The investigation was performed using the standard level of care and diligence normally practiced by recognized geotechnical engineering firms in this area, presently performing similar services under similar circumstances. The report has been prepared exclusively for the project and location described in this report and is intended to be used in its entirety. If pertinent project details change or otherwise differ from those described herein, AEC should be notified immediately and retained to evaluate the effect of the changes on the recommendations presented in this report and revise the recommendations if necessary. The scope of services does not include a fault investigation. The recommendations presented in this report should not be used for other structures located at other sites, without additional evaluation and/or investigation.



APPENDIX A

Plate A-1	Vicinity Map
Plate A-2	Boring Location Plan
Plates A-3 to A-76	Boring Logs
Plate A-77	Key to Symbols
Plate A-78	Classification of Soils for Engineering Purposes
Plate A-79	Terms Used on Boring Logs
Plate A-80	ASTM & TXDOT Designation for Soil Laboratory Tests
Plate A-81	Sieve Analysis Results
Plates A-82 and A-83	Organic Content Test Results







B-50

B-49

BORING LOCATION PLAN

HOUSTON AIRPORT SYSTEM TAXIWAY L GEOTECHNICAL INVESTIGATION AT ELLINGTON AIRPORT (EFD) HOUSTON, TEXAS

	AEC PROJECT NO .:	DATE:	SOURCE DRAWING PROVIDED BY:
174	G103-21	9-23-2021	ATKINS/GOOGLE
- 16	APPROX. SCALE:	DRAFTED BY:	PLATE NO.:
	1" = 800'	MRH	PLATE A-2



ENGINEERING CORP. BORING

DA	ATE 8	8/17/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Locat	ion I	Plar	<u> </u>	
		DESCRIPTION		Γ, %		SHEAR STRENGTH, TSF				
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
0		Fill: very stiff to hard, dark gray and dark brown Fat Clay (CH), with calcareous nodules -with roots 0'-2'		16			96	88	25	63
	$\not>$	-gray and dark gray, with ferrous nodules 2'-4' Firm to stiff, gray Fat Clay (CH), with		37			30		20	00
- 5 -		slickensides and ferrous nodules -grayish tan, with calcareous nodules 6'-8'		38	81.9					
		Stiff to very stiff, tan and gray Lean Clay (CL),		40			00	40	16	22
- 10 -		with fat clay seams 8'-10'		29			98	49	16	33
		Stiff to very stiff, tan and gray Fat Clay (CH),		24	101.6					
		with slickensides, calcareous nodules, and lean clay seams -tan 14'-16'		22						
- 15 -		Termination Depth = 16 feet		27						
- 20 -										
- 25 -										
- 30 -										
- 35 -										
F		IG DRILLED TO 16 FEET WITHOUT DF	 2		 = r	<u> </u>				
		R ENCOUNTERED AT N/A FEET WHILE								
		R LEVEL AT N/A FEET AFTER COMPLI	ETE							
	JRILL	ED BY JH Drilling DRAFTED BY		MF	KH	LOGGED BY	JH			



ENGINEERING CORP. BORING

G **B-2**

D/	ATE <u>8</u>	/4/2021 TYPE 4" Dry Auger			LOC	CATION See Boring Locat	ion I	Plar	<u>۱</u>	
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3187859.09	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer 	ESH	LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
	SYMBOL	Northing: 13783422.56 Elevation: 22.68	S.P.T. I	MOIST	DRY DI	$\Box \text{Torvane} \\ 0.5 1 1.5 2 \\ \hline$	-200 MESH	LIQUID LIMIT	PLAST	PLAST
0		Soft to very stiff, dark gray Fat Clay (CH), with slickensides -with roots 0'-2' -gray 2'-6', with calcareous nodules 2'-4'		29 39	80.9		95	72	24	48
- 5 -		-with ferrous nodules 4'-8' -tan and gray, with abundant calcareous	3	44			-			
		Firm to stiff, tan Lean Clay (CL), with fat clay		23						
- 10 -		pockets Firm to very stiff, tan Fat Clay (CH), with	8	21 26	97.8		98	38	16	22
		slickensides and calcareous nodules -with silty clay seams 10'-14' -tan and gray 12'-16'	Ŧ	37	97.0		-			
- 15 -			11	29			-			
		Termination Depth = 16 feet								
- 20 -										
- 25 -							-			
							-			
- 30 -										
- 35 -										
F		G DRILLED TO 16 FEET WITHOUT DF	 		 =1 1 117					
\	NATEF	R ENCOUNTERED AT <u>12</u> FEET WHILE	E DR							
		R LEVEL AT <u>12</u> FEET AFTER <u>COMPL</u> D BY <u>JH Drilling</u> DRAFTED BY	ETE	MF	RH	LOGGED BY	DN			
L										



ENGINEERING CORP. GEOTECHNICAL ENGINEERS BORING

DA	ATE <u>8</u>	/4/2021 TYPE 4" Dry Auger	LOCATION See Boring Location Plan							
		DESCRIPTION		NT, %		SHEAR STRENGTH, TSF				
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3188038.56 Northing: 13783566.78 Elevation: 22.35	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
0		Fill: very stiff, dark gray and gray Fat Clay (CH), with roots and shell fragments		28			95	69	23	46
		Firm to very stiff, gray Fat Clay (CH), with slickensides		35	85.2	•	-			
- 5 -				37		4				
		-gray and tan, with calcareous nodules 6'-8' and ferrous nodules 6'-10'		36			96	86	25	61
- 10 -		-reddish tan and gray 8'-10', with lean clay seams 8'-12'		29	97.3					
		-tan and gray, with calcareous nodules 10'-16'		23						
		_		29			_			
- 15 -		2	Z	27			-			
		Termination Depth = 16 feet					-			
- 20 -							-			
							-			
							-			
- 25 -							-			
							-			
- 30 -										
- 35 -										
V	VATE	G DRILLED TO <u>16</u> FEET WITHOUT DR R ENCOUNTERED AT <u>15</u> FEET WHILE	E DR	ILLI						
		R LEVEL AT <u>14</u> FEET AFTER <u>COMPLI</u> D BY JH Drilling DRAFTED BY			IRH	LOGGED BY	DN			
							PLA	тс	A 6	



ENGINEERING CORP. GEOTECHNICAL ENGINEERS BORING

DA	ATE <u>8</u>	/5/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Locat	ion l	Plan	<u> </u>	
		DESCRIPTION		Т, %		SHEAR STRENGTH, TSF				
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3188032.25 Northing: 13783767.15 Elevation: 22.64	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
0		Firm to hard, dark brownish gray Fat Clay (CH), with slickensides -with roots 0'-2' and ferrous nodules 0'-10' -tannish gray 2'-4', with calcareous nodules 2'-6		23 36	85.5		96	73	22	51
- 5 -		-gray and tan 4'-8'	6	35			-			
		-reddish tan 8'-10', with calcareous nodules 8'- 16'	11	29 21	97.2		96	53	17	36
- 10 -		-tan 10'-12'		20			-			
		-reddish tan 12'-16', with lean clay seams 12'- 14'	-	22	107.6		-			
- 15 -		-with silt seams 14'-16'	₹ 8	24						
		Termination Depth = 16 feet					-			
- 20 -										
							-			
- 25 -							-			
- 30 -							-			
							-			
- 35 -							-			
l V	NATE	G DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT <u>15</u> FEET WHILI R EVEL AT <u>12</u> FEET AFTER COMPL	E DR				<u>. </u>	1	<u> </u>	L
		R LEVEL AT <u>13</u> FEET AFTER <u>COMPL</u> ED BY <u>JH Drilling</u> DRAFTED BY _			IRH	LOGGED BY	DN			
PF		Г NO. G103-21					PLA [.]	TF	Δ-6	



ENGINEERING CORP. BORING

DATI	ATE <u>8/5/2021</u> TYPE <u>4" Dry Auger</u>				LOCATION See Boring Location Plan							
DEPTH IN FEET SYMBOI	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3188025.19 Northing: 13783960.47 Elevation: 17.12	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH		PLASTICITY INDEX				
0	 Fill: very stiff, tannish gray and dark gray Fat Clay (CH), with calcareous and ferrous nodules Stiff to very stiff, gray and dark gray Fat Clay (CH), with slickensides and ferrous nodules -dark and olive gray 4'-6' -gray and tan 6'-8' 	-	31 32 33 35	89.1		92 8	4 24	60				
- 10 -	Very stiff to hard, tan and gray Lean Clay (CL), with fat clay seams and pockets -reddish tan and tan, with calcareous nodules 10'-12' -with calcareous nodules and silt pockets 14'- 16'	-	20 24 22 22	104.0		97 4	4 15	29				
- 20 -	Termination Depth = 16 feet											
- 25 -												
- 30 -												
WA WA	ORING DRILLED TO <u>16</u> FEET WITHOUT DF ATER ENCOUNTERED AT <u>N/A</u> FEET WHILE ATER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u> RILLED BY <u>JH Drilling</u> DRAFTED BY	E DR ETE		NG -		DN	·					



ENGINEERING CORP. BORING

DATE	7/1/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Locat	ion F	Plan		
DEPTH IN FEET SYMBOL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3188019.81 Northing: 13784137.34 Elevation: 24.15	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
	 Fill: stiff, gray Fat Clay (CH), with sandy lean clay seams, shell fragments, and roots Soft to very stiff, gray and tannish gray Fat Clay (CH), with slickensides -with ferrous nodules 2'-4' and calcareous nodules 2'-8' -tan and gray 6'-14', with ferrous stains 6'-8' -with calcareous nodules 10'-12' Very stiff, tan and gray Lean Clay (CL), with calcareous nodules, silty clay seams, and fat clay pockets Termination Depth = 16 feet 		2 39 41 39 32 32 32 28 36 19	93.7		93	56	21	39 39
- 35 -									
WAT WAT	ING DRILLED TO <u>16</u> FEET WITHOUT DF ER ENCOUNTERED AT <u>14</u> FEET WHILE ER LEVEL AT <u>13</u> FEET AFTER <u>COMPL</u> LED BY JH Drilling DRAFTED BY	E DR	XILLII ₹			DN			
			-			-			



8-7

PLASTICITY INDEX PLASTIC LIMIT

21 53

23 57

DATE	7/1/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location	Plan
DEPTH IN FEET SYMBOL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3188011.52 Northing: 13784336.88 Elevation: 24.86	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2	LIQUID LIMIT
	 <i>Elevation:</i> 24.86 Pavement: 6.5" concrete Fill: stiff to very stiff, gray and dark gray Fat Clay with Sand (CH), with silty sand seams and ferrous nodules Firm to very stiff, dark gray Fat Clay with Sand (CH) -with ferrous nodules 2'-4' -gray 4'-6', with calcareous nodules 4'-8' -tan and gray 6'-10', with ferrous nodules 6'-8' Stiff to very stiff, brown and gray Lean Clay (CL), with ferrous nodules 12'-14' Stiff to very stiff, brown Fat Clay (CH), with calcareous nodules Termination Depth = 16 feet 	<i>о</i> і 8 9 11	∑ 17 34 31 34 35 23 21 20	87.2		 74 80
25 - 30 - 35 - BOR WAT	NG DRILLED TO <u>16</u> FEET WITHOUT DR ER ENCOUNTERED AT <u>N/A</u> FEET WHILE ER LEVEL AT N/A FEET AFTER COMPLE	DRI				



ENGINEERING CORP. BORING

B-8

DA	DATE <u>7/1/2021</u> TYPE <u>4" Dry Auger</u>					CATION See Boring Location Plan
		DESCRIPTION		% '		SHEAR STRENGTH, TSF
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL		S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2
0		Firm to very stiff, gray Fat Clay (CH), with				
		slickensides -with roots 0'-2' and ferrous nodules 0'-10'		39 37	83.3	
- 5 -		-tan and gray 4'-12', with calcareous nodules 4'- 10'	7	36		92 88 25 63
			10	35 33	90.4	
- 10 -			10	29		99 54 19 35
		-brown and gray 12'-16', with ferrous nodules 12'-14' and calcareous nodules 12'-16'		23	105.1	
- 15 -		Termination Depth = 16 feet	11	24		
- 20 -						
- 25 -						
- 30 -						
- 35 -						
٧	VATE	IG DRILLED TO <u>16</u> FEET WITHOUT DR R ENCOUNTERED AT <u>N/A</u> FEET WHILE R LEVEL AT 14 FEET AFTER COMPLE	E DR	ILLI		
		ED BY JH Drilling DRAFTED BY		Y	Y	LOGGED BY DN
PF		T NO. G103-21				PLATE A-10

PROJECT: EFD Taxiway L Geotechnical Investigation



ENGINEERING CORP. BC

DAT	DATE 7/1/2021 TYPE 4" Dry Auger LOCATION See Boring Location Plan								
	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3188046.14 Northing: 13784766.46 Elevation: 23.64	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
0 5 10 10 115 20 20 20 30 30 30 30 30 31	Firm to very stiff, dark gray Fat Clay (CH), with slickensides -with roots 0'-2' -with ferrous nodules 2'-10' -gray and tannish gray 4'-6' -tan and gray 6'-12' -tan 12'-14', with calcareous nodules and ferrous stains 12'-16' -brown and gray 14'-16' Termination Depth = 16 feet		29 33 31 34 24 23 22	90.2		86	69		48
WA WA	DRING DRILLED TO <u>16</u> FEET WITHOUT DR ATER ENCOUNTERED AT <u>N/A</u> FEET WHILE ATER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLE</u> RILLED BY <u>JH Drilling</u> DRAFTED BY	E DR		NG -		DN			



ENGINEERING CORP. BO

DA	ATE <u>8</u> /	'3/2021 TYPE 4" Dry Auger			LOC	CATION See Boring Loca	tion	Plar	<u> </u>	
		DESCRIPTION		Т, %		SHEAR STRENGTH, TSF				
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3188178.70 Northing: 13784911.62 Elevation: 23.85	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
0		Soft to very stiff, gray Fat Clay (CH)		33			95	87	22	65
		-with ferrous nodules 2'-8'	7	37	83.9	••••				
- 5 -		-tan and gray 6'-8', with calcareous nodules 6'- 10'	2	43 33	86.9		-			
		-brown and gray 8'-10'	8	41			98	79	25	54
- 10 -		Stiff to very stiff, tan and gray Lean Clay (CL) -with fat clay pockets 10'-12'		21						
		-brown and gray, with ferrous stains 12'-14' and calcareous nodules 12'-16'		22						
- 15 -		-light brown 14'-16'	10	24						
		Termination Depth = 16 feet *: groundwater is likely perched								
- 20 -										
- 25 -										
							-			
- 30 -										
- 35 -							-			
							1	1	<u> </u>	
V	VATEF	R ENCOUNTERED AT <u>4*</u> FEET WHILE R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLI</u>	ETE	Ţ						
		D BY <u>JH Drilling</u> DRAFTED BY		YY/N	IRH	LOGGED BY	DN PLA			



ENGINEERING CORP. GEOTECHNICAL ENGINEERS BORING B-11

DATE 6	5/21/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location PI	an
	DESCRIPTION		г, %		SHEAR STRENGTH, TSF	
DEPTH IN FEET SYMBOL SAMPLE INTERVAL	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	PLASTIC LIMIT PLASTIC LIMIT PLASTICITY INDEX
0	Firm to very stiff, dark gray Fat Clay (CH), with slickensides -with roots 0'-2' -gray 2'-4', with ferrous nodules 2'-6' -grayish tan 4'-6', with calcareous nodules 4'-10' -tan and light gray 6'-8'		35 40 38 34	83.7	94	0 24 66
10	-tan and gray 8'-10'	V	26		96 7	3 24 49
- 15 -	Stiff to hard, tan and gray Lean Clay (CL) -reddish brown and gray, with fat clay pockets 12'-14' -reddish tan and gray, with silty clay and silty sand seams, and calcareous nodules 14'-16'	Z	20 21 22	105.9		3 15 28
	Termination Depth = 16 feet					
- 20 -						
- 25 -						
- 30 -						
- 35 -						
WATE	G DRILLED TO <u>16</u> FEET WITHOUT DR R ENCOUNTERED AT <u>14</u> FEET WHILE	E DR	ILLI			
	R LEVEL AT <u>10</u> FEET AFTER <u>COMPLI</u> ED BY <u>JH Drilling</u> DRAFTED BY			IRH	LOGGED BY	

PROJECT: EFD Taxiway L Geotechnical Investigation



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

DATE	DATE 6/21/2021 TYPE 4" Dry Auger LOCATION See Boring Location Plan						
DEPTH IN FEET SYMBOL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3188442.08 Northing: 13785200.94 Elevation: 24.02	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane ○ 5 1 15 2	PLASTICITY INDEX	
	 <i>Elevation: 24.02</i> Firm to very stiff, dark brown Fat Clay (CH), with slickensides -with roots 0'-2' -gray and dark gray 2'-6' -with ferrous nodules 4'-10' -tan and gray 6'-16', with calcareous nodules 6'- 10' -with ferrous nodules 12'-14' and calcareous nodules 12'-16' 	5	33 37 37 33 33 35 30 25	93.8	96 79 2 •	1 52	
20 - 22 - 22 - 22 - 22 - 22 - 22 - 22 -	Termination Depth = 16 feet	14	24				
WAT	NG DRILLED TO <u>16</u> FEET WITHOUT DR ER ENCOUNTERED AT <u>N/A</u> FEET WHILE ER LEVEL AT N/A FEET AFTER COMPLE	E DR					
	LED BYJH Drilling DRAFTED BY		Y	Y	LOGGED BY	_	



ENGINEERING CORP. BORING

RING <u>**B-13**</u>

DA	ATE	6/21/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Locat	tion Pla	n	
DEPTH IN FEET	SYMBOL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3188580.17 Northing: 13785353.95 Elevation: 23.97	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	PLASTIC LIMIT	PLASTICITY INDEX
- 5 -		Stiff to very stiff, dark brown Fat Clay (CH), with slickensides -with roots 0'-2' and ferrous nodules 0'-4' -dark gray 2'-4' -gray 4'-6' -tan and gray 6'-14', with ferrous nodules 6'-12'		28 28 30 27 30	93.4		95 70) 18	52
- 10 -		-with calcareous nodules 10'-16' -tan 14'-16'		23 23 23 23	93.0		93 55	5 17	38
- 20 - - 20 - - 25 - - 30 - - 35 -	3ORI	Termination Depth = 16 feet		NGF					
	NATI NATI	NG DRILLED TO <u>16</u> FEET WITHOUT DF ER ENCOUNTERED AT <u>N/A</u> FEET WHILE ER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLI</u> LED BY JH Drilling DRAFTED BY	E DR	RILLIN E	NG -	$\sum_{i=1}^{n}$			
		_ED BY <u>JH Drilling</u> DRAFTED BY CT NO. G103-21		Y	T	LOGGED BY	DN PLATE		



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

DA	DATE 6/21/2021 TYPE 4" Dry Auger LOCATION See Boring Location Plan UNIT DESCRIPTION DESCRIPTION H-1/SMOTH H-1/SMOTH SHEAR STRENGTH, TSF I							
PTH IN FEET	MBOL MPLE INTERVAL		.T. BLOWS / FT.	ISTURE CONTENT, %	Y DENSITY, PCF			
	SY SA		S.F	ω	DR			
- 5 		with calcareous nodules and roots Firm to hard, gray Fat Clay (CH), with slickensides	6		86.2	85 63 21 4 85 63 21 4 99 75 25 5		
25 -								
35 -								
W	/ATE	G DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT <u>N/A</u> FEET WHILE R LEVEL AT N/A FEET AFTER COMPL I	E DR					
		ED BY JH Drilling DRAFTED BY		Y	Y	LOGGED BY DN		



ENGINEERING CORP. BORING

IG <u>B-15</u>

D	ATE 7/1/202	1 TYPE	4" Dry Auger				EOTECHN				g Lo	cat	ion l	Plar	1	
DEPTH IN FEET	Tex. Eas Non SAMPLE INTE Non Elev	DESCRII D Coordinates (US as State Plane Zone ting: 3188846.78 thing: 13785649.4 ration: 26.53	Survey ft): :: 4204	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	△ (● (○ F	Confin Jncon Pocke Forvar	ed Co fined t Peno	ompre Com	essior press	ı	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
0	Fill: s		gray Lean Clay (CL),		28			0					89	46	19	27
	Firm	sandy lean clay poo to very stiff, dark g ensides	ray Fat Clay (CH), with		28	92.1										
- 5 -					28				$\left \right\rangle$							
					30											
		and gray 8'-10', with us nodules 8'-12'	n calcareous and		30								93	68	20	48
- 10 -	-brow	n and dark gray 10)'-12'		32	90.8		-8-								
	-tan a 14'	and dark gray, with	lean clay seams 12'-		31			HĄ								
- 15 -	Stiff t	o very stiff, tan and	l gray Lean Clay (CL)		21				$\frac{1}{2}$							
- 20 -	Term	ination Depth = 16	feet													
			FEET WITHOUT DR					<u>++++</u>			<u>++++</u>	<u>+++</u>				<u> </u>
۱	WATER LEV	ELAT <u>N/A</u> FE	ET AFTER COMPLI	ETE	Ţ			LOG	GED) BY	,		DN			



ENGINEERING CORP. BORING

G **B-16**

DATE 8/3/2021 TYPE 4" Dry Auger LOCATION See Boring Location Plan							
				%		SHEAR STRENGTH, TSF	
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3188978.40 Northing: 13785797.47 Elevation: 25.42	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	
0		Soft to hard, dark brown Fat Clay (CH) -with ferrous nodules and roots 0'-2' -light tan and tan, with lean clay seams 2'-4' and calcareous nodules 2'-6' -gray and grayish tan, with ferrous nodules 4'-6' -reddish tan and light gray 6'-8'	¥	18 25 27 33	99.6	86 50 17 33	
10 -		-tan and gray 8'-10' Stiff to very stiff, tan and gray Lean Clay (CL) -with silty sand pockets and partings 10'-12' -tan, with calcareous nodules, ferrous stains, and fat clay pockets 12'-14'	7	38 23 24	102.7	98 49 18 31	
20 -		Hard, tan Silty Clay (CL-ML), with silt seams Termination Depth = 16 feet	12	11			
		G DRILLED TO <u>16</u> FEET WITHOUT DE R ENCOUNTERED AT 4.2 FEET WHILI					
V	VATEF	R LEVEL AT 6.3 FEET AFTER COMPL	ETE			LOGGED BY DN	
PR							



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

DATE <u>8/3/2021</u> TYPE <u>4" Dry Auger</u> LOCATION <u>See Boring Location Plan</u>								
DESCRIPTION		, %		SHEAR STRENGTH, TSF				
GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3189107.23 Northing: 13785943.43 GElevation: 26.76	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 × and the second sec				
0 Stiff to very stiff, brownish gray Fat Clay (CH), with calcareous nodules -with ferrous nodules and roots 0'-2' -gray and dark gray 2'-4' -tannish gray and gray 4'-6', with ferrous nodules 4'-10' -tan and gray 6'-8' -reddish tan and gray 8'-10' 10 Stiff to very stiff, tan and gray Lean Clay (CL), with slickensides -red and gray, with fat clay pockets 12'-14' 15 20 30 30		27 29 27 22 32 23 24 21	96.4	91 66 19 47				
BORING DRILLED TO 16 FEET WITHOUT D	RILLI	NG I						
WATER ENCOUNTERED AT <u>N/A</u> FEET WHIL	E DR	ILLI						
WATER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u>								
DRILLED BY DRAFTED BY		YY/N	IRH	LOGGED BY DN				



ENGINEERING CORP. BORING

NG <u>**B-18**</u>

D	ATE <u>8</u>	/3/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location	Plar	<u>ו</u>	
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3189237.78	P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
	SYMBOL	Northing: 13786090.78 Elevation: 27.16	S.P.T.	MOIS	DRY I	□ Torvane 5 0.5 1 1.5 2	LIQUI	PLAS	PLAS
0		Firm to hard, dark brown Fat Clay (CH), with slickensides -with roots 0'-2' -dark gray 2'-4'		23 27	94.9	93	3 55	18	37
- 5 -		-gray 4'-6', with ferrous nodules 4'-8'	7	27					
		-red and gray 6'-8', with calcareous nodules and pockets 6'-12'		20					
- 10 -		-reddish brown and gray 8'-10' -tan and gray 10'-16', with ferrous nodules 10'-	11	30		97	7 63	20	43
		12'		32	91.1				
- 15 -		Ζ	z	23					
		Termination Depth = 16 feet	₩ 9	22					
- 20 -									
- 25 -									
- 30 -									
- 35 -									
۱	NATEF	R ENCOUNTERED AT <u>15</u> FEET WHILE R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u> I ED BY JH Drilling DRAFTED BY	ETE			₩ LOGGED BY DI	J		
				1 1/1			•		



ENGINEERING CORP. BORING

G **B-19**

DATE	E 8/3/2021 TYPE 4" Dry Auger			LOC	CATION See Boring Locat	ion	Plar	<u> </u>	
DEPTH IN FEET SYMBOL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3189368.77 Northing: 13786238.83 Elevation: 27.62	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
	Firm to hard, dark brown Fat Clay with Sand (CH) -with roots 0'-2' -gray, with ferrous and calcareous nodules 2'-6' Stiff to hard, tan and gray Fat Clay (CH), with slickensides -with ferrous nodules 6'-8', and calcareous nodules and pockets 6'-10' -reddish tan and gray 8'-10' -brown and gray 10'-12', with ferrous stains 10'- 16' -reddish tan 12'-14', with calcareous nodules 12'-16' -brown 14'-16' Termination Depth = 16 feet		19 26 22 19 30 24 22 21	95.6		95	54	16	38 36
	RING DRILLED TO <u>16</u> FEET WITHOUT DR					1			
WA	NTER ENCOUNTERED AT <u>N/A</u> FEET WHILE NTER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLE</u>			NG 🗎					
DR	ILLED BY JH Drilling DRAFTED BY		YY/N	IRH	LOGGED BY	DN			



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

D	ATE .	8/3/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Loc	ation I	Plan	<u> </u>
FEET		DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204	WS / FT.	MOISTURE CONTENT, %	DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compressio	n –	ΛΙΤ	IMIT Y INDEX
DEPTH IN FEET	SYMBOL	Easting: 3189495.76 Northing: 13786382.46 Elevation: 27.49	S.P.T. BLOWS / FT.	MOISTURE	DRY DENS	 Pocket Penetrometer Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT PLASTICITY INDEX
0		Firm to hard, dark gray Fat Clay (CH) -with roots 0'-2' -gray 2'-6', with calcareous nodules 2'-10'		26					
- 5 -		X	6	33 29	87.6		86	68	19 49
		-reddish tan 6'-10', with ferrous stains 6'-8'	Ū	23					
- 10 -		-brown and gray 10'-16', with ferrous stains 10'-	11	29	100 5				
		12' -with calcareous nodules and pockets 12'-16'		24 24	103.8		100	51	20 31
- 15 -			15	20					
		Termination Depth = 16 feet							
- 20 -									
- 25 -									
- 30 -									
- 35 -									
F	30RII	 NG DRILLED TO 16 FEET WITHOUT DF	 	NG F	-LUIF	$\begin{array}{c} \left + + + + + + + + + + + + + + + + + + $			
۱ <i>۱</i>	NATE	ER ENCOUNTERED AT <u>N/A</u> FEET WHILE	E DR	ILLI					
		ER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u> .ED BY JH Drilling DRAFTED BY		Ţ ¥¥/N	IRH	LOGGED BY	DN		
							PLA	TE	



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

DATE	DATE 8/2/2021 TYPE 4" Dry Auger LOCATION See Boring Location Plan							
DEPTH IN FEET SYMBOL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3189626.79 Northing: 13786530.17 Elevation: 27.49	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT PLASTIC LIMIT	PLASTICITY INDEX
0	 Hard, dark brown Lean Clay (CL), with roots Stiff, dark gray Fat Clay (CH) -gray and dark gray, with ferrous nodules 4'-6' Very stiff, gray and tan Fat Clay with Sand (CH) with lean clay seams, and calcareous and ferrous nodules Very stiff, reddish tan and gray Fat Clay (CH), with slickensides and calcareous nodules Firm to very stiff, light gray and tan Lean Clay 		22 29 27 22 32	97.3		85	61 17 36 15	44
- 15 -	<pre>(CL), with fat clay seams and pockets -with sand pockets 10'-12' -with silty clay seams and calcareous nodules 12'-14' -tan and gray 14'-16' Termination Depth = 16 feet</pre>	25	30 22 26	102.3				
WA ⁻ WA ⁻ DRII	RING DRILLED TO <u>16</u> FEET WITHOUT DI TER ENCOUNTERED AT <u>N/A</u> FEET WHIL TER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u> LED BY <u>JH Drilling</u> DRAFTED BY ECT NO. G103-21	E DR ETE		NG 🛓		DN		



ENGINEERING CORP. BORING B-22

D/	ATE 3	3/2/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Loca	tion P	Plan	-
I FEET	NTEDVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204	.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression	т	MIT	PLASTICITY INDEX
DEPTH IN FEET	SYMBOL SAMPLE NITEDV		S.P.T. BL	MOISTUR	DRY DEN	 Pocket Penetrometer Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTICI
0		Stiff to very stiff, dark gray Fat Clay (CH) -with shell fragments 0'-2' and roots 0'-4' -gray 2'-6'		22 26		·····	91	65 18	3 47
- 5 -			9	20			-		
		-reddish tan and gray, with calcareous nodules and pockets 6'-8' Firm to stiff, tan and gray Lean Clay (CL)		29	96.0	← · · · · · · · · · · · · · · · · · · ·	-		
- 10 -		-with fat clay seams 10'-12'	1 1 ¥	20 22	104.4		90	30 17	7 13
		Tan and gray Silt (ML), with sand pockets and lean clay seams, wet Medium dense, tan and gray Silty Clayey Sand	-	22			-		
- 15 -		(SC-SM), with lean clay pockets and calcareous nodules, wet Termination Depth = 16 feet	11	23			• - -		
- 20 -							-		
							-		
- 25 -									
							-		
- 30 -							-		
		IG DRILLED TO <u>16</u> FEET WITHOUT DR R ENCOUNTERED AT 10 FEET WHIL							
V	VATE	R LEVEL AT <u>7.9</u> FEET AFTER <u>15 MII</u> ED BY JH Drilling DRAFTED BY	IS			₩ LOGGED BY	DN		
		CT NO. G103-21		11/1				E A-	 24



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

DA	ATE <u>8</u>	X/2/2021 TYPE 4" Dry Auger			LOC	CATION See Boring Loca	tion	Plar	<u> </u>	
		DESCRIPTION		, %		SHEAR STRENGTH, TSF				\square
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	CRID Coordinates (IIS Survey fi);	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
0	\bigotimes	Base:12" stabilized sand with shells		6						
- 5 -		<no 1'-2'="" recovery=""> Stiff to very stiff, dark gray Fat Clay (CH), with slickensides -with ferrous nodules 2'-8' -gray 4'-6'</no>		26 24	99.2	•••••	90	62	18	44
		-tan and gray 6'-8', with calcareous nodules 6'- 10'		23						
		-reddish tan and gray 8'-10'		33	94.3					
- 10 -		Stiff to very stiff, tan and gray Lean Clay (CL) -with fat clay seams 10'-12'		20			90	33	14	19
		-with silty clay seams and ferrous stains 12'-14'	-	23						
- 15 -		Stiff to very stiff, reddish tan and gray Silty Clay (CL-ML), with sandy lean clay pockets	F	21						
		Termination Depth = 16 feet					-			
- 20 -										
- 25 -										
- 30 -										
- 35 -										
F	L L 30RIN	G DRILLED TO 16 FEET WITHOUT DF	l RILLT	l Ng f	 -LUII	+++++++++++++++++++++++++++++++++++++	Η			Ц
۱ V	NATEI	R ENCOUNTERED AT <u>14</u> FEET WHILE	E DR							
		R LEVEL AT <u>7.1</u> FEET AFTER <u>15 MIN</u> ED BY JH Drilling DRAFTED BY			IRH	LOGGED BY	DN			
		T NO. G103-21		/ //			PLA	TF	Δ-2	



ENGINEERING CORP. GEOTECHNICAL ENGINEERS BORING

DATE 8/2/2021 TYPE 4" Dry Auger LOCATION See Boring Locati							tion P	' lan	
		DESCRIPTION		т, %		SHEAR STRENGTH, TSF			
DEPTH IN FEET	SYMBOL	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3190019.68 Northing: 13786974.37 Elevation: 27.73	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT PLASTICITY INDEX
0	\square	Firm to very stiff, gray and dark brown Fat Clay (CH), with slickensides		23	95.9				
		-with sandy lean clay seams and roots 0'-2' -gray 2'-4', with ferrous nodules 2'-8'		21		·····	88	55	15 40
- 5 -		-tan 4'-6', with calcareous nodules 4'-14'	7	24					
		-reddish brown and gray, with calcareous pockets 6'-8'	V	26	99.5		-		
		-reddish tan and gray 8'-10'	10	26					
- 10 -		-tan and gray 10'-14', with calcareous pockets 10'-12'		27			97	61	20 41
		-with lean clay with sand seams 12'-14'		27			_ -		
- 15 -		Medium dense, reddish tan Silt (ML), with silty clay seams, wet	- ¥ 11	23					
		Termination Depth = 16 feet							
- 20 -									
- 25 -									
- 30 -									
							-		
							-		
- 35 -							- -		
		NG DRILLED TO <u>16</u> FEET WITHOUT DE ER ENCOUNTERED AT 15 FEET WHILI					<u> </u>	1	
۱	VATE	ER LEVEL AT <u>7.7</u> FEET AFTER <u>15 MIN</u> ED BY JH Drilling DRAFTED BY	IS			LOGGED BY	DN		
		CT NO. G103-21		/19			PLAT		<u> </u>



ENGINEERING CORP. BORING

G <u>B-25</u>

D	ATE 8	X/2/2021 TYPE 4" Dry Auger			LOC	CATION See Boring Location	on Plan	<u> </u>		
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3190150.63 Northing: 13787123.06 Elevation: 27.80	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 SHEAR STRENGTH, TSF Confined Compression Unconfined Compression Pocket Penetrometer Torvane 	200 MESH -IQUID LIMIT	PLASTIC LIMIT PLASTICITY INDEX		
- 5 -		Stiff to very stiff, gray Fat Clay with Sand (CH) -with clayey sand seams and roots 0'-2' -dark gray 2'-4' -tannish gray and dark gray, with calcareous nodules 4'-6' and ferrous nodules 4'-8' -tan and gray 6'-8' -groundwater measured at 6.6 ft approximately 15 mins afetr initial encounter -reddish tan and gray, with calcareous nodules and pockets 8'-10' Very stiff, reddish tan and gray Lean Clay (CL),		27 24 27 25 24	97.1		83 54	15 39		
- 15 -		Tan Silt (ML), with sand pockets, wet	Z	20 21 21	110.6		93 29	18 11		
- 20 -										
- 25 -										
- 35 -	BORIN	G DRILLED TO 16 FEET WITHOUT DF		NGT						
١	NATEF NATEF	R ENCOUNTERED AT <u>14</u> FEET WHILE R LEVEL AT <u>6.6</u> FEET AFTER <u>COMPLI</u> ED BY JH Drilling DRAFTED BY	E DR ETE		NG ÷	$\overline{\Sigma}$	DN			
	ROJEC.			/ //				 Δ_27		



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

Image: Construction Image: Construct	DATE <u>8</u> /	2/2021 TYPE <u>4" Dry Auger</u>		LOC	CATION See Boring Locat	ion I	Plan	1		
Pint of Very Suit, dark of Very Very Very Very Suit, dark of Very Very Very Very Very Very Very Very		GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3190283.37 Northing: 13787273.58	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
WATER ENCOUNTERED AT <u>14</u> FEET WHILE DRILLING \ WATER LEVEL AT <u>7.9</u> FEET AFTER <u>15 MINS</u> \		Firm to very stiff, dark brown Fat Clay (CH), with slickensides -with lean clay pockets and roots 0'-2' -dark gray 2'-4', with ferrous nodules 2'-6' -gray 4'-6' -reddish tan and gray, with calcareous nodules and pockets 6'-8' Stiff to very stiff, tan and gray Lean Clay (CL) Loose, tan Silt with Sand (ML), wet -reddish tan 12'-14'	16	25 24 31 16 23 24			-			42
WATER ENCOUNTERED AT <u>14</u> FEET WHILE DRILLING \ WATER LEVEL AT <u>7.9</u> FEET AFTER <u>15 MINS</u> \			 	NG F	 - \ JIF	<u> </u>	-			_
	WATER WATER DRILLE	R ENCOUNTERED AT <u>14</u> FEET WHILI R LEVEL AT <u>7.9</u> FEET AFTER <u>15 MIN</u> D BY <u>JH Drilling</u> DRAFTED BY	E DR 1 s	llLli ₹	NG -	₩ Ţ	DN			



ENGINEERING CORP. GEOTECHNICAL ENGINEERS BORING B-27

D/	ATE <u>7/</u>	1/2021 TYPE <u>4" Dry Auger</u>		LOC	CATION See Boring Location Plan	
		DESCRIPTION		% ,		SHEAR STRENGTH, TSF
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3190347.65 Northing: 13787345.15 Elevation: 28.98	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2
0		Pavement: 2.5" asphalt		10		85 48 16 32
- 5 -		Fill: hard, brown and black Lean Clay with Sand (CL), with gravel Very stiff to hard, dark brown and black Fat Clay (CH), with slickensides -dark brown 4'-6'	-	18 22 21	104.1	
		-gray and dark gray, with ferrous nodules 6'-8' -reddish tan and gray, with calcareous nodules		23		86 60 17 43
- 10 -		and pockets 8'-10' Very stiff, tan and reddish tan Lean Clay (CL), with clayey sand seams and pockets		28 21	99.4	
		-tan 12'-14', wet at 12'	Z	23		88 29 19 10
- 15 -		Tan Silt (ML), wet		24		
- 20 -		Termination Depth = 16 feet				
		G DRILLED TO <u>16</u> FEET WITHOUT DF ENCOUNTERED AT 14 FEET WHILI				
\	NATER	LEVEL AT <u>11</u> FEET AFTER <u>COMPL</u>	ETE	- -		
	DRILLEI	D BY JH Drilling DRAFTED BY		YY/N	IRH	LOGGED BY DN



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

D	ATE <u>6</u>	/21/2021 TYPE 4" Dry Auger			LOC	CATION See Boring Location Plan
=EET	TERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204	WS / FT.	MOISTURE CONTENT, %	DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ⊥
DEPTH IN FEET	SYMBOL SAMPLE INTERV	Easting: 3190587.56 Northing: 137876613.52 Elevation: 25.94	S.P.T. BLOWS / FT.	MOISTURE	DRY DENS	Confined Compression Unconfined Compression Unconfined Compression Pocket Penetrometer Torvane 0.5 1 1.5 2
0 - 5 - 10 - 10 - 15 - 20 - 20 - 20 - 25 - 30 - 30 - 30 - 35 - 35		Very stiff, brown and dark gray Fat Clay (CH) Soft to very stiff, tan and gray Lean Clay (CL), with sand partings -with ferrous nodules 2'-4' Medium dense, tan and gray Silty Sand (SM), wet -with clayey sand seams 6'-8' Loose to medium dense, light tan and gray Poorly Graded Sand with Silt (SP-SM), wet -with clayey sand seams 10'-12' -grayish tan 12'-14' -tan, with fat clay seams 14'-16' Termination Depth = 16 feet	7 14 17 9	22 18 21 20 21 21 21	109.2	58 19 39 58 19 NP 13 NP NP 11 II I
۱ ۱	WATE	G DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT <u>N/A</u> FEET WHILI	E DR	ILLI		
		R LEVEL AT <u>4</u> FEET AFTER <u>COMPL</u>			v	
	URILLE	ED BY JH Drilling DRAFTED BY		Y	ĭ	LOGGED BY DN



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

DATE <u>6/21/20</u>	21 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan
LEE CLARENCE EN LEE CLARENCE E	-	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2
0Very s with leHard, with feHard, with feStiff to with s -with l -reddi 8'Firm t -with f10-tan 1 -with s-with s -with sFirm t calcar	stiff, gray and dark brown Fat Clay (CH), ean clay and silty sand pockets tan and gray Lean Clay with Sand (CL), errous nodules to very stiff, tan and gray Fat Clay (CH), lickensides and calcareous nodules lean clay seams 4'-6' ish brown, with sandy lean clay partings 6' to very stiff, tan and gray Lean Clay (CL) ferrous nodules 8'-12'		20 18 27 30 20 21 24 26	103.1	75 41 14 27 95 37 15 22
- 35 -					
WATER ENC WATER LEVE	LLED TO <u>16</u> FEET WITHOUT DF OUNTERED AT <u>14</u> FEET WHILE EL AT <u>7</u> FEET AFTER COMPLE 	E DR		NG -	



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

DA	ATE <u>6</u>	/21/2021 TYPE 4" Dry Auger			LOC	CATION See Boring Location Plan			
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3190855.46 Northing: 13787912.42	.P.T. BLOWS / FT.	MOISTURE CONTENT, %	RY DENSITY, PCF	SHEAR STRENGTH, TSF ⊥ △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1			
		<i>Elevation: 28.36</i> Very stiff, dark brown Lean Clay (CL), with sand partings Stiff to very stiff, dark gray Fat Clay with Sand (CH), with slickensides -with ferrous nodules 2'-6' -tan and dark gray 4'-6', with calcareous nodules 4'-8' -reddish tan 6'-8'	<u>о</u> 12	16 23 22 33	102.0				
- 10 -		-brown and gray 8'-10' Stiff to very stiff, brown Lean Clay (CL) -with calcareous nodules 10'-12' -with ferrous nodules 12'-14'	13	26 21 22	105.6	96 33 16 17			
- 15 -		-tan and gray, with fat clay pockets and calcareous nodules 14'-16' Termination Depth = 16 feet	13	22					
- 25 -									
- 30 -									
V	VATE	R ENCOUNTERED AT <u>14</u> FEET WHILE R LEVEL AT <u>11</u> FEET AFTER COMPL ED BY JH Drilling DRAFTED BY		Ţ		⊊ LOGGED BY DN			



ENGINEERING CORP. BORING

D	ATE 6	/21/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Loca	tion	Plar	<u>۱</u>	
		DESCRIPTION		т, %		SHEAR STRENGTH, TSF	Τ			\square
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3190990.08 Northing: 13788062.33 Elevation: 28.64	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
0		Very stiff, dark brown Lean Clay with Sand (CL), with roots		20		c	83	40	17	23
		Stiff to very stiff, dark brown Fat Clay (CH), with slickensides -with ferrous nodules 2'-8'		24						
- 5 -		-gray and dark gray 4'-6'		24	100.0	↓ ↓ ↓ ↓ ♦ ↓ ♦ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓				
		-tan and reddish tan, with lean clay seams 6'-8'		23						
- 10 -		-reddish tan 8'-10', with calcareous nodules 8'- 14'		27		à	90	62	24	38
		-tan 10'-14'		31			-			
				26	99.6					
- 15 -		Very stiff, reddish tan Lean Clay (CL)		23		·····				
		Termination Depth = 16 feet								
- 20 -							+-			
							+			
- 25 -							+			
- 30 -							+-			
- 35 -					<u> </u>					
١	WATEF	G DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT <u>N/A</u> FEET WHILE	E DR	ILLI						
		R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLI</u> ED BY JH Drilling DRAFTED BY	TE	Ţ Ţ	Y	LOGGED BY	DN			
PF							PLA	TF	Δ-3	3



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

D	DATE 8/2/2021 TYPE 4" Dry Auger LOCATION See Boring Location Plan									
		DESCRIPTION		NT, %		SHEAR STRENGTH, TSF				
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3191126.90 Northing: 13788214.86 Elevation: 28.58	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
0		Firm to hard, dark brown Fat Clay (CH), with slickensides		26			88	54	19	35
		-with roots 0'-2' -dark gray 2'-6'		27	95.0		_			
- 5 -		-with calcareous nodules 4'-16'	7	29			-			
		-reddish tan and gray 6'-8'		26	102.1		-			
		-brown, with calcareous pockets 8'-10'	16	19			99	59	22	37
- 10 -		-brown and gray 10'-12'		29		×	-			
		-tan and gray 12'-14'		28			-			
- 15 -		-brown and gray 14'-16'	19	33			-			
		Termination Depth = 16 feet					-			
							_			
- 20 -							-			
							-			
							-			
- 25 -							-			
							-			
- 30 -										
- 35 -										
F	BORIN	G DRILLED TO 16 FEET WITHOUT DF		NG F		$\frac{1}{2}$				Ц
۱ ۱	NATE	R ENCOUNTERED AT <u>N/A</u> FEET WHILE	E DR							
		R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLI</u> ED BY JH Drilling DRAFTED BY			εH	LOGGED BY	DN			
	PROJECT NO. G103-21 PLATE A-34							4		



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

with Sand (CH), with ferrous and calcareous ondues -gray 4'-6' 29 94.8 •	DATE	8/2/2021 TYPE <u>4" Dry Auger</u>	LOCATION See Boring Location Plan								
0 Fill: very stiff, dark brownish gray Fat Clay (CH), with gravel, ferrous nodules, and roots 27 00 10 5 53 18 16 -gray 4-0' -gray 4-0' 23 24 24 24 24 24 24 24 25 53 18 16 -gray 4-0' -gray 4-0' 26 24 23 100.0 96 65 24 17 -tan, with calcareous nodules 26 100.0 96 65 24 18 -tan, with calcareous pockets 12:14' 26 26 100.0 98 65 24 28 Termination Depth = 16 feet 24 26 24 26 24 26 24 26 24 26 24 26 24 26 24 26 24 26 24 26 24 26 24 26 24 26 24 24 26 24 24 26 24 24 26 24 24 26 24 26 24 26 26 26 26 24	DEPTH IN FEET SYMBOL	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3191256.90 Northing: 13788359.82	S.P.T. BLOWS / FT.	AOISTURE CONTENT, %	DRY DENSITY, PCF	 △ Confined Compression Unconfined Compression Unconfined Compression ⊢ ШИ ТОЦЬ □ Pocket Penetrometer □ Torvane 					
10 with slickensides and calcareous nodules 26 100.0 26 100.0 98 65 24 -tan, with calcareous pockets 12'-14' -tan and reddish tan 14'-16' 26 24 26 24 98 65 24 15 Termination Depth = 16 feet 7		Fill: very stiff, dark brownish gray Fat Clay (CH), with gravel, ferrous nodules, and roots Stiff to very stiff, gray and dark gray Fat Clay with Sand (CH), with ferrous and calcareous nodules -gray 4'-6'		29 24	94.8						
Image: Second secon		with slickensides and calcareous nodules -tan, with calcareous pockets 12'-14'		30 26	100.0						
BORING DRILLED TO <u>16</u> FEET WITHOUT DRILLING FLUID WATER ENCOUNTERED AT <u>N/A</u> FEET WHILE DRILLING \rightleftharpoons WATER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLETE</u>	20 -	Termination Depth = 16 feet									
WATER ENCOUNTERED AT <u>N/A</u> FEET WHILE DRILLING \ WATER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLETE</u> \											
DRILLED BY JH Drilling DRAFTED BY MRH LOGGED BY DN	WA1 WA1	ER ENCOUNTERED AT <u>N/A</u> FEET WHILI	E DR	NILLIN ₹	NG -						



ENGINEERING CORP. BC

D	ATE <u>6</u>	15/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3191389.97 Northing: 13788508.18 Elevation: 28.52	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF ⊥ ⊥ △ Confined Compression ⊥ ⊥ ● Unconfined Compression HS HS ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2
0		Stiff to hard, dark brown Lean Clay with Sand		_		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
		(CL) -with roots 0'-2' -tan and tannish gray 2'-4', with ferrous nodules 2'-6'		22 23	100.5	
- 5 -		-brown and gray, with calcareous nodules 4'-6'	16	16		
		Stiff to hard, reddish tan Fat Clay (CH), with slickensides -with calcareous pockets 6'-8' and nodules 6'-		26		
- 10 -		12' -brown, with ferrous stains 8'-10' -brown and gray 10'-12'	20	24		99 59 21 38
		-tan and gray, with ferrous stains 12'-14'		29 31	96.0	
- 15 -		-with calcareous nodules 14'-16'	16	30		
- 20 -		Termination Depth = 16 feet				
		G DRILLED TO <u>16</u> FEET WITHOUT DF ₹ ENCOUNTERED AT N/A FEET WHILI				
۱	NATEF	R LEVEL AT <u>N/A</u> FEET AFTER COMPL D BY JH Drilling DRAFTED BY				LOGGED BY DN
	ROJEC			-		



PLASTICITY INDEX

41

29

PROJECT: EFD Taxiway L Geotechnical In	vestigation		E	ENGINEERING CORP. BORING	E	8-35	;
DATE <u>6/15/2021</u> TYPE <u>4" Dry Aug</u>	er		LOC	CATION See Boring Locat	on F	Plar	<u> </u>
DESCRIPTION		IT, %		SHEAR STRENGTH, TSF			
GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3191523.83 Northing: 13788656.52 Elevation: 28.58	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT
Hard, dark brown Lean Clay (CL), with partings and roots	n sand	16					
Very stiff, tannish gray and gray Fat C with ferrous nodules	lay (CH),	24			88	59	18
-tan and gray, with abundant calcareo nodules 4'-6'	bus	16	115.9				
Stiff to very stiff, tan and reddish tan L (CL), with fat clay pockets and calcare nodules		26					
-with ferrous nodules 6'-8' -brown, with calcareous pockets 8'-10	,	22			89	49	20
Very stiff, brown and gray Fat Clay (C slickensides -with calcareous nodules 10'-12'	H), with	26	99.8	¢			
-tan and gray, with ferrous nodules 12	2'-14'	30					
-tan, with silty sand seams 14'-16'		32					
Termination Depth = 16 feet							
- 20 -							
- 25 -							
- 30 -							
- 35 -							
BORING DRILLED TO <u>16</u> FEET WITH							L
WATER ENCOUNTERED AT <u>N/A</u> FEE WATER LEVEL AT N/A FEET AFTER			NG -	÷			
DRILLED BY JH Drilling DRAFTE			Y	LOGGED BY	DN		



ENGINEERING CORP. B

DA	te <u>6</u>	/15/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan
	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3191657.43 Northing: 13788805.19 Elevation: 28.03	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2
		Very stiff, dark brown Lean Clay with Sand (CL) Firm to hard, dark gray Fat Clay (CH), with slickensides -with ferrous nodules 2'-6' -gray and grayish tan 4'-6', with calcareous nodules 4'-14' -tan and gray 6'-8' -brown, with calcareous pockets 8'-10' -reddish tan 10'-12' -tan and gray, with calcareous pockets 12'-14' -tan, with ferrous stains 14'-16' Termination Depth = 16 feet	8	20 25 19 22 23 29 28 30	104.7	80 38 16 22 97 59 22 37
		G DRILLED TO <u>16</u> FEET WITHOUT DF				
W	/ATEI	R ENCOUNTERED AT <u>N/A</u> FEET WHILE R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u>	ETE	Ţ		
וט		ED BY JH Drilling DRAFTED BY		YY/N	n KH	LOGGED BY DN



ENGINEERING CORP. BORING

			G	GEOTECHNICAL ENGINEERS
DATE <u>6/15/2021</u> TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan
DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3191791.89 Northing: 13788954.42 S Elevation: 28.03	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2
0 Hard, brown Fat Clay (CH), with calcareous nodules Very stiff, dark gray Lean Clay (CL) 5 Stiff to very stiff, gray and light gray Fat Clay with Sand (CH), with calcareous nodules -with lean clay seams 4'-6' -tan and gray, with ferrous nodules 6'-8' Stiff to very stiff, tan and gray Fat Clay (CH), with slickensides, and calcareous nodules and pockets -reddish tan and gray 10'-12' -tan 14'-16' 15 20 20 30 30		20 20 22 20 25 24 31 28	105.7	82 58 19 39
BORING DRILLED TO <u>16</u> FEET WITHOUT DE WATER ENCOUNTERED AT <u>N/A</u> FEET WHIL	E DR	RILLII		
WATER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u> DRILLED BY <u>JH Drilling</u> DRAFTED BY			IRH	LOGGED BY DN
· · · · · · · · · · · · · · · · · · ·				



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

DATE	DATE 6/15/2021 TYPE 4" Dry Auger LOCATION See Boring Location Plan							
	DESCRIPTION		ENT, %	ш	SHEAR STRENGTH, TSF			
DEPTH IN FEET SYMBOL SAMDIE INTEDVA	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3191927.79 Northing: 13789103.10 Elevation: 28.23	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH LIQUID LIMIT	PLASTIC LIMIT PLASTICITY INDEX	
	Fill: hard, brown and reddish tan Lean Clay (CL), with fat clay seams, sand partings, and calcareous nodules Stiff to very stiff, dark gray Fat Clay (CH), with		18 29	91.4	9	6 47	18 29	
5	slickensides -with ferrous nodules 4'-8'	10	23					
	-tan and gray 6'-8', with calcareous nodules 6'- 16'		20					
10	-tan and dark gray 8'-10' -reddish tan, with calcareous pockets 10'-12'	21	19		8	9 59	22 37	
	-red 12'-14'		22 30	102.6				
15	-brown and gray 14'-16'	22	26					
	Termination Depth = 16 feet							
- 20 -								
- 25 -								
- 30 -								
- 35 -								
WATE	I IG DRILLED TO <u>16</u> FEET WITHOUT DI R ENCOUNTERED AT <u>N/A</u> FEET WHIL	E DR					I	
	R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u> ED BY <u>JH Drilling</u> DRAFTED BY			IRH	LOGGED BY D	N		



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

D	ATE 🧕	6/14/2021 TYPE <u>4" Dry Auger</u>	LOCATION See Boring Location Plan						
		DESCRIPTION		, %		SHEAR STRENGTH, TSF			
DEPTH IN FEET	SYMBOL SAMPI F INTERVAL		S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 × 3 du Licitation 			
0		Fill: stiff, dark brown and tan Fat Clay (CH), with slickensides and lean clay seams		27	97.7				
		Stiff to very stiff, dark brown Lean Clay (CL)		21		89 49 16 33			
- 5 -		Stiff to hard, gray and dark gray Fat Clay (CH), with slickensides		24					
		-with ferrous nodules 4'-10' and calcareous nodules 4'-12' -light gray and tan 6'-8' -tan and gray 8'-10'		21	103.9				
- 10 -				18					
		-reddish tan and gray 10'-14'		24		99 57 21 36			
- 15 -		-reddish tan 14'-16'		26 29					
		Termination Depth = 16 feet							
- 20 -									
- 25 -									
- 30 -									
- 35 -									
		IG DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT N/A FEET WHILE							
\	NATE	R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLI</u> ED BY JH Drilling DRAFTED BY	ETE	- -					



ENGINEERING CORP. B

DA	DATE 6/14/2021 TYPE 4" Dry Auger LOCATION See Boring Location Plan								
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3192199.30 Northing: 13789396.53 Elevation: 27.42	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2			
0 - 5 - - 10 - - 10 - - 15 - - 20 - - 20 - - 25 - - 30 - - 30 -		Fill: very stiff, dark gray and tan Fat Clay with Sand (CH), with lean clay seams and roots Stiff to very stiff, gray and dark gray Fat Clay (CH) -with ferrous nodules 2'-4' -dark gray 4'-6' -gray and tan, with calcareous and ferrous nodules 6'-8' Very stiff, tan and gray Lean Clay with Sand (CL), with calcareous nodules and pockets Stiff to very stiff, tan and gray Fat Clay (CH), with slickensides -with calcareous nodules 10'-12' -tan and light gray 12'-14' Termination Depth = 16 feet	9 17 14	22 24 22 16 17 25 28 26	98.6	77 43 17 24			
V	VATE	G DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT <u>N/A</u> FEET WHILI R LEVEL AT N/A FEET AFTER COMPL	E DR						
	DRILLED BY JH Drilling DRAFTED BYYY/MRH LOGGED BY								



ENGINEERING CORP. BO

DA	TE <u>6</u>	/14/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan
		DESCRIPTION		Т, %		SHEAR STRENGTH, TSF
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL		S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 × X DU X × X D
		Fill: hard, dark gray and brown Fat Clay (CH), with calcareous nodules and roots		25		89 65 22 43
		Stiff to very stiff, light tannish gray Lean Clay with Sand (CL), with abundant calcareous nodules -tan and gray 4'-6', with ferrous stains 4'-8'		24	106.2	
- 5 -		-tan 6'-8'		21 16		75 42 16 26
- 10 -		Stiff to very stiff, tan and gray Fat Clay (CH), with slickensides -with calcareous nodules 8'-10' -reddish tan 10'-14'		24 24		
		-with ferrous nodules 12'-14'		32	90.5	
- 15 -		-tan 14'-16'		30		100 72 27 45
- 20 - - 25 - - 30 - - 35 -		Termination Depth = 16 feet				
		G DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT N/A FEET WHILE				
V	VATE	R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLI</u> ED BY <u>JH Drilling</u> DRAFTED BY				LOGGED BY BJ



ENGINEERING CORP. GEOTECHNICAL ENGINEERS BORING

B-42

DATE 6/14/2021 TYPE 4" Dry Auger LOCATION See Boring Location Plan						
DEPTH IN FEET	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3192474.48 Northing: 13789691.68 Elevation: 26.34	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF X and X a	
	Fill: hard, brown Lean Clay (CL) -with silt pockets and roots 0'-2'	.,	13	_	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
	-dark brown and brown 2'-4' Stiff to very stiff, brown Lean Clay (CL)		17	113.7		
- 5 -	-gray and tan, with ferrous nodules and stains 6'-8'	13	15 18	111.7	89 46 15 31	
10	Stiff to hard, tan and gray Fat Clay (CH), with slickensides -with silty sand pockets and calcareous nodules 8'-10'	12	21	105.0	95 53 20 33	
	-reddish tan and gray 10'-12' -reddish tan, with calcareous nodules 12'-16'		22 26	105.6		
15	Termination Depth = 16 feet	13	28			
- 20 -						
- 25 -						
- 30 -						
- 35 -						
W A	DRING DRILLED TO <u>16</u> FEET WITHOUT DR ATER ENCOUNTERED AT <u>N/A</u> FEET WHILE	DR				
	ATER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLE</u> RILLED BY <u>JH Drilling</u> DRAFTED BY		¥ YY/N	IRH	LOGGED BY DN	



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

DATE <u>7/1/2021</u> TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Locat	ion Plan
DESCRIPTION	FT.	NTENT, %	PCF	SHEAR STRENGTH, TSF	
Image: State Plane Zone: 4204 Image: State Plane Zone: 4204 <td< td=""><td>.P.T. BLOWS / FT.</td><td>MOISTURE CONTENT,</td><td>DRY DENSITY, PCF</td><td> △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane </td><td>-200 MESH LIQUID LIMIT PLASTIC LIMIT</td></td<>	.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 	-200 MESH LIQUID LIMIT PLASTIC LIMIT
Image: Constraint of the second se	ο Ο	2		0.5 1 1.5 2	
Pavement: 7.25" concrete	1				
Base: 14" stabilized soil					
Stiff to very stiff, gray and dark gray Fat Clay (CH), with slickensides		28			
-with calcareous nodules 2.7'-4'		24	99.5		
-gray 4'-6', with ferrous nodules 4'-8' -with calcareous nodules 6'-8'		27	00.0		
-with calcareous hodules 6-6		26			92 58 18 40
-reddish tan and gray 8'-10'					
		31	93.6		
- 10 -tan and gray 10'-12'					
		31			
-tan, with ferrous nodules 12'-14'		34			73 28 45
brown and grow 14! 16!		0-1			
-brown and gray 14'-16'		34			
Termination Depth = 16 feet	-				
- 25 -					
- 30 -					
- 35 -					
BORING DRILLED TO 16 FEET WITHOUT DR	 				
WATER ENCOUNTERED AT N/A FEET WHIL					
WATER LEVEL AT N/A FEET AFTER COMPL				-	
DRILLED BY DRAFTED BY			IRH	LOGGED BY	DN



ENGINEERING CORP. BORING

G _____B-44

D	DATE <u>6/14/2021</u> TYPE <u>4" Dry Auger</u>					LOCATION See Boring Location Plan				
O DEPTH IN FEET	SYMBOL SAMPI F INTERVAL		S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF ▲				
- 5 - - 10 - - 10 - - 20 - - 20 - - 25 - - 30 - - 30 -		Fill: hard, dark gray and dark brown Lean Clay with Sand (CL), with fat clay pockets and roots Stiff to hard, dark gray Fat Clay (CH), with slickensides -gray and tan, with calcareous nodules 4'-8' -with ferrous stains 6'-8' -reddish tan and gray 8'-10' -tan, with calcareous nodules 10'-12' -reddish tan 12'-16' Termination Depth = 16 feet	11	17 22 15 21 23 27 30 30	96.8	75 41 16 25 52 21 31				
E	BORIN	I IG DRILLED TO <u>16</u> FEET WITHOUT DF		NG F	L LUI)				
۱ <i>۱</i>	NATE	R ENCOUNTERED AT <u>N/A</u> FEET WHILI	E DR							
		R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u>								
		ED BY DRAFTED BY		YY/N	IRH					
PF	ROJEC	CT NO. G103-21				PLATE A-46				



ENGINEERING CORP. GEOTECHNICAL ENGINEERS BORING

B-45

D	DATE 6/14/2021 TYPE 4" Dry Auger LOCATION See Boring Location Plan									
DEPTH IN FEET	SYMBOL SAMPI F INTFRVAI	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3192932.66 Northing: 13790012.28 Elevation: 25.35	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2				
0 - 5 - - 10 - - 15 - - 20 - - 20 - - 25 -		Fill: hard, brown and tan Fat Clay with Sand (CH), with calcareous nodules and gravel Stiff to very stiff, brown and tan Fat Clay (CH), with slickensides -with ferrous nodules 2'-8' -tan and gray, with calcareous nodules 4'-8' -reddish tan and gray, with calcareous pockets 8'-10' -reddish tan 10'-16' Termination Depth = 16 feet		23 23 19 30 28 30 32	97.3	83 55 19 36				
- 30 -										
	NATE NATE	IG DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT <u>N/A</u> FEET WHILI R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u> ED BY <u>JH Drilling</u> DRAFTED BY	E DR ETE		NG -					
PF		T NO. G103-21				PLATE A-47				



B-46

66 23 43

22 16 6

PLASTICITY INDEX PLASTIC LIMIT LIQUID LIMIT

DA	ATE e	6/14/2021 TYPE 4" Dry Auger			LOC	CATION See Boring Location P
		DESCRIPTION		П, %		SHEAR STRENGTH, TSF
DEPTH IN FEET	SYMBOL SAMPI F INTFRVAI	Texas State Plane Zone: 4204 Easting: 3193066.91 Northing: 13790165.72	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane ○ 5 1 15 2
0		<i>Elevation:</i> 24.87 Fill: very stiff, reddish brown and dark brown	0			
		Fat Clay (CH), with sandy lean clay pockets a ¬roots	nd	24		
		Fill: dark gray Silty Clayey Sand (SC-SM), wit shell fragments	n	14		41 2
5 -		Fill: firm to stiff, tan and gray Lean Clay (CL), with sandy lean clay seams and shell fragmen	nts 9	15		
		Stiff to very stiff, tan Lean Clay (CL), with ferrous nodules and abundant calcareous		22	105.4	
10 -		nodules Firm to very stiff, tan and gray Fat Clay (CH), with slickensides	13	24		
10 -		-reddish tan 10'-14'		26		97 6
				29	93.9	
15 -		-reddish tan and gray 14'-16'	12	28		
		Termination Depth = 16 feet				
0 -						
25 -						
30 -						
35 -						

JH Drilling

DRILLED BY

DN



ENGINEERING CORP. GEOTECHNICAL ENGINEERS BORING

G _____B-47

DATE <u>6/14/2021</u> TYPE <u>4" Dry Auger</u>					LOCATION See Boring Location Plan					
۲ VAL	DESCRIPTION GRID Coordinates (US Survey ft):	FT.	NTENT, %	PCF	SHEAR STRENGTH, TSF			DEX		
DEPTH IN FEET SYMBOL SAMPLE INTER	Texas State Plane Zone: 4204 Easting: 3193199.53 Northing: 13790317.36 Elevation: 24.87	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	PLASTIC LIMIT	PLASTICITY INDEX		
	Elevation: 24.87 Fill: hard, brown Fat Clay (CH), with gravel and roots Soft to stiff, tan and grayish tan Fat Clay (CH), with slickensides -tan and gray 4'-6' Stiff to very stiff, dark gray Lean Clay with Sand (CL) -gray and tan, with ferrous nodules and calcareous pockets 8'-10' Very stiff, gray and tan Fat Clay (CH) -with ferrous nodules and lean clay pockets 10'- 12' -with calcareous nodules 12'-16' -reddish tan 14'-16' Termination Depth = 16 feet	-	 ≤ 24 36 35 21 19 20 23 28 	74.0		?'	3 26	57		
- 35 -										
WATEI WATEI	G DRILLED TO <u>16</u> FEET WITHOUT DI R ENCOUNTERED AT <u>N/A</u> FEET WHIL R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u> ED BY <u>JH Drilling</u> DRAFTED BY	E DR . ETE	RILLIN E	NG 🖣		DN	_			



ENGINEERING CORP. BORING

D	DATE 6/14/2021 TYPE 4" Dry Auger LOCATION See Boring Location Plan								
		DESCRIPTION		NT, %		SHEAR STRENGTH, TSF		\square	
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3193332.02 Northing: 13790468.75 Elevation: 24.48	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	PLASTIC LIMIT	PLASTICITY INDEX	
0		Fill: stiff to hard, reddish brown and gray Fat Clay (CH), with slickensides and calcareous		27		90 66	3 22	44	
		nodules -gray, with silty sand seams and pockets, and ferrous nodules 2'-4'		15	116.0	++++++++++++++++++++++++++++++++++++++			
- 5 -		Firm to hard, dark gray Lean Clay with Sand (CL)	8	19					
		-with ferrous nodules 6'-8'		22					
40		-with calcareous nodules 8'-10'	13	22		84 44	15	29	
- 10 -		Stiff to very stiff, tan and gray Fat Clay (CH), with slickensides -with calcareous and ferrous nodules 10'-12'		26	100.5				
				29					
- 15 -		-reddish tan and gray 14'-16'	14	26					
		Termination Depth = 16 feet							
- 20 -									
- 25 -									
- 30 -									
- 35 -									
F	JORIN	IG DRILLED TO 16 FEET WITHOUT DF	 	NG F	 	<u> </u>]			
۱	NATE	R ENCOUNTERED AT <u>N/A</u> FEET WHILE	E DR	ILLI					
		R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u> ED BY JH Drilling DRAFTED BY		Ţ ¥¥/N	IRH	LOGGED BY DN			
		T NO. G103-21			•	<u>PLATE</u>	Δ-5		



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

DA	ATE E	6/14/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan	
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3193277.37 Northing: 13790676.93 Elevation: 25.90	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2	PLASTICITY INDEX
		Fill: stiff to very stiff, dark gray and brown Fat Clay (CH) -with calcareous nodules 0'-4' -brown and gray, with sandy lean clay pockets 2'-4' -reddish brown and black, with sand pockets and roots 4'-6' Stiff to very stiff, gray and dark gray Lean Clay (CL), with ferrous nodules and fat clay seams -tan and gray, with calcareous nodules and pockets 8'-10' Stiff to very stiff, tan and gray Fat Clay (CH), with slickensides -with calcareous nodules 10'-12' -reddish tan and gray 14'-16' Termination depth = 16 feet *: groundwater is likely perched G DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT <u>2*</u> FEET WHILE					43
V	VATE	R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u> I	ETE	Ţ			
		ED BY JH Drilling DRAFTED BY		YY/N	IRH	LOGGED BY DN	
PR		CT NO. G103-21				PLATE A-5	1



ENGINEERING CORP. BORING

B-50

DATE <u>8</u>	/4/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Loca	tion P	Plan		
DEPTH IN FEET SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3193142.56 Northing: 13790781.27 Elevation: 27.33	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
0 5 5 10 10 15 20 20 20 30 30 30 35 BORIN	Fill: stiff to very stiff, reddish tan and gray Fat Clay (CH), with calcareous nodules -gray and dark gray 2'-6' -with ferrous nodules 4'-6' Stiff to very stiff, gray Fat Clay (CH), with slickensides -with lean clay seams 6'-8' -gray and tan 8'-14', with ferrous nodules 8'-10' and calcareous nodules 8'-14' -with calcareous pockets 10'-12' -with ferrous stains 12'-14' -reddish tan 14'-16' Termination Depth = 16 feet GDRILLED TO <u>16</u> FEET WITHOUT DF	9 13 9 9	17 23 19 21 22 23 24 30	102.4 105.7		90	60 59	20	40
WATE	R ENCOUNTERED AT <u>14</u> FEET WHILI R LEVEL AT <u>10</u> FEET AFTER <u>COMPL</u>	ETE	Ţ						
	ED BY JH Drilling DRAFTED BY		YY/N	IRH	LOGGED BY				
PROJEC [®]	T NO. G103-21					PLAT	ΓE .	A-52	2



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

DATE <u>8/10/2021</u> TYPE <u>4" Dry Auger</u>			LOC	ATION See Boring Location Plan
DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3192959.63 Northing: 13790936.77 Elevation: 29.51	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF ⊥ △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 0.5 1
9 Pavement: 15.5" concrete Pavement: 5.9" concrete Base: 5.25" stabilized soil Fill: very stiff, dark gray and brown Fat Clay v Sand (CH) -brown and black, with lean clay seams 4'-6' Fill: very stiff to hard, gray and black Fat Clay (CH) -with calcareous nodules and lean clay pocked 6'-8' 10 Very stiff, dark gray Fat Clay (CH), with ferrou nodules -gray and tan, with calcareous nodules 14'-16 -15 20 20 30 30	ets us	23 17 24 20 22 21	110.0	91 56 16
BORING DRILLED TO <u>16</u> FEET WITHOUT WATER ENCOUNTERED AT <u>N/A</u> FEET WH WATER LEVEL AT <u>N/A</u> FEET AFTER <u>COM</u> I DRILLED BY <u>JH Drilling</u> DRAFTED BY	ILE DF PLETE	RILLII	NG -	



ENGINEERING CORP. BORING

B-52

DA	TE 8	B/10/2021 TYPE 4" Dry Auger	LOCATION See Boring Location Plan					
		DESCRIPTION		% ;		SHEAR STRENGTH, TSF		
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL		S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 × 3 1.5 2 		
0		Fill: very stiff, gray and tan Fat Clay with Sand (CH), with ferrous and calcareous nodules		20		84 50 15 35		
- 5 -		Stiff to very stiff, gray and tan Fat Clay (CH), with slickensides -with ferrous nodules 2'-6' -with calcareous nodules 4'-8'		19 24	102.4			
		-with lean clay seams and calcareous pockets 6'-8' -with claystone pockets 8'-10'		22				
10		-reddish tan and gray, with calcareous nodules		27	02.0	98 61 23 38		
		10'-12' -tan 12'-14'		31 33	92.6			
15 -		-reddish tan and gray, with sandy lean clay seams 14'-16'		33				
- 20 -		Termination Depth = 16 feet						
V	VATE	IG DRILLED TO <u>16</u> FEET WITHOUT DR R ENCOUNTERED AT <u>N/A</u> FEET WHILE	E DR	ILLI				
		R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLE</u> ED BY <u>JH Drilling</u> DRAFTED BY		YY/N	IRH	LOGGED BY		



ENGINEERING CORP. BORING

ING <u>**B-53**</u>

D	ATE 8	/10/2021 TYPE 4" Dry Auger	LOCATION See Boring Location Plan					
		DESCRIPTION		т, %		SHEAR STRENGTH, TSF	\square	
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3191884.44 Northing: 13789619.01 Elevation: 28.80	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	PLASTICITY INDEX	
0		Fill: very stiff, dark and tannish gray Fat Clay (CH), with ferrous nodules and roots		23		92 54 18	36	
		Stiff to very stiff, dark gray Fat Clay (CH), with ferrous nodules		25	99.0	••••••••••••••••••••••••••••••••••••••		
- 5 -		-gray, with calcareous nodules 6'-8'	11	24				
				22				
- 10 -		Stiff to very stiff, tan and gray Lean Clay with Sand (CL), with calcareous and ferrous nodules Stiff to hard, tan and gray Fat Clay (CH), with	10	17		79 48 16	32	
		slickensides		23	102.9			
		-with calcareous nodules 14'-16'		27				
- 15 -		Termination Depth = 16 feet	10	23				
- 20 -								
- 25 -								
- 30 -								
- 35 -								
١	NATEF	G DRILLED TO <u>16</u> FEET WITHOUT DR R ENCOUNTERED AT <u>N/A</u> FEET WHILE	E DR	ILLI				
		R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLE</u> D BY JH Drilling DRAFTED BY			IRH	LOGGED BY DN		
							 5	



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

DA	ATE e	5/15/2021 TYPE 4" Dry Auger	LOCATION See Boring Location Plan					
		DESCRIPTION		IT, %		SHEAR STRENGTH, TSF		
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL		S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF			
0		Hard, dark brown Lean Clay with Sand (CL), with silty sand seams and roots		20		0.5 1 1.5 2 4 46 18 28		
		Stiff to hard, gray and dark gray Fat Clay (CH), with slickensides -with ferrous nodules 2'-4' -tannish gray, with roots 4'-6'		24	97.3			
- 5 -		-gray and tan, with calcareous and ferrous nodules 6'-8'		26 16				
- 10 -		-gray and reddish tan 8'-10', with calcareous pockets 8'-14'		23	101.3			
		-tan and gray 10'-12'		25		99 62 23 39		
		-red and tan, with calcareous nodules 12'-14'		27				
- 15 -		-tan and gray 14'-16'		26				
		Termination Depth = 16 feet						
- 20 -								
- 25 -								
- 30 -								
- 35 -								
۱ V	NATE	IG DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT <u>N/A</u> FEET WHILE R LEVEL AT N/A FEET AFTER COMPLI	E DR					
		ED BY JH Drilling DRAFTED BY		YY/N	IRH	LOGGED BY DN		
PF		T NO. G103-21				PLATE A-56		



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

DATE <u>8/3/2021</u> TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan	
DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3191889.04 Northing: 13788625.07 Elevation: 28.99	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2	PLASTICITY INDEX
0 Pavement: 2" asphalt Base: 6" sand and gravel Firm to hard, dark brown Fat Clay (CH), with slickensides -with sandy lean clay pockets 0.7'-2' -gray and dark gray 2'-4', with ferrous nodules 2'-8' -tannish gray 4'-6' -tan and red 6'-8', with calcareous nodules 6'-10' -red and gray, with calcareous pockets 8'-10' -red and gray 10'-12' -tan and gray 12'-14' -tan and gray 12'-14' -reddish tan and gray 14'-16' Termination Depth = 16 feet 20 30 30	8	27 29 24 19 20 23 26 20	93.8	90 61 18	43
BORING DRILLED TO <u>16</u> FEET WITHOUT DR WATER ENCOUNTERED AT <u>N/A</u> FEET WHILE WATER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLE</u> DRILLED BY <u>JH Drilling</u> DRAFTED BY	E DR Ete		NG ÷		



ENGINEERING CORP. GEOTECHNICAL ENGINEERS BORING

G <u>B-56</u>

D	ATE 8	/10/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3191085.93 Northing: 13788726.98	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2
0 0	is to	Elevation: 28.61	ы. Ю	ž	ä	
		Fill: very stiff, tannish gray and brown Fat Clay (CH), with ferrous nodules and roots Firm to hard, dark gray Fat Clay (CH), with slickensides	-	28 20	104.5	92 77 24 53
- 5		-with ferrous nodules 2'-8' -gray and dark gray 4'-6' -reddish tan and tan 6'-8'	8	25		
		-reddish tan 8'-10'	11	29 24	99.8	98 55 22 33
- 10 -		-tan and gray 10'-12', with calcareous nodules 10'-14' -tan 12'-16', with silt seams 12'-14'		30		
- 15 -		-with ferrous nodules 14'-16'	12	24 28		
		Termination Depth = 16 feet				
- 20 -						
25						
- 30 -						
- 35 -						
١	WATE	G DRILLED TO <u>16</u> FEET WITHOUT DE R ENCOUNTERED AT <u>N/A</u> FEET WHIL R LEVEL AT <u>N/A</u> FEET AFTER COMPL	E DR	ILLI		
	DRILLE	ED BY JH Drilling DRAFTED BY		YY/N	IRH	LOGGED BY DN



ENGINEERING CORP. BORING

D	ATE <u>8/10/2021</u>	Image: Type 4" Dry Auger	LOCATION See Boring Location Plan					
	DE	SCRIPTION		т, %		SHEAR STRENGTH, TSF		
DEPTH IN FEET	국 GRID Coordinates 도 전 및 Easting: 31912	s (US Survey ft):	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	PLASTICITY INDEX	
0	Stiff to hard, tan Fa slickensides and o -with ferrous nodu -reddish tan and ta -tan and gray 4'-8'	alcareous nodules les 0'-4'		24 23	103.8		37	
- 5 -				24 25				
- 10 -	-with ferrous stains Stiff to very stiff, ta	s and silt partings 8'-10'	_	30	95.7	92 33 15	18	
		ms and pockets 12'-16'		20 21	106.1		10	
- 15 -			Ŧ	23	100.1			
	Termination Depth	n = 16 feet						
- 20 -								
- 25 -								
- 30 -								
- 35 -								
١	WATER ENCOUNTERE	<u>16</u> FEET WITHOUT D D AT <u>15</u> FEET WHIL FEET AFTER COMPL	E DR					
		ling DRAFTED BY			IRH	LOGGED BY DN		
PF	ROJECT NO. G103-21					PLATE A-59		



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

D	ATE 8	3/4/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Loca	tion	Plar	<u> </u>	
		DESCRIPTION		Γ, %		SHEAR STRENGTH, TSF				Π
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL		S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
0		Fill: stiff to very stiff, dark gray Fat Clay (CH) -with shell fragments and roots 0'-2'		21						
		-brownish and dark gray, with calcareous nodules 2'-4'		22	102.6	•				
- 5 -		Firm to hard, dark brownish gray Fat Clay (CH), with slickensides	6	22			87	55	18	37
		-tan and gray 6'-16', with ferrous nodules 6'-8'		27	98.8	<u>-</u>				
- 10 -		-with calcareous nodules 8'-10'	16	25						
		-with ferrous nodules 10'-12'		31			98	70	24	46
		-with calcareous nodules 12'-14'		34	90.6	4				
- 15 -		-with sandy lean clay seams 14'-16'	10	27						
		Termination Depth = 16 feet								
- 20 -										
- 25 -										
- 30 -										
- 35 -										
۱	NATE	IG DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT <u>N/A</u> FEET WHILE	E DR							
		R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u> ED BY JH Drilling DRAFTED BY		Ţ ¥¥/N	IRH	LOGGED BY	DN			
		TNO. G103-21					PLA	TF	Δ_6	



ENGINEERING CORP. E

DATE <u>8/10/2021</u> TYPE <u>4" Dry Auger</u>				LOCATION See Boring Location Plan					
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3190514.38 Northing: 13787800.88	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2			
0		<i>Elevation:</i> 23.57 Hard, gray and tan Sandy Lean Clay (CL), with ferrous and calcareous nodules		17		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			
- 5 -		Stiff to hard, reddish tan and gray Fat Clay (CH), with slickensides -with calcareous nodules and clayey sand seams 2'-4' -reddish tan, with ferrous nodules 4'-8'	-	26 40	99.6	97 74 29 4			
		Soft to stiff, tan and gray Lean Clay (CL)	-	38					
- 10 -		-tan 10'-12'	¥	23	104.4	99 30 19 1			
- 15 -		Firm to stiff, tan Silty Clay (CL-ML)		27					
		Termination Depth = 16 feet		20					
- 20 -									
- 25 -									
- 30 -									
- 35 -									
۱ ۱	WATE	IG DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT <u>10</u> FEET WHILI R LEVEL AT <u>4</u> FEET AFTER COMPL	E DR						
[DRILLI	ED BY JH Drilling DRAFTED BY		YY/N	IRH	LOGGED BY DN			



ENGINEERING CORP. BO

Image: Description Image: De	+ +	91 PLASTIC LIMIT 61 PLASTICITY INDEX
• • <td>+ +</td> <td></td>	+ +	
• • <td>35</td> <td>16 19</td>	35	16 19
Firm to hard, gray Fat Clay (CH), with		
- tan and gray, with lean clay seams 4'-6' and calcareous nodules 4'-10'		
-reddish tan and gray, with calcareous pockets 6'-8'		
-tan and gray 8'-12'	54	16 38
-reddish tan, with calcareous nodules and pockets 12'-16'		
15 12 24		
Termination Depth = 16 feet		
- 25 -		
- 35 -		
BORING DRILLED TO <u>16</u> FEET WITHOUT DRILLING FLUID		
WATER ENCOUNTERED AT <u>12</u> FEET WHILE DRILLING WATER LEVEL AT <u>10</u> FEET AFTER <u>COMPLETE</u> ₩		
DRILLED BY JH Drilling DRAFTED BYYY/MRH LOGGED BY DN PROJECT NO. G103-21 PL	ATE A	



ENGINEERING CORP. BORING B-61

D/	ATE <u>8/</u>	4/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan
		DECODIDITION		%		SHEAR STRENGTH, TSF
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3189874.38 Northing: 13786976.90 Elevation: 28.74	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2
0		Base: 12" sand with shell				
		Stiff to hard, black and dark brown Fat Clay (CH), with ferrous nodules -with roots 1'-2' -dark gray 2'-6'		19 22		
- 5 -				25	98.8	
		Very stiff, tan and gray Sandy Lean Clay (CL), with slickensides and ferrous nodules -with fat clay pockets and calcareous nodules	-	20		63 48 15 33
- 10 -		6'-10' -with calcareous pockets 8'-10'		24		
				21	107.2	
		Gray and tan Sandy Silt (ML) -with silty clay and lean clay pockets 12'-14'	¥.	23		72 24 21 3
- 15 -		-tan 14'-16'	¥	22		
		Termination Depth = 16 feet				
- 20 -						
- 25 -						
- 30 -						
- 35 -						
		R ENCOUNTERED AT <u>15</u> FEET WHILI R LEVEL AT 13 FEET AFTER COMPL			NG -	,
		D BY DRAFTED BY		YY/N	IRH	LOGGED BY DN
PF		NO. G103-21				PLATE A-63



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

D/	ATE <u>8/10/2021</u> TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan
	DESCRIPTION	FT.	NTENT, %	PCF	SHEAR STRENGTH, TSF
DEPTH IN FEET	Image: Texas State Plane Zone: 4204 Image: Texas Te	.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	Confined Compression Unconfined Compression Unconfined Compression Pocket Penetrometer Torvane 0.5 1 1.5 2
0 0		ن ن	Σ	ā	0.5 1 1.5 2 $\stackrel{\heartsuit}{}$ \Box \overline{a}
	Pavement: 12.5" concrete	_			
	Pavement: 3" asphalt	-			
	Base: 13.1" stabilized soil	-	30		96 68 20 48
	Stiff to very stiff, dark gray Fat Clay (CH), with slickensides				
- 5 -	-with ferrous nodules 4'-6'		30		
_			32	89.6	
	-tan and gray 8'-12', with ferrous nodules 8'-10'				
- 10 -	and calcareous nodules 8'-12'		24		
			32	90.8	
	-reddish tan 12'-14'				
			34		
- 15 -	-tan and gray, with lean clay seams 14'-16'		30		
	Termination Depth = 16 feet	-			
	4				
- 20 -					
	4 11				
- 25 -					
	4				
- 30 -					
	4 11				
	1				
- 35 -					
	 BORING DRILLED TO 16 FEET WITHOUT D			 _	
	WATER ENCOUNTERED AT N/A FEET WHIL				
	WATER LEVEL AT <u>N/A</u> FEET AFTER <u>COMP</u>			-	
	DRILLED BY JH Drilling DRAFTED BY		YY/N	IRH	LOGGED BY JH/DN
PF	ROJECT NO. G103-21	_	_	_	PLATE A-64



ENGINEERING CORP. BORING

DA	ATE E	8/10/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring L	ocation	Plan	_
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3187757.15 Northing: 13785144.79 Elevation: 25.59	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 SHEAR STRENGTH, TS △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 5 2 	n sion _I	LIQUID LIMIT	PLASTIC LIMIT PLASTICITY INDEX
- 10 - - 10 - - 10 - - 15 - - 15 - - 20 - - 20 - - 30 - - 30 - - 30 - - 30 -	SYV	Figure 11 1000000000000000000000000000000000000		31 29 34 34 23 20	92.6 88.5 107.8			72 2	YI 51 21 51 22 55
						<u> </u>			
	NATE NATE	IG DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT <u>N/A</u> FEET WHILE R LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u> I ED BY <u>JH Drilling</u> DRAFTED BY	E DR ETE		NG -		JH/D	N	
PF	ROJEC	T NO. G103-21					PLA	TE A	-65



ENGINEERING CORP. BORING

D	ATE 8	/10/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan
		DESCRIPTION		% ;		SHEAR STRENGTH, TSF
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3187758.98 Northing: 13784963.94 Elevation: 23.56	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2
0		Fill: firm to very stiff, dark gray Fat Clay (CH),		28		93 73 21 52
		with slickensides -with calcareous nodules and roots 0'-2' -with shell fragments 2'-4'		28	94.2	
- 5 -		-with ferrous nodules 4'-6'	6	32		
		Stiff to very stiff, tan and gray Fat Clay (CH), with slickensides -with calcareous nodules 6'-8'		30	94.8	
- 10 -			10	35		
		Hard, tan and gray Lean Clay (CL) Stiff to very stiff, brown and gray Fat Clay (CH)		18		
		-with calcareous and ferrous nodules 12'-14'		21	106.8	
- 15 -		-tan, with lean clay pockets 14'-16'	∓ ¥ 6	20		
	-	Termination Depth = 16 feet				
- 20 -	-					
- 25 -						
- 30 -						
- 35 -						
		G DRILLED TO <u>16</u> FEET WITHOUT DR				
		R ENCOUNTERED AT <u>15</u> FEET WHIL			NG -	¥
		R LEVEL AT <u>14</u> FEET AFTER <u>COMPL</u> ED BY <u>JH Drilling</u> DRAFTED BY		Ţ ¥¥/N	IRH	LOGGED BY DN
L						



ENGINEERING CORP. BORING

DA	ATE <u>8</u> /	5/2021 TYPE 4" Dry Auger			LOC	CATION See Boring Location Plan	
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3187914.00 Northing: 13783900.36 Elevation: 24.07	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2	PLASTIC LIMIT PLASTICITY INDEX
- 5 -		Stiff to hard, dark brown Fat Clay (CH), with slickensides -with roots 0'-2' and ferrous nodules 0'-10' -dark gray 2'-4' -gray and tannish gray 4'-6'		23 29 30	92.4	96 70	21 49
- 10 -		-gray and tan 6'-10'		32 25	100.3	98 73	21 52
		-reddish tan and gray 10'-12', with calcareous nodules 10'-14' -tan and gray 12'-14'	Ŧ	23 22			
- 15 -		Tan Silt (ML), with fat clay seams, wet Termination Depth = 16 feet	-	23			
- 20 -							
- 25 -							
- 30 -							
- 35 -							
V V	VATEF VATEF	G DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT <u>14</u> FEET WHILE R LEVEL AT <u>11</u> FEET AFTER COMPL	E DR ETE	RILLIN E	NG -		
		D BY <u>JH Drilling</u> DRAFTED BY		YY/N	икн	LOGGED BY DN PLATE A	



	PROJE	CT: EFD Taxiway L Geotechnical Investigation	on		E	ENGINEERING CORP. GEOTECHNICAL ENGINEERS	
		8/17/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan	
DEPTH IN FEET		DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3187503.54 Northing: 13783873.31 Elevation: 25.36	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2	PLASTICITY INDEX
- 5		Fill: hard, dark brown Lean Clay (CL), with calcareous nodules, shell fragments, and roots Fill: stiff to very stiff, gray and dark gray Fat Clay (CH), with slickensides and ferrous nodules Firm to very stiff, gray Fat Clay (CH), with slickensides -with ferrous nodules 4'-8' -grayish tan, with calcareous nodules 6'-8' -tan 8'-12'	6	16 33 38 36	87.4 86.6	96 84 24	60
- 10		-tan and gray 12'-16', with calcareous nodules	6	35 28	404 7		37
- 15		12'-14' -with silt seams 14'-16' Termination Depth = 16 feet	11	24	101.7		
- 20							
- 25	_						
	_						
- 30							
- 35		NG DRILLED TO 16 FEET WITHOUT DF	511 1 1				
	WATE WATE	ER ENCOUNTERED AT <u>N/A</u> FEET WITHOUT DE ER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u> I ED BY JH Drilling DRAFTED BY	E DR	ILLI	NG -		



DATE 8/17/2021 TYPE 4" Dry Auger LOCATION See Boring Location Plan Lunconfined Compression GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Eaching: 13733866.81 : Elevation: 24.99 5 5 5 5 0 Confined Compression Unconfined Compression Operationation Compression Unconfined Compression Operationation Compression Unconfined Compression Unconfined Compression Operationation Compression Unconfined Comp	PROJECT: EFD Taxiway L Geotechnical Investigati	ion		G	GEOTECHNICAL ENGINEERS	i <u> </u>	-67	-
Line DESCRIPTION Line Line Confined Compression Line Line <thline< th=""> Line Line</thline<>	DATE <u>8/17/2021</u> TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Loca	tion P	lan	_
Fin. sin to very suit, datk gray Fal Clay with calcareous nodules, shell fragments, and roots Fim. bowers with calcareous nodules 2-4' -yeik ferrous nodules 2'-4' -gray 4-6' -tan 6'-16', with ferrous nodules 6'-8' and calcareous nodules 6'-8' and calcareous nodules 10'-12' -with ferrous nodules 10'-12' 10 -with ferrous nodules 10'-12' 11 34 7 15 Termination Depth = 16 feet 12 13 20 35 80.1 21 22 10 with ferrous nodules 10'-12' 12 12 22 10 33 14 15 Termination Depth = 16 feet 12 13 14 15 16 17 28 29 29 20 20 21 22 23	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3187265.19 Northing: 13783866.81 Elevation: 24.99	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 	-200 MESH	LIQUID LIMIT	PLASTICITY INDEX
BORING DRILLED TO _16_ FEET WITHOUT DRILLING FLUID WATER ENCOUNTERED AT _N/A_ FEET WHILE DRILLING ₩	 Fill: stiff to very stiff, dark gray Fat Clay with Sand (CH), with calcareous nodules, sand pockets, shell fragments, and roots Firm to very stiff, dark gray Fat Clay (CH), with slickensides -with ferrous nodules 2'-4' -gray 4'-6' -tan 6'-16', with ferrous nodules 6'-8' and calcareous nodules 6'-16' -with ferrous nodules 10'-12' Termination Depth = 16 feet 	5	31 41 35 35 34 23 22	80.1		84	70 2	1 49
WATER ENCOUNTERED AT FEET WHILE DRILLING 😤						-		
DRILLED BY JH Drilling DRAFTED BY MRH LOGGED BY BpJ	WATER ENCOUNTERED AT <u>N/A</u> FEET WHIL WATER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPL</u>	E DF	RILLII ¥	NG -	$\overline{\Sigma}$	1		



Р	ROJE	CT: EFD Taxiway L Geotechnical Investigation	on		E	ENGINEERING CORP. BORING B-68	
D	ATE	8/17/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan	
DEPTH IN FEET	SYMBOL	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3186896.05 Northing: 13783851.50 Elevation: 23.83	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2	PLASTICITY INDEX
0 - 5 - 10 - 10 - 15 - 20 - 20 - 25 - 30 - 30 - 35		Termination Depth = 16 feet	7	25 41 39 36 31 20 21	79.5		
	WATE WATE	NG DRILLED TO <u>16</u> FEET WITHOUT DR ER ENCOUNTERED AT <u>N/A</u> FEET WHILE ER LEVEL AT <u>15</u> FEET AFTER <u>COMPLE</u>	E DR Ete	XILLII ¥	NG -	$\sum_{\overline{=}}$	
	DRILL	ED BY JH Drilling DRAFTED BY		MF	RH	LOGGED BY BpJ	



ENGINEERING CORP. GEOTECHNICAL ENGINEERS

D	ATE <u>8</u>	/17/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Loc	ation F	Plan	<u> </u>	
		DESCRIPTION		ЧТ, %		SHEAR STRENGTH, TSF				
DEPTH IN FEET	SYMBOL SAMPLE INTERVAL	GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3187467.24 Northing: 13783412.24 Elevation: 26.71	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
0		Pavement: 16.25" concrete								
- 5 -		Base: 7.75" cement stabilized base Subbase: 9.75" stabilized soil Fill: very stiff, brown and gray Fat Clay (CH), with calcareous nodules, sandy lean clay pockets, and gravel Firm to very stiff, dark grayish brown Fat Clay (CH), with slickensides and ferrous nodules		37 42 36	83.4		91	68	20	48
- 10 -		-brownish gray 6'-8' -grayish tan 8'-10', with calcareous nodules 8'- 14'		34	00.1		96	83	26	57
		-tan and gray 10'-16'		38 36	84.6					
- 15 -				23						
		Termination Depth = 16 feet								
- 20 -										
- 25 -										
- 30 -							+			
- 35 -							+-			
۱ ۱	NATE	G DRILLED TO <u>16</u> FEET WITHOUT DF R ENCOUNTERED AT <u>N/A</u> FEET WHILE R LEVEL AT N/A FEET AFTER COMPLI	E DR	ILLI						
		ED BYJH Drilling DRAFTED BY		MF	RH	LOGGED BY	DN/JH	ł		
PF	ROJEC	T NO. G103-21					PLA	TF	Δ_71	0



PROJECT: EFD Taxiway L Geotechnical Investigation	on		G	ENGINEERING CORP. BORING	B-70	
DATE <u>8/17/2021</u> TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Locat	ion Plan	
DESCRIPTION TV TV TV TV TV TV TV TV TV TV	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	 SHEAR STRENGTH, TSF Confined Compression Unconfined Compression Pocket Penetrometer Torvane 0.5 1 1.5 2 	-200 MESH LIQUID LIMIT PLASTIC LIMIT	PLASTICITY INDEX
0 Pavement: 15.5" concrete Base: 8" cement stabilized base Subbase: 12" stabilized soil Fill: stiff to very stiff, dark gray and brown Fat Clay (CH), with slickensides -with gravel 3'-4" -with ferrous and calcareous nodules 6'-8' Stiff to very stiff, gray and tan Fat Clay (CH), with slickensides -with ferrous nodules 8'-14' -tan 10'-12", with calcareous nodules 10'-14' -reddish tan and gray 12'-14' Termination Depth = 16 feet 20 30 30 30 30		28 37 30 38 39 33 20	90.2		98 86 25 94 80 26	
WATER ENCOUNTERED AT <u>N/A</u> FEET WHILI WATER LEVEL AT <u>N/A</u> FEET AFTER COMPL	E DR	ILLI				
DRILLED BY JH Drilling DRAFTED BY		MF	Н	LOGGED BY D	N/JH	



ENGINEERING CORP. BORING

B-71

DA	ATE <u>8/17/2021</u> TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Loca	tion I	Plan	<u> </u>	
	DESCRIPTION		, %		SHEAR STRENGTH, TSF				
DEPTH IN FEET	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3187613.52 Northing: 13786754.06 Elevation: 26.11	S.P.T. BLOWS / FT.	MOISTURE CONTENT,	DRY DENSITY, PCF	 △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2 	-200 MESH	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
0	Pavement: 13" concrete								
	Fill: dark brown Silty Sand (SM), with fat clay seams and pockets		20			92	56	10	37
	Stiff to very stiff, dark gray Fat Clay (CH), with slickensides		26	95.3		92	50	19	31
- 5 -			26						
	-with ferrous nodules 6'-12'		23						
- 10 -	-gray and tan 8'-14', with calcareous nodules 8'- 10'		28			94	67	20	47
			31						
	-with lean clay seams 12'-14'		19	108.3					
- 15 -	Stiff to very stiff, tan and gray Lean Clay (CL), with silt partings		21						
- 20 -	Termination Depth = 16 feet								
- 25 -									
- 30 -									
- 35 -									
	BORING DRILLED TO 16 FEET WITHOUT DR)							
۱ V	WATER ENCOUNTERED AT <u>N/A</u> FEET WHILE	E DR							
	WATER LEVEL AT <u>N/A</u> FEET AFTER <u>COMPLE</u>	TE				D			
	DRILLED BY <u>JH Drilling</u> DRAFTED BY ROJECT NO. G103-21		MR		LOGGED BY	BpJ/J PLA			
						F I A			



ENGINEERING CORP. B

D	ATE 8	8/17/2021 TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan
DEPTH IN FEET	SYMBOL SAMPI F INTFRVAI	DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3187389.62 Northing: 13786733.82	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2
0 0	is où		ω.	ž	ā	
- 5 -		Fill: hard, dark brown Fat Clay (CH), with calcareous nodules and roots Firm to very stiff, dark gray Fat Clay (CH), with slickensides -with ferrous nodules 2'-10' -gray 4'-6' -tan and gray, with calcareous nodules 6'-12'	6	18 21 24 28	99.0	
- 10 -			7	33 21		96 66 20 44
- 15 -		Firm to stiff, tan and gray Lean Clay (CL) -tan, with silty clay pockets 14'-16'	9	24 26	103.2	
		Termination Depth = 16 feet		20		
- 20 -						
- 25 -						
- 30 -						
- 35 -						
	NATE NATE	G DRILLED TO <u>16</u> FEET WITHOUT DI R ENCOUNTERED AT <u>N/A</u> FEET WHIL R LEVEL AT <u>11</u> FEET AFTER <u>COMPL</u>	E DR	XILLII ¥	NG -	
		ED BY DRAFTED BY		MF	RH	LOGGED BY BpJ
PF	ROJEC	CT NO. G103-21				PLATE A-74



B-73

DATE <u>8/17/2021</u> TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan	-
DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3187069.64 Northing: 13786711.34 Elevation: 24.70	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2	PLASTICITY INDEX
 Fill: hard, dark brown Fat Clay with Sand (CH), with ferrous nodules, shell fragments, gravel, and roots Firm to very stiff, dark gray Fat Clay (CH), with slickensides -with calcareous nodules 2'-4' -gray and tan 4'-8', with sandy lean clay pockets 4'-6' -reddish tan and gray 8'-12' -with ferrous nodules 10'-14' -tan and gray 12'-16', with lean clay pockets and silty clay seams 12'-14' Termination Depth = 16 feet 	6 8 8	12 29 27 34 36 31 23 25	90.0		6 34 6 46



PROJECT: EFD Taxiway L Geotechnical Investigation	ROJECT: EFD Taxiway L Geotechnical Investigation			ENGINEERING CORP. BORING B-74 Geotechnical engineers	-
DATE <u>8/17/2021</u> TYPE <u>4" Dry Auger</u>			LOC	CATION See Boring Location Plan	1
DESCRIPTION GRID Coordinates (US Survey ft): Texas State Plane Zone: 4204 Easting: 3186704.33 Northing: 13786699.81 Elevation: 20.79	S.P.T. BLOWS / FT.	MOISTURE CONTENT, %	DRY DENSITY, PCF	SHEAR STRENGTH, TSF △ Confined Compression ● Unconfined Compression ○ Pocket Penetrometer □ Torvane 0.5 1 1.5 2	PLASTIC LIMIT
 Fill: very stiff, gray and dark gray Fat Clay with Sand (CH), with calcareous nodules Stiff to very stiff, tan and gray Fat Clay (CH), with calcareous and ferrous nodules Stiff to hard, reddish tan and tan Lean Clay (CL), with calcareous nodules and pockets Firm to very stiff, reddish tan and gray Fat Clay (CH), with slickensides -with sandy lean clay seams and sandy silt pockets 8'-10' Firm to stiff, reddish tan Silty Clay with Sand (CL-ML) -with sand seams 10'-12' -tan 12'-16' -with calcareous nodules 14'-16', wet at 14' Termination Depth = 16 feet 30 	11 7 7	21 26 17 39 21 23 26	104.2	82 61	20
- 35 -					
BORING DRILLED TO <u>16</u> FEET WITHOUT DF WATER ENCOUNTERED AT <u>10</u> FEET WHILE WATER LEVEL AT <u>8</u> FEET AFTER <u>5 MIN</u> DRILLED BY JH Drilling DRAFTED BY	E DR S	ILLII ¥			

PLASTICITY INDEX

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KEY TO SYMBOLS

_	Description	_	Description
<u>Strata</u>	symbols	<u>Soil Sa</u>	mplers
	Fill		Undisturbed thin wall Shelby tube
	High plasticity clay	\square	Standard penetration test
	Low plasticity clay		Rock core
	Paving		Auger
	Silty low plasticity clay		No recovery
	Silt		
	Silty clayey sand		
	Silty sand		
y / / / y 4 / / y 7 / / y	Poorly graded sand with clay		
Misc. S	ymbols		
0	Pocket Penetrometer		
•	Unconfined Compression		
\bigtriangleup	Confined Compression		
\ Ţ	Water table depth during drilling		
	Subsequent water table depth		
	Torvane		



CLASSIFICATION OF SOILS FOR ENGINEERING PURPOSES

ASTM Designation D-2487

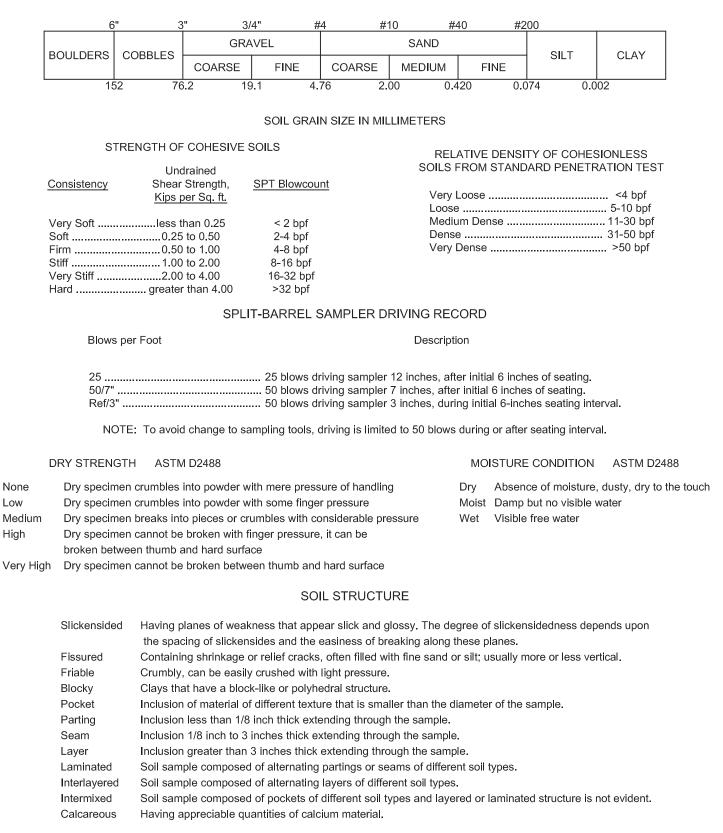
	MAJOR DIVISIONS			GROUP SYMBOL	TYPICAL NAMES	
	oarse sieve)	CLEAN GRAVELS (Less than 5% passes		GW	Well-graded gravel, well-graded gravel with sand	
eve)	(Less that 5/6 passes No. 200 sieve)		GP	Poorly-graded gravel, poorly-graded gravel with sand		
COARSE-GRAINED SOILS (Less than 50% passes No. 200 sieve)	GRAVELS (Less than 50% of coarse fraction passes No. 4 sieve)	GRAVELS WITH FINES (More than 12% passes	Limits plot below "A" line & hatched zone on plasticity chart	GM	Silty gravel, silty gravel with sand	
AINED (sses No	(Less fractio	No. 200 sieve)	Limits plot above "A" line & hatched zone on plasticity chart	GC	Clayey gravel, clayey gravel with sand	
COARSE-GRAINED SOILS than 50% passes No. 200 s	arse sieve)		AN SANDS	SW	Well-graded sand, well-graded sand with gravel	
COAR s than 5	SANDS or more of coarse passes No. 4 siev	(Less than 5% p	basses No. 200 sieve)	SP	Poorly-graded sand, poorly-graded sand with gravel	
(Les	SANDS (50% or more of coarse fraction passes No. 4 sieve)	SANDS WITH FINES (More than 12% passes	Limits plot below "A" line & hatched zone on plasticity chart	SM	Silty sand, silty sand with gravel	
	(50% (fraction	No. 200 sieve)	Limits plot above "A" line & hatched zone on plasticity chart	SC	Clayey sand, clayey sand with gravel	
					Silt, silt with sand, silt with gravel, sandy silt, gravelly silt	
) S	SILTS AND CLAYS (Liquid Limit Less Than 50%) USUBLY AND CLAYS USUBLY AND CLAYS SILTS AND CLAYS (Liquid Limit 50% or More)		CL	Lean clay, lean clay with sand, lean clay with gravel, sandy lean clay, gravelly lean clay		
NED SO			OL	Organic clay, organic clay with sand, sandy organic clay, organic silt, sandy organic silt		
GRAI				МН	Elastic silt, elastic silt with sand, sandy elastic silt, gravelly elastic silt	
	% or me		AND CLAYS hit 50% or More)	СН	Fat clay, fat clay with sand, fat clay with gravel, sandy fat clay, gravelly fat clay	
	(50'			он	Organic clay, organic clay with sand, sandy organic clay, organic silt, sandy organic silt	
			e No. 200 sieve and fine-grained so	oils with limit	s plotting in the hatched zone	
NOTE: Coarse soils between 5% and 12% passing the No. 200 sieve and fine-grained soils with limits plotting in the hatched zone of the plasticity chart are to have dual symbols. DEGREE OF PLASTICITY OF COHESIVE SOIL Degree of Plasticity Plasticity Index NOTE: PLASTICITY CHART DEGREE OF PLASTICITY OF COHESIVE SOIL Degree of Plasticity Plasticity Index None 0 - 4 Slight 5 - 10 Medium 11 - 20 High 21 - 40 Very High Soil SYMBOLS Fill Sand IQUID LIMIT (LL) Sand Equation of A-Line: Horizontal at Pl=4 to LL=25.5, then Pl=0.73(LL-20) Equation of U-Line: Vertical at LL=16 to Pl=7, then Pl=0.9(LL-8)					egree of Plasticity Plasticity Index one 0 - 4 ight 5 - 10 edium 11 - 20 gh 21 - 40 ery High >40 SOIL SYMBOLS Fill Clay (CH) Silt	



TERMS USED ON BORING LOGS

SOIL GRAIN SIZE

U.S. STANDARD SIEVE





ASTM & TXDOT DESIGNATION FOR SOIL LABORATORY TESTS

SOIL TEST	ASTM TEST DESIGNATION	TXDOT TEST DESIGNATION
Unified Soil Classification System	D 2487	Tex-142-E
Moisture Content	D 2216	Tex-103-E
Specific Gravity	D 854	Tex-108-E
Sieve Analysis	D 6913	Tex-110-E (Part 1)
Hydrometer Analysis	D 7928	Tex-110-E (Part 2)
Minus No. 200 Sieve	D 1140	Tex-111-E
Liquid Limit	D 4318	Tex-104-E
Plastic Limit	D 4318	Tex-105-E
Standard Proctor Compaction	D 698	Tex-114-E
Modified Proctor Compaction	D 1557	Tex-113-E
California Bearing Ratio	D 1883	-
Swell	D 4546	-
Consolidation	D 2435	-
Unconfined Compression	D 2166	-
Unconsolidated-Undrained Triaxial	D 2850	Tex-118-E
Consolidated-Undrained Triaxial	D 4767	Tex-131-E
Permeability (constant head)	D 5084	-
Pinhole	D 4647	-
Crumb	D 6572	-
Double Hydrometer	D 4221	-
pH of Soil	D 4972	Tex-128-E
Soil Suction	D 5298	-
Soil Sulfate	C 1580	Tex-145-E
Organics	D 2974	Tex-148-E

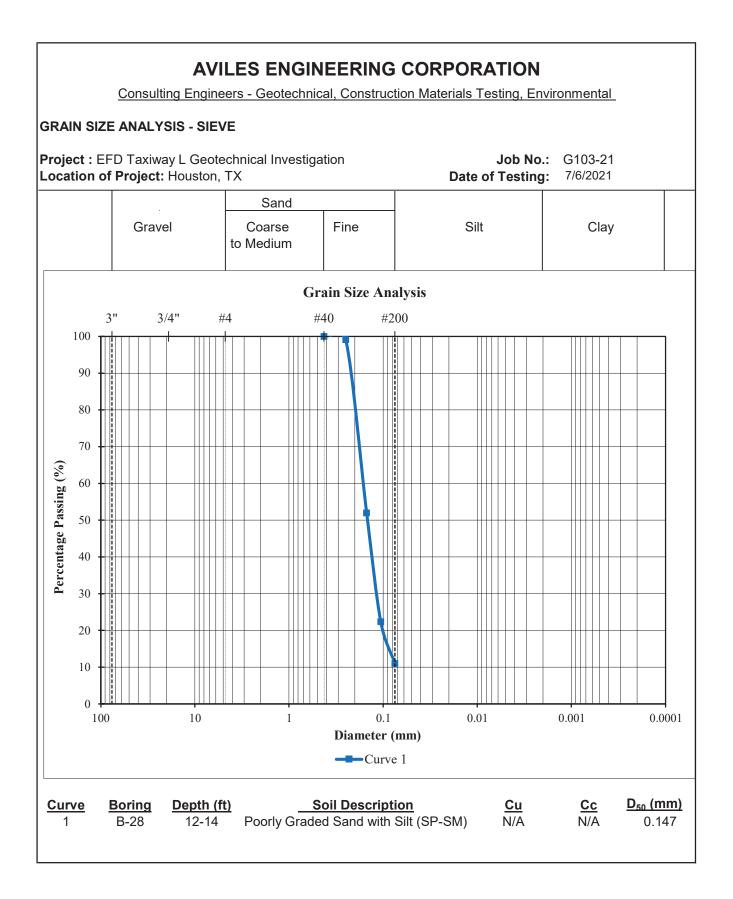


PLATE A-81

AVILES ENGINEERING CORPORATION

Consulting Engineers - Geotechnical, Construction Materials Testing, Environmental

ORGANIC MATTER IN SOILS

ASTM D 2974, Test Method C

Project : EFD Taxiway	L Geotechnical Investigation
Location of Project:	Houston, Texas

Job No.: G103-21 Date of Testing:

Boring	B-1	B-5	B-9	B-13
Depth (ft)	6 to 8	0 to 2	2 to 4	0 to 2
Soil Description	Fat Clay (CH)	Fill: Fat Clay (CH)	Fat Clay (CH)	Fat Clay (CH)
Organic Matter Content	4.6%	5.0%	5.5%	5.7%
Furnace Temperature, °C	440	440	440	440
Boring	B-17	B-21	B-25	B-31
Depth (ft)	0 to 2	0 to 2	4 to 6	0 to 2
Soil Description	Fat Clay (CH)	Lean Clay (CL)	Fat Clay with Sand (CH)	Lean Clay with Sand (CL)

Organic Matter Content	5.7%	5.3%	3.0%	3.8%
Furnace Temperature, °C	440	440	440	440

Boring	B-33	B-37	B-41	B-45
Depth (ft)	0 to 2	0 to 2	0 to 2	4 to 6
Soil Description	Fill: Fat Clay (CH)	Fat Clay (CH)	Fill: Fat Clay (CH)	Fat Clay (CH)
Organic Matter Content	6.2%	5.8%	5.2%	3.1%
Furnace Temperature, °C	440	440	440	440

Boring	B-49	B-53	B-57	B-61
Depth (ft)	2 to 4	0 to 2	2 to 4	6 to 8
Soil Description	Fill: Fat Clay (CH)	Fill: Fat Clay (CH)	Fat Clay (CH)	Sandy Lean Clay (CL)
Organic Matter Content	2.5%	4.1%	3.1%	2.5%
Furnace Temperature, °C	440	440	440	440

AVILES ENGINEERING CORPORATION

Consulting Engineers - Geotechnical, Construction Materials Testing, Environmental

ORGANIC MATTER IN SOILS

ASTM D 2974, Test Method C

Project : EFD Taxiway L Geotechnical Investigation **Location of Project:** Houston, Texas

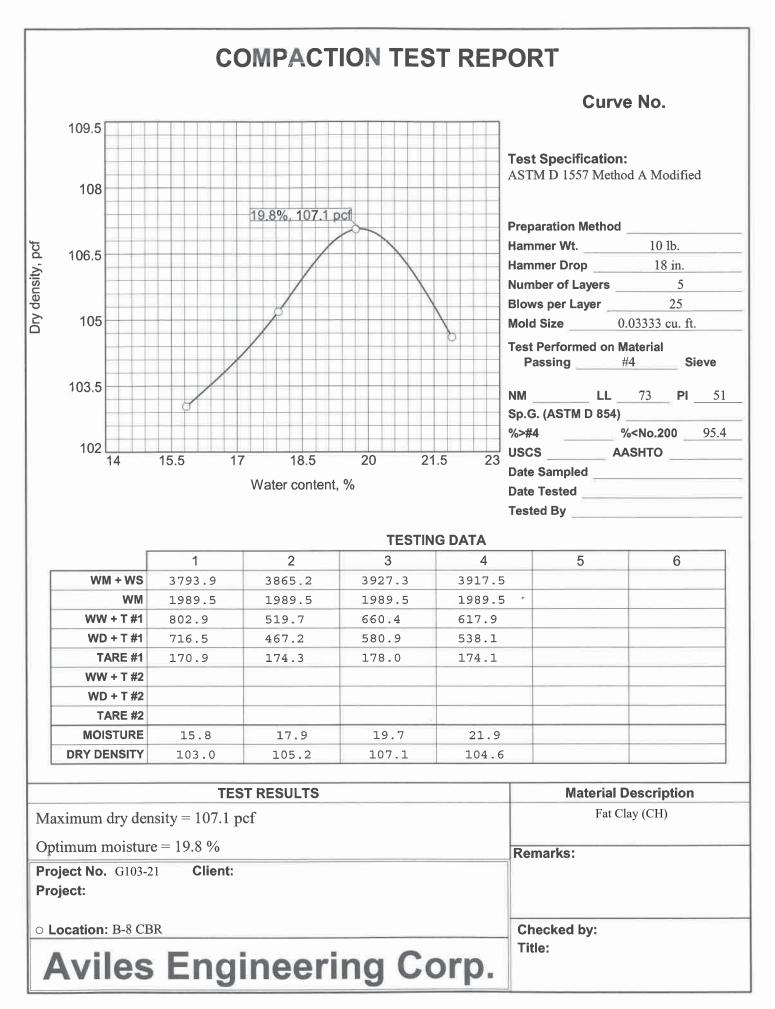
Job No.: G103-21 Date of Testing:

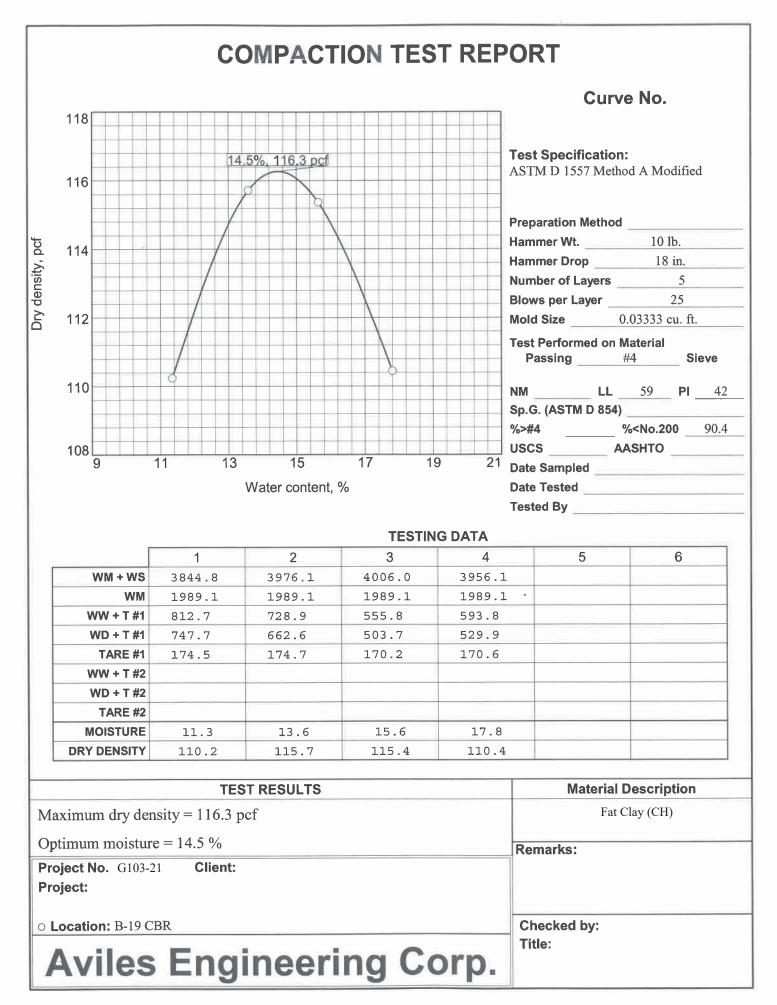
Boring	B-65	B-69	B-73	
Depth (ft)	6 to 8	6 to 8	0 to 2	
Soil Description	Fat Clay (CH)	Fat Clay (CH)	Fill: Fat Clay with Sand (CH)	
Organic Matter Content	4.5%	5.9%	3.9%	
Furnace Temperature, °C	440	440	440	

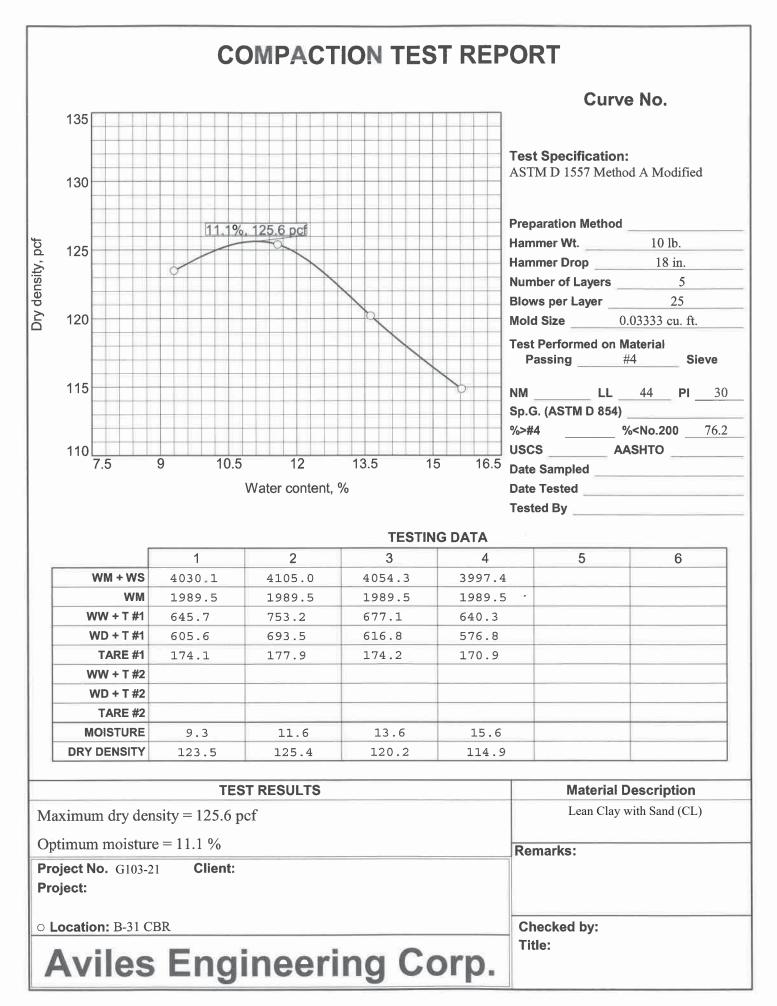


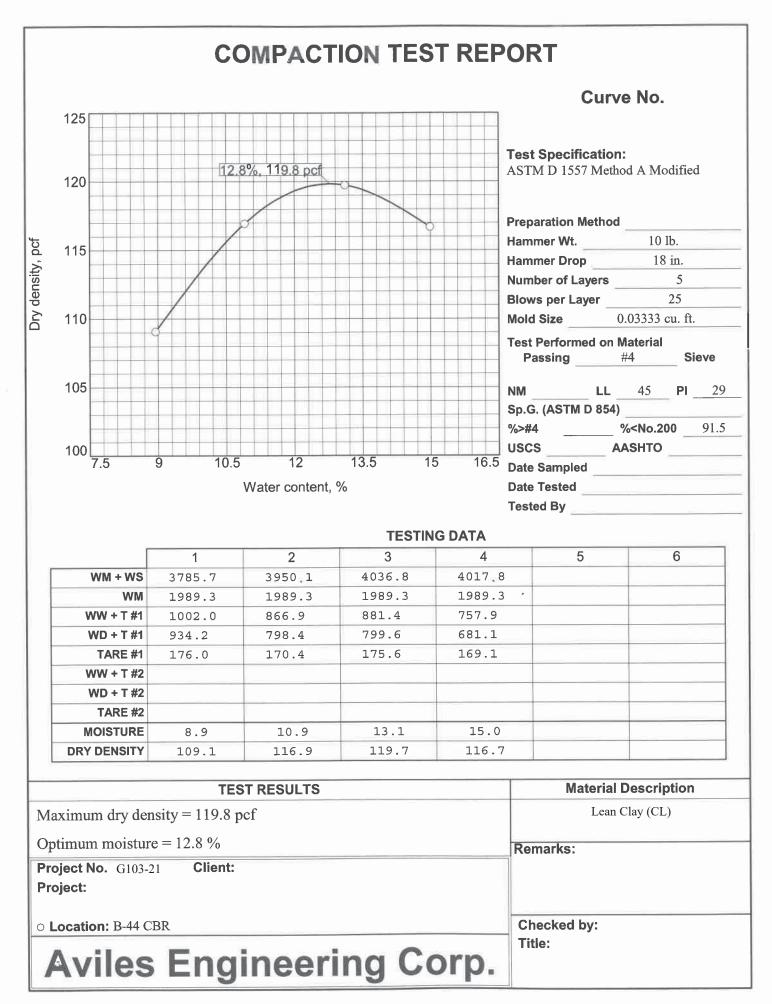
APPENDIX B

Plates B-1 to B-4Modified Proctor Test ResultsPlates B-5 to B-12California Bearing Ratio (CBR) Test ResultsPlates B-13 to B-49Dynamic Cone Penetrometer Test Results

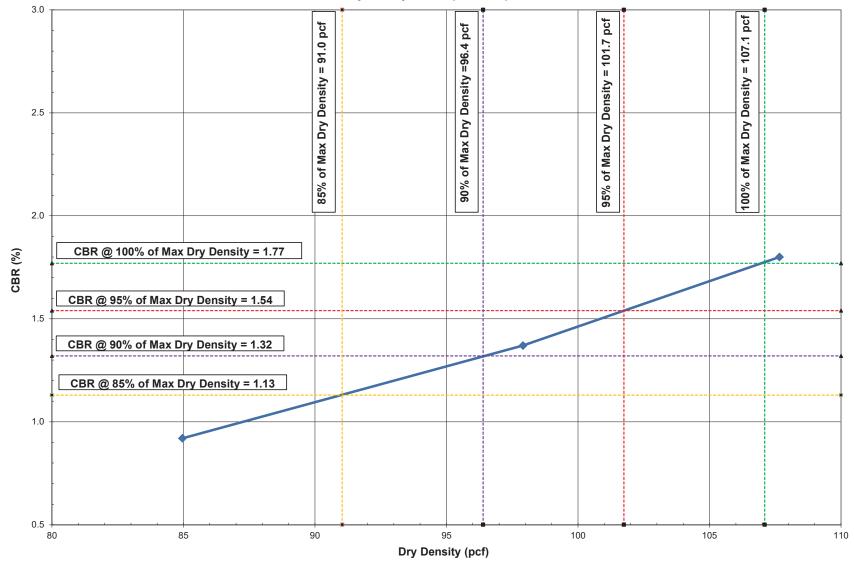


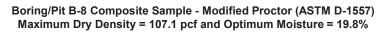


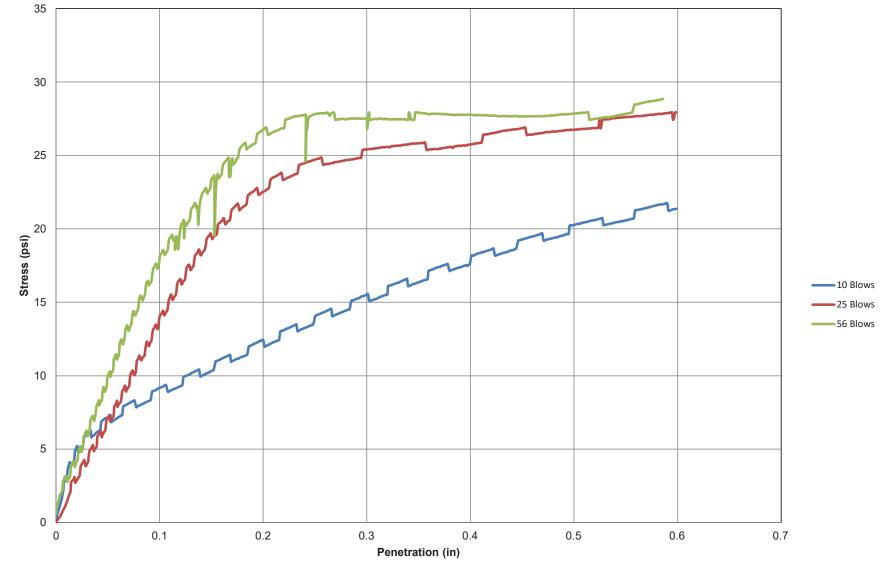




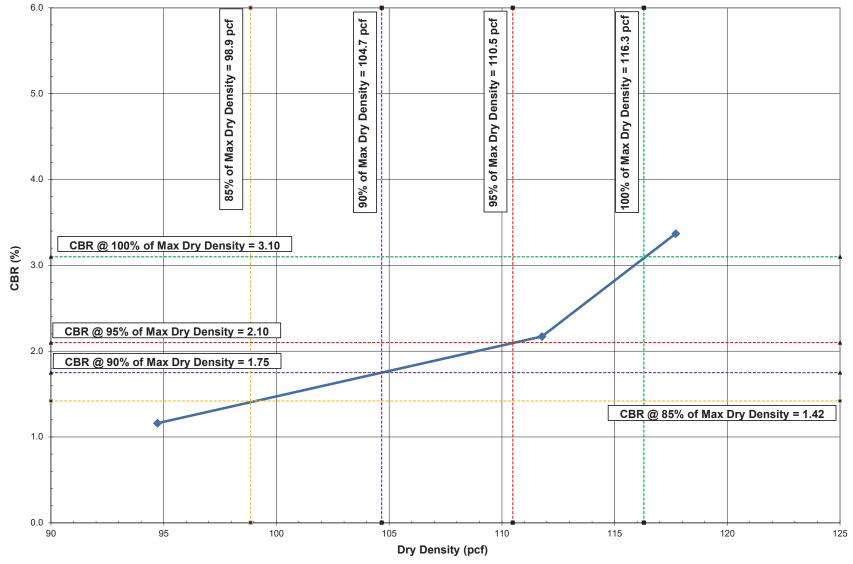
Boring/Pit B-8 Composite Sample - Modified Proctor (ASTM D-1557) Maximum Dry Density = 107.1 pcf and Optimum Moisture = 19.8%







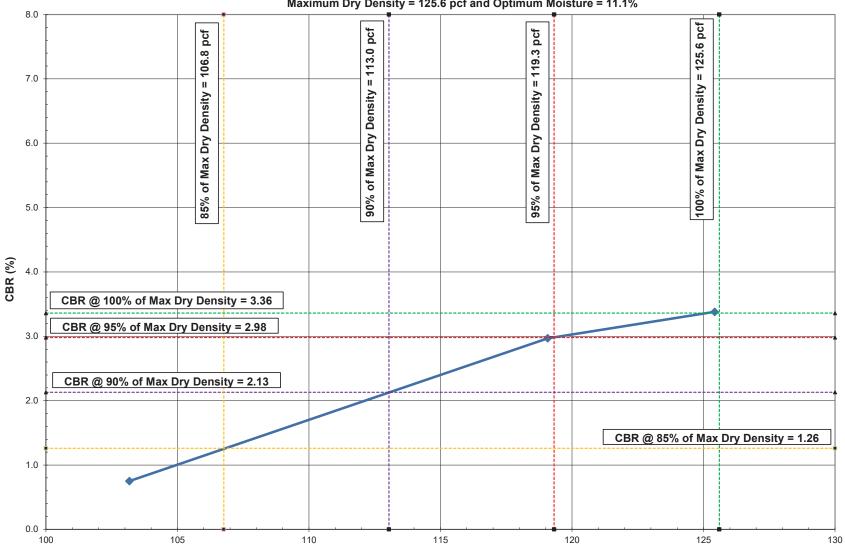
Boring/Pit B-19 Composite Sample - Modified Proctor (ASTM D-1557) Maximum Dry Density = 116.3 pcf and Optimum Moisture = 14.5%



Boring/Pit B-19 Composite Sample - Modified Proctor (ASTM D-1557) Maximum Dry Density = 116.3 pcf and Optimum Moisture = 14.5% 80 70 60 50 Stress (psi) 05 10 Blows 25 Blows 56 Blows 30 20 10 0 0.1 0.2 0.3 0.4 0.5 0.6 0

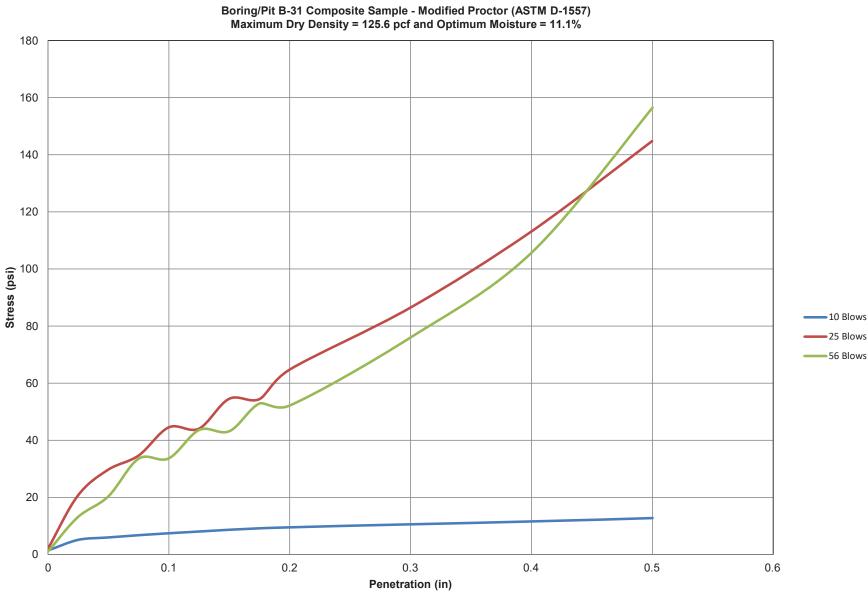
Penetration (in)

G103-21 HAS Taxiway L Geotechnical Investigation California Bearing Ratio (ASTM D-1883)

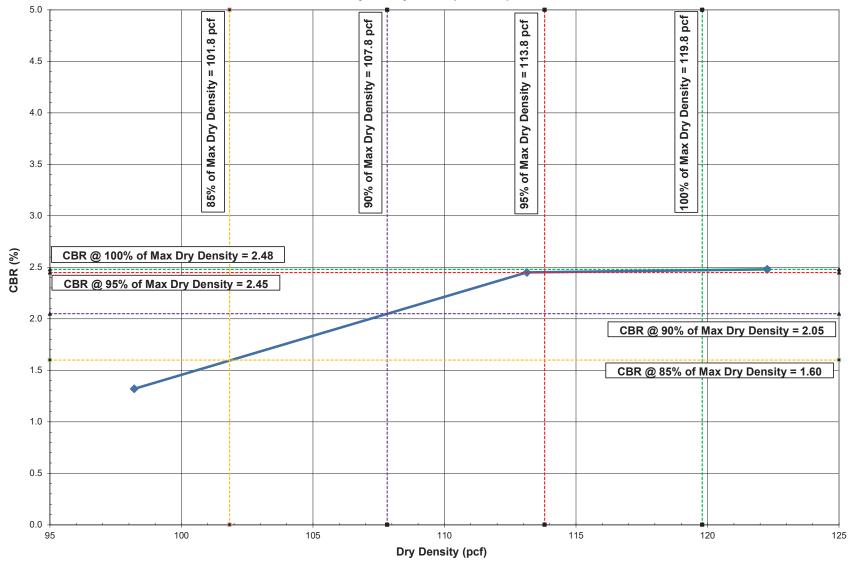


Boring/Pit B-31 Composite Sample - Modified Proctor (ASTM D-1557) Maximum Dry Density = 125.6 pcf and Optimum Moisture = 11.1%

Dry Density (pcf)



Boring/Pit B-44 Composite Sample - Modified Proctor (ASTM D-1557) Maximum Dry Density = 119.8 pcf and Optimum Moisture = 12.8%



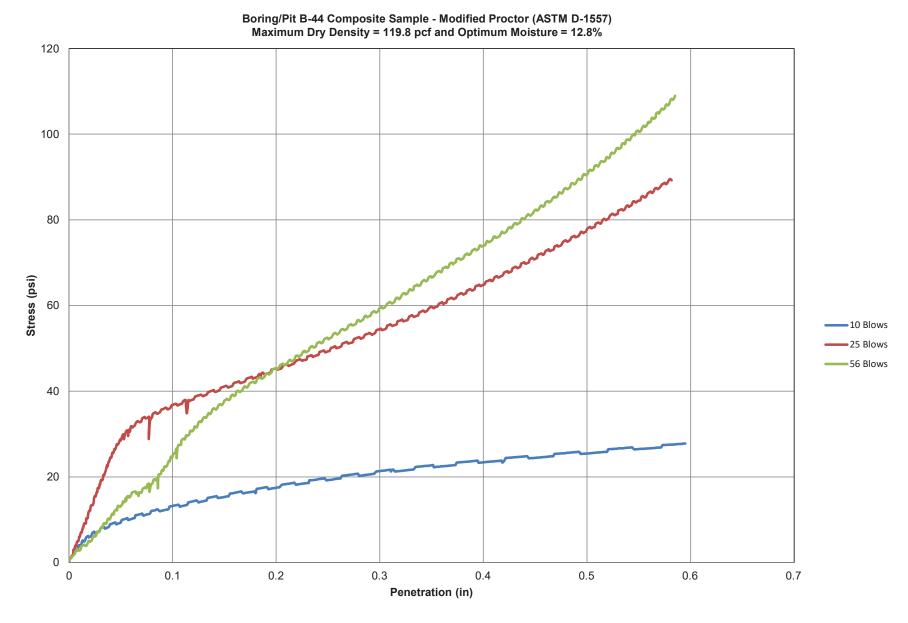
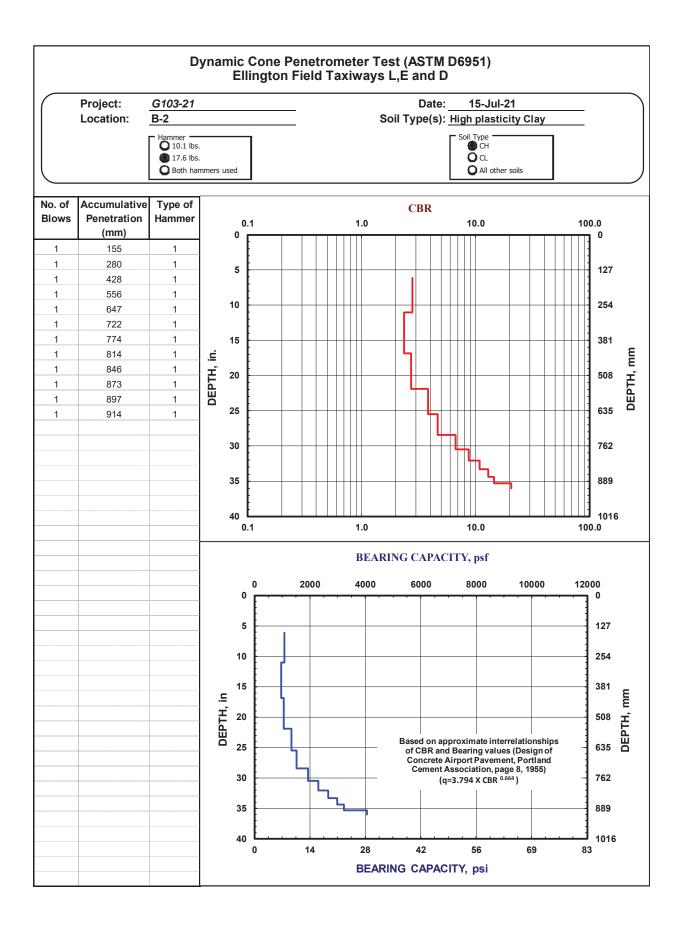
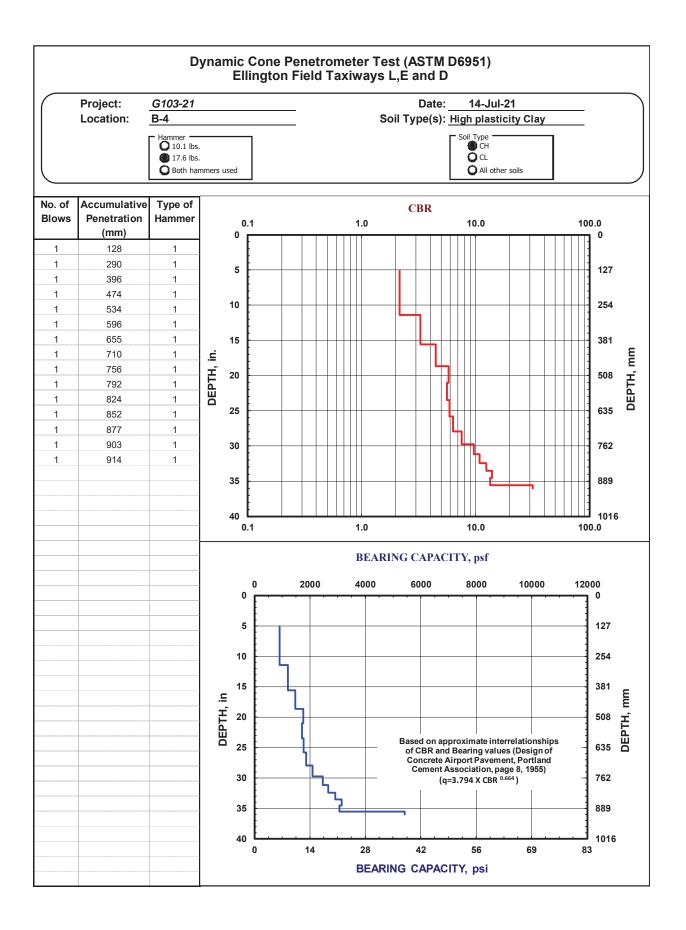
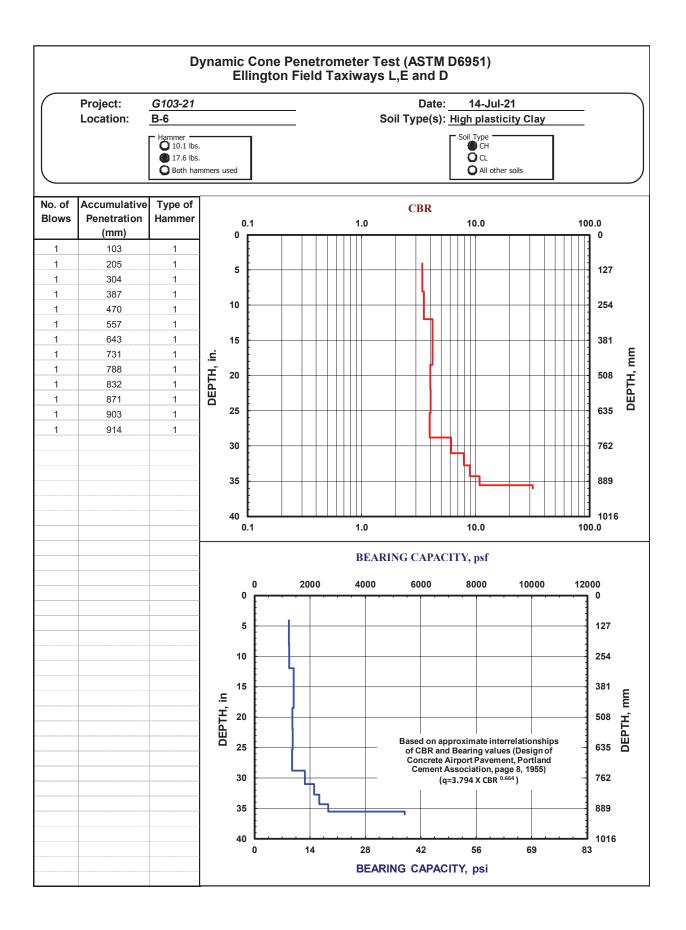
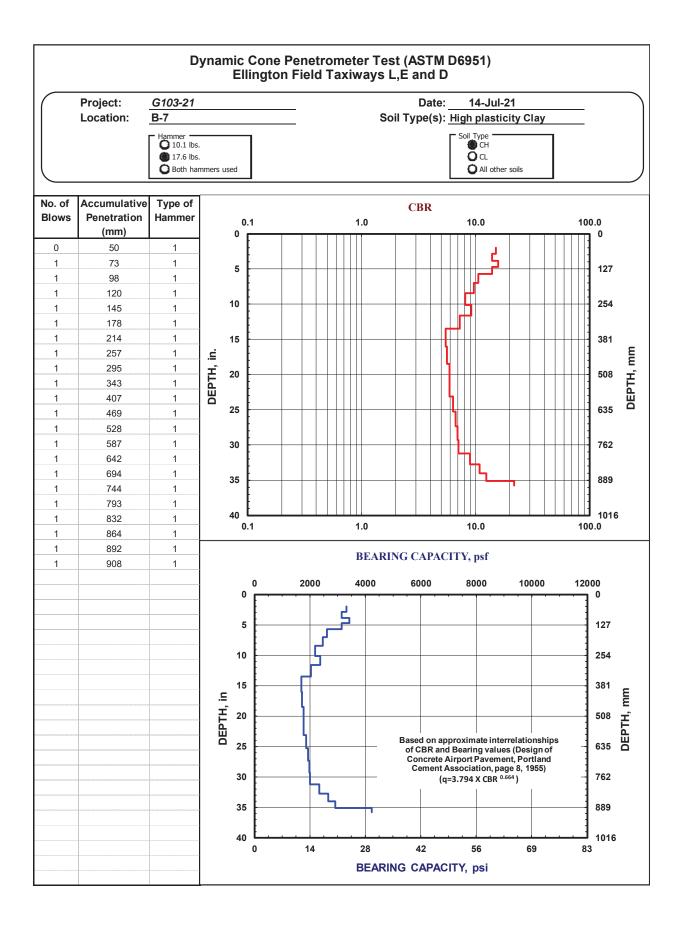


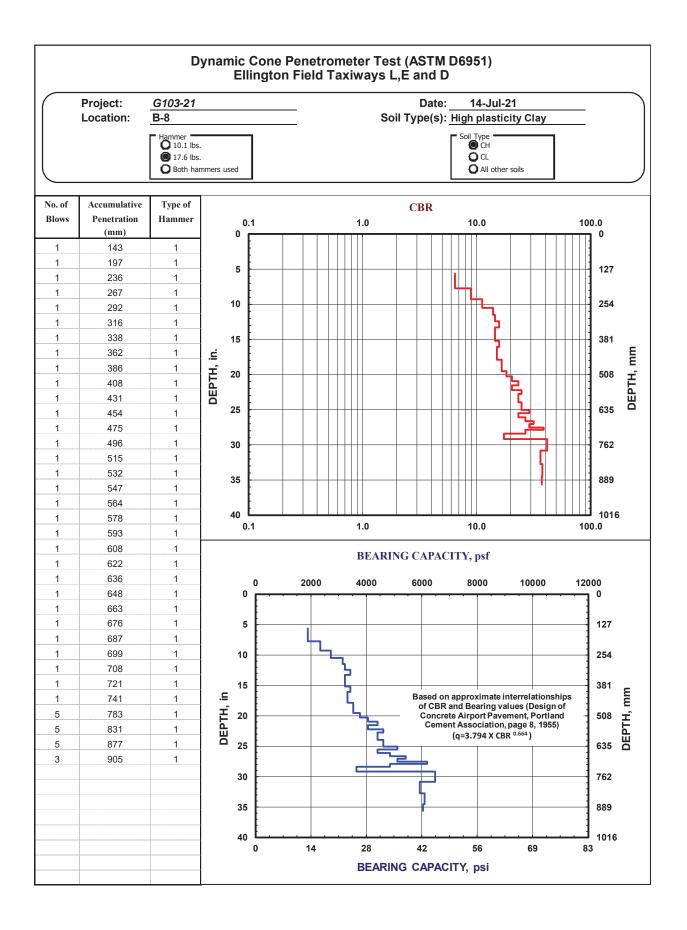
PLATE B-12

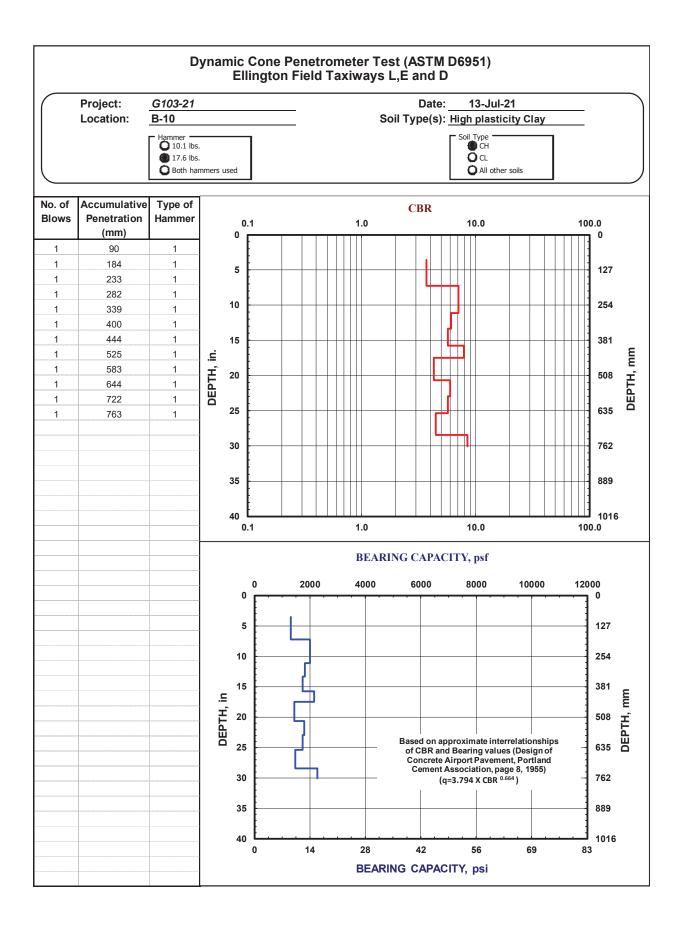


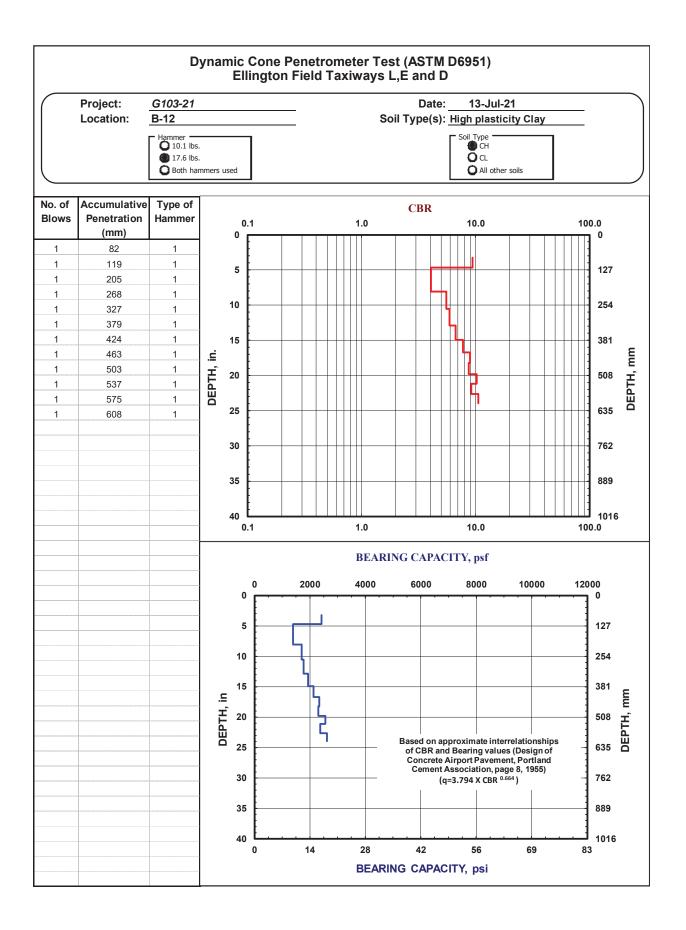


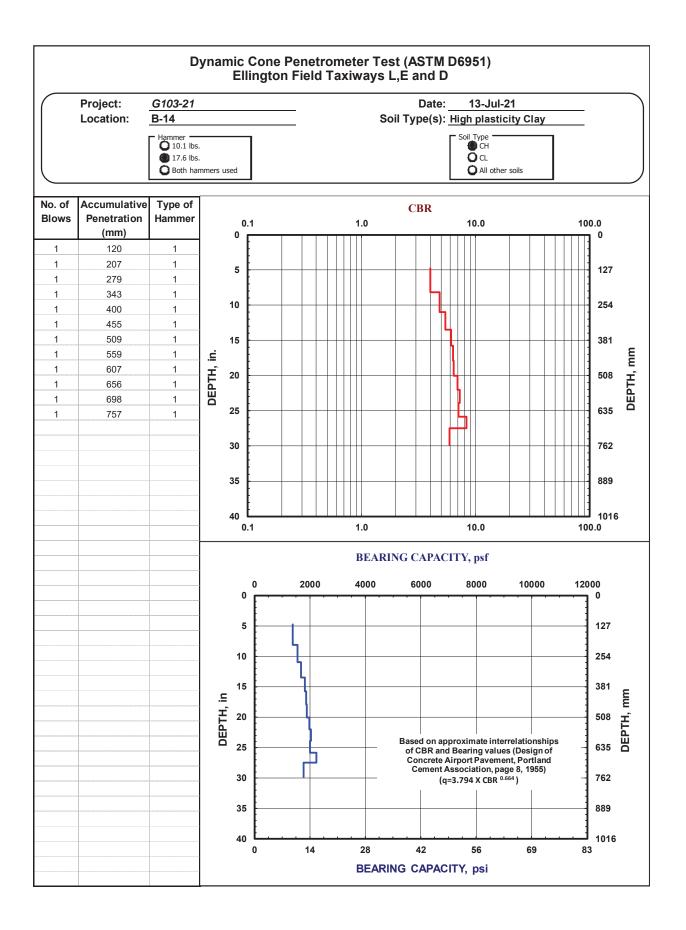


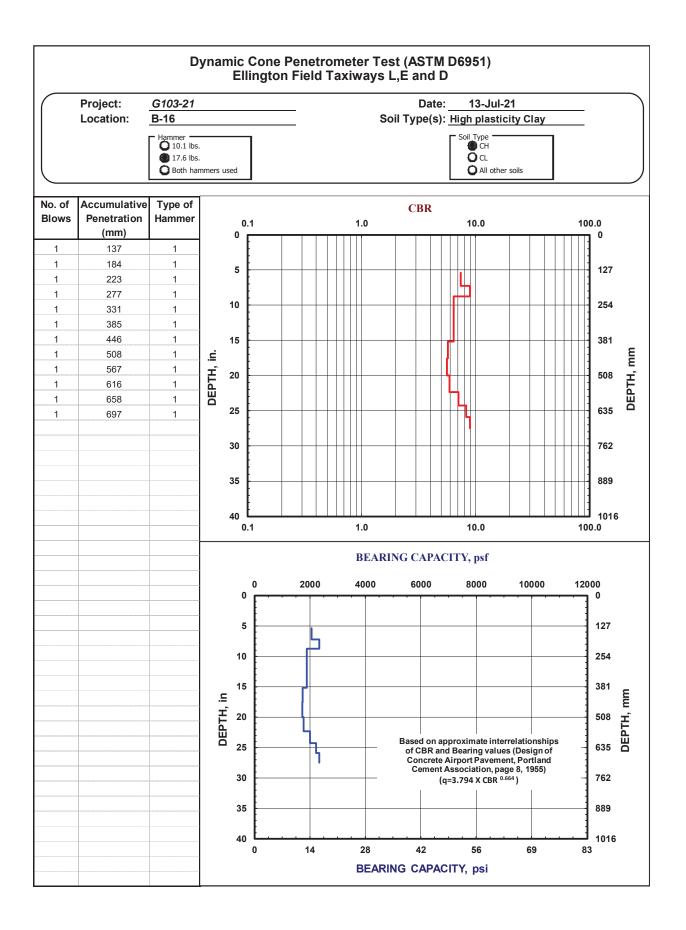


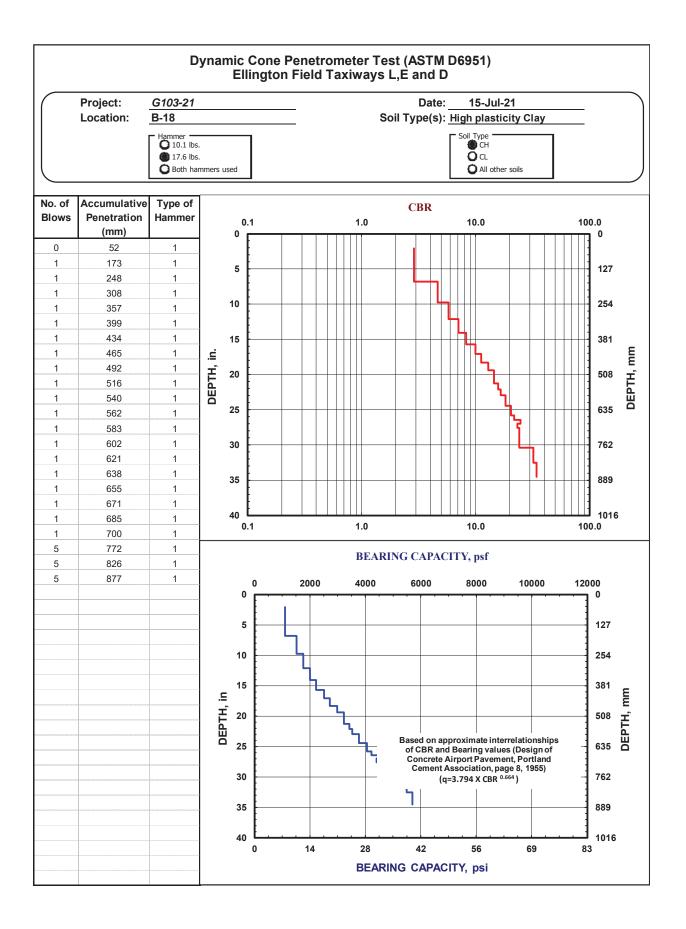


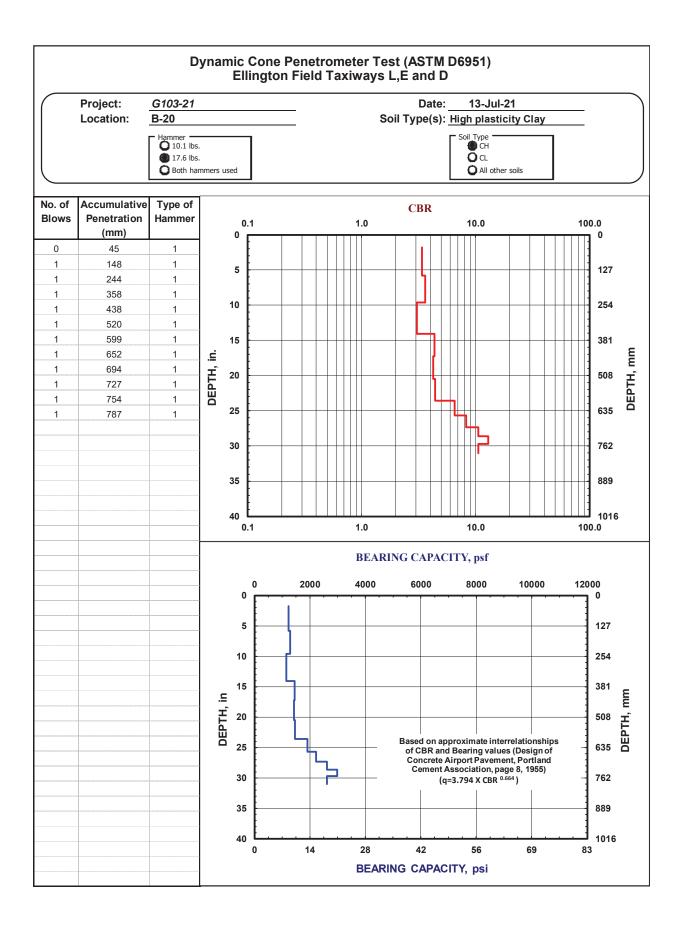


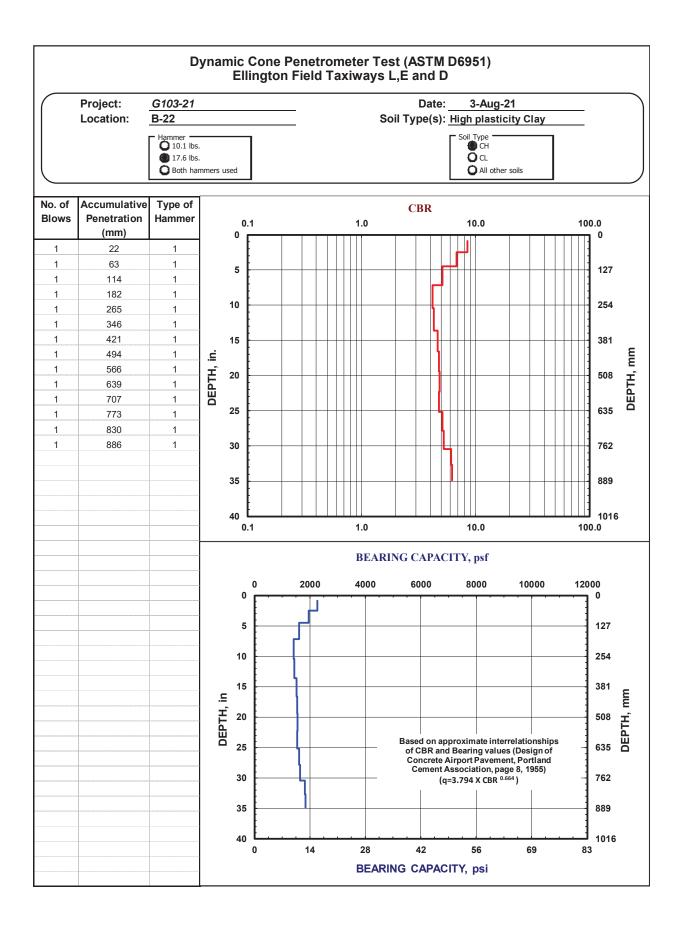


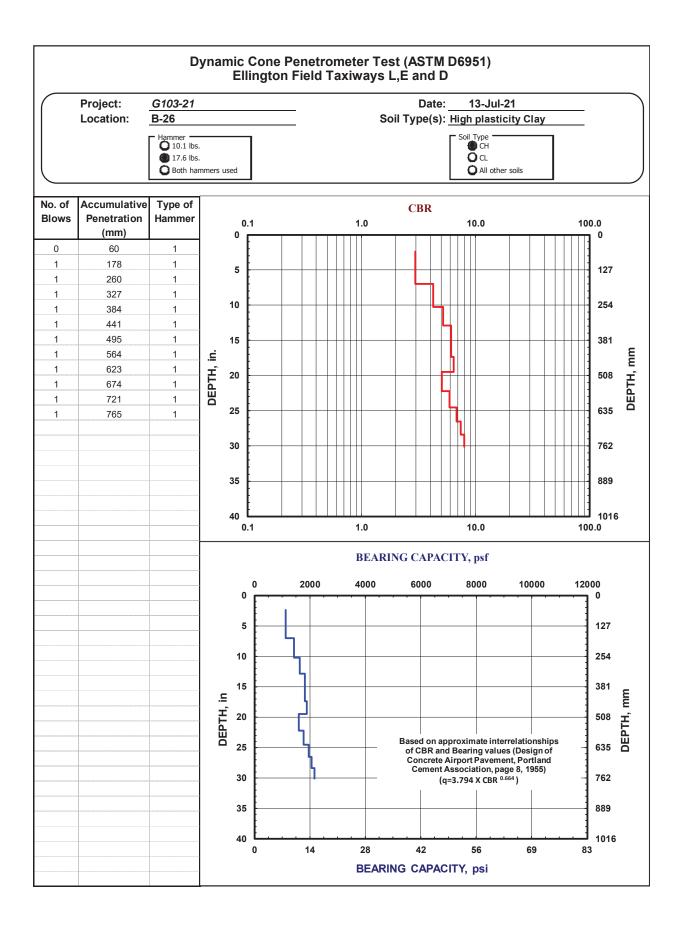


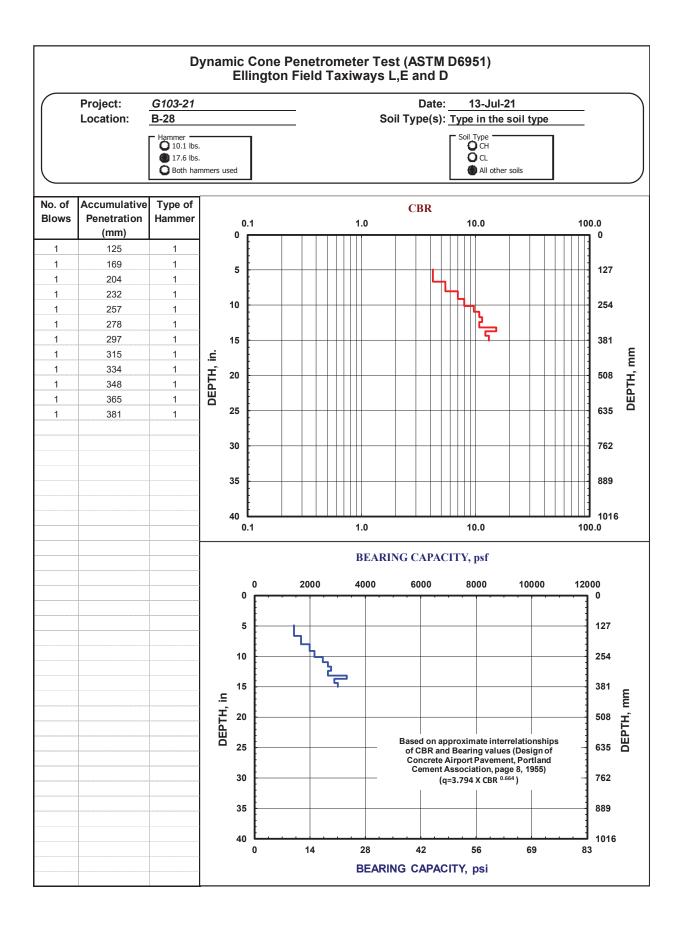


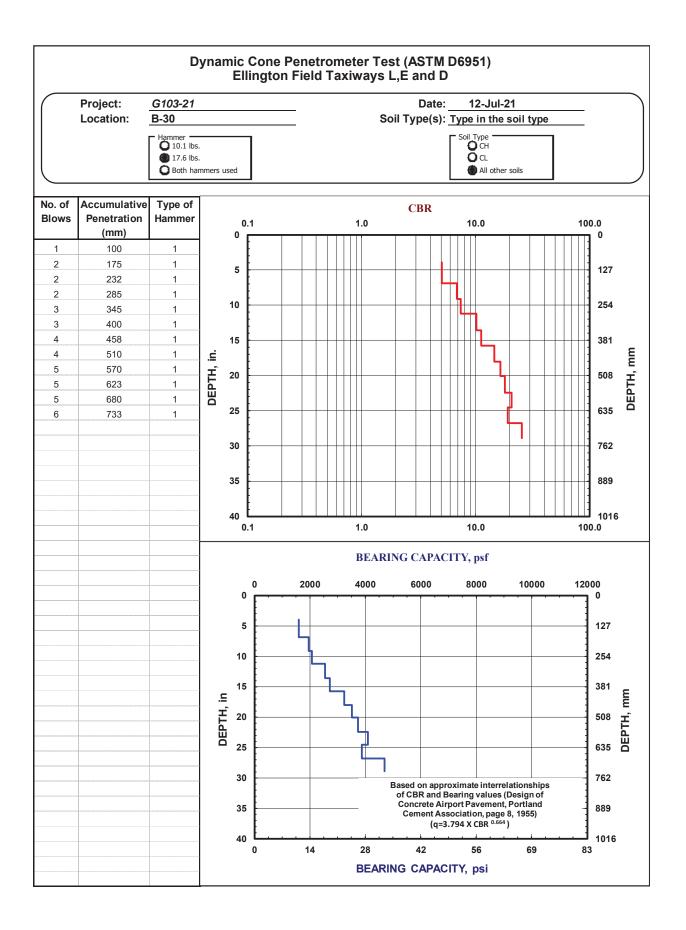


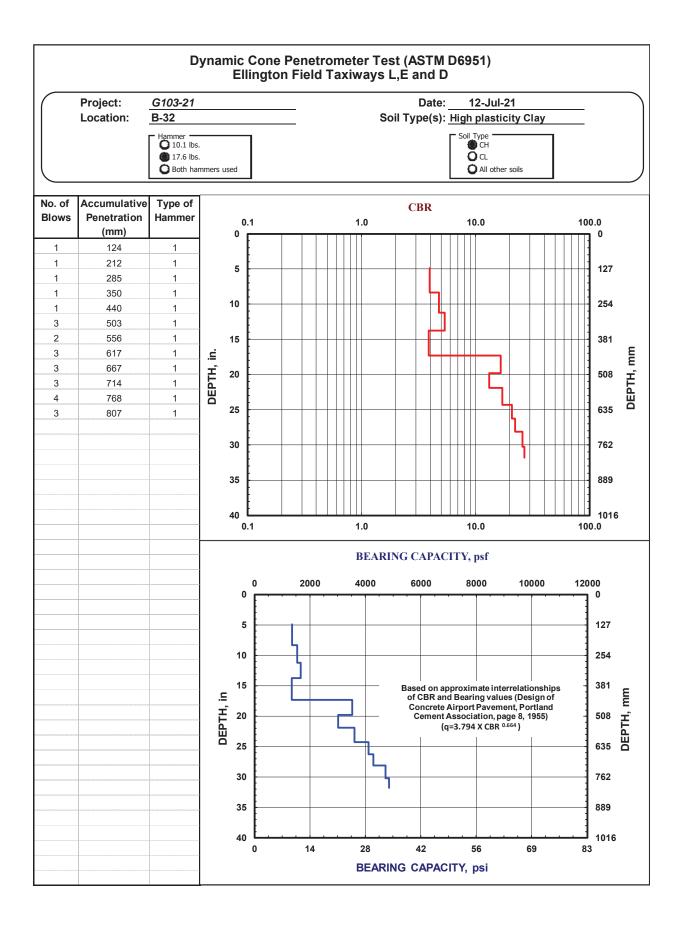


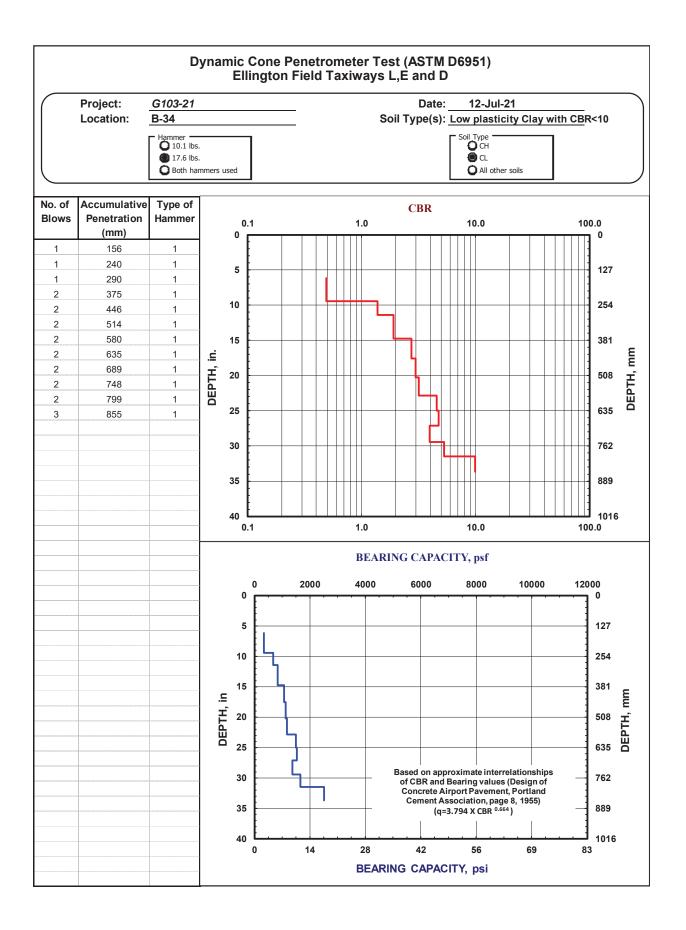


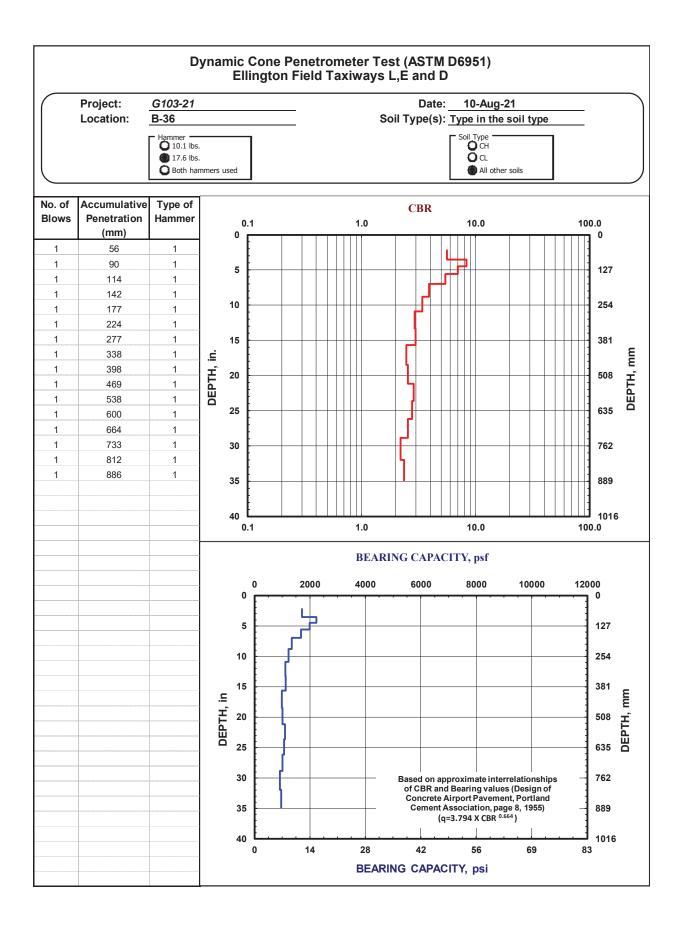


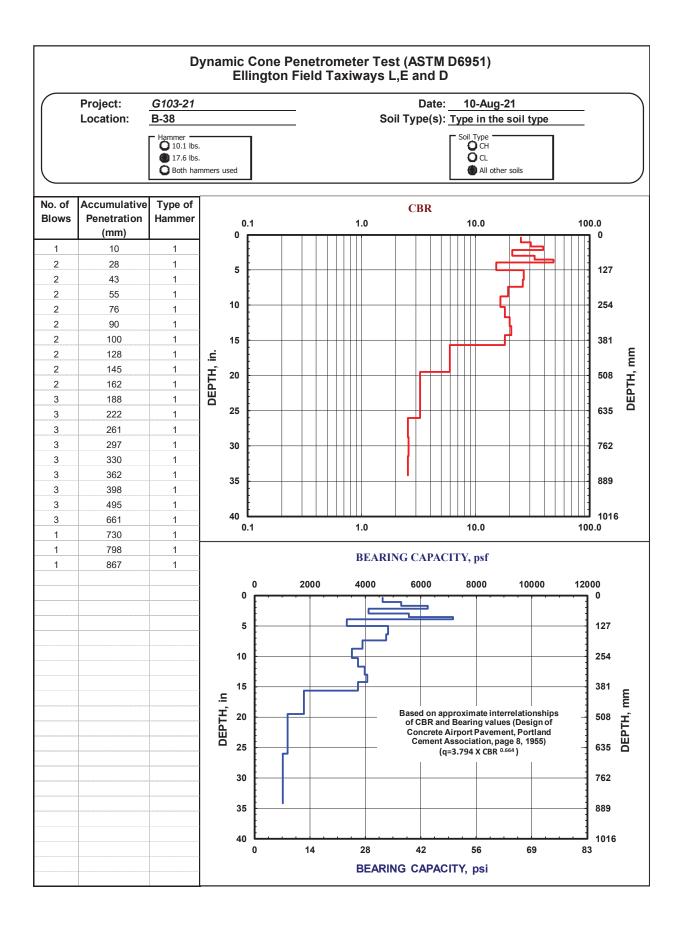


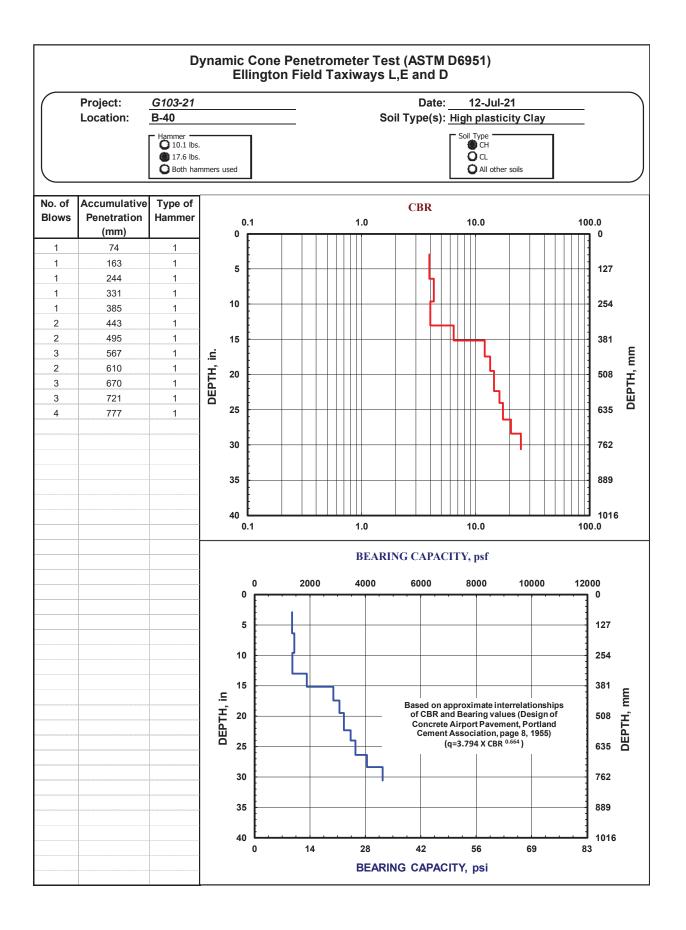


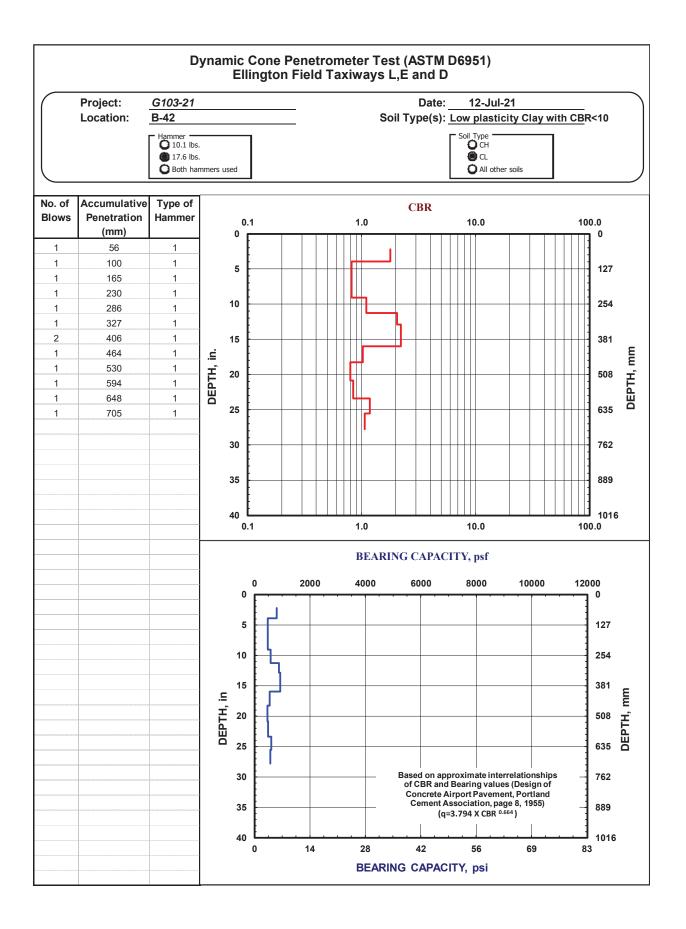


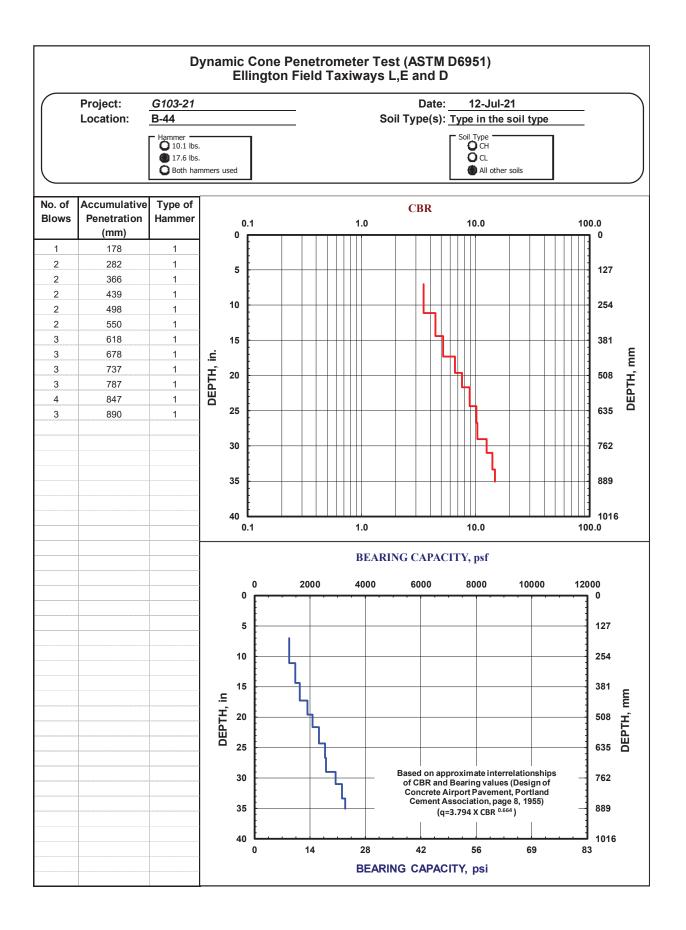


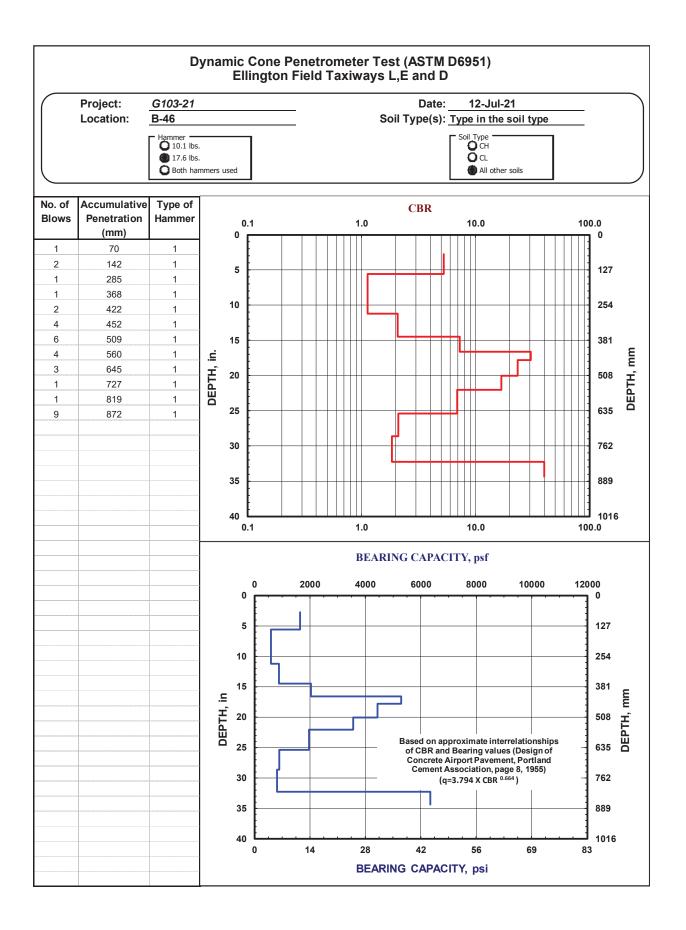


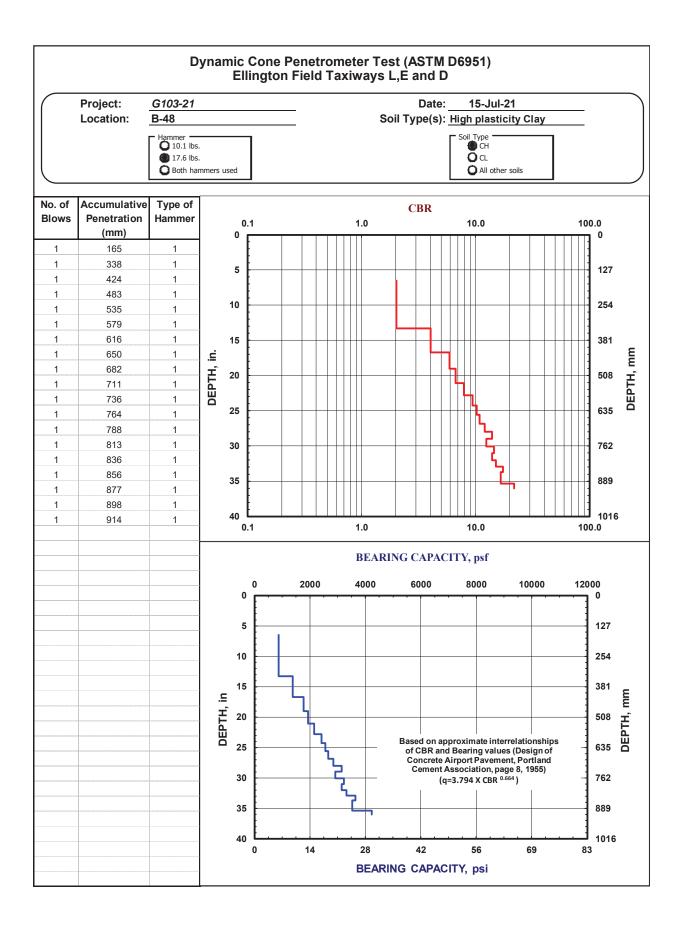


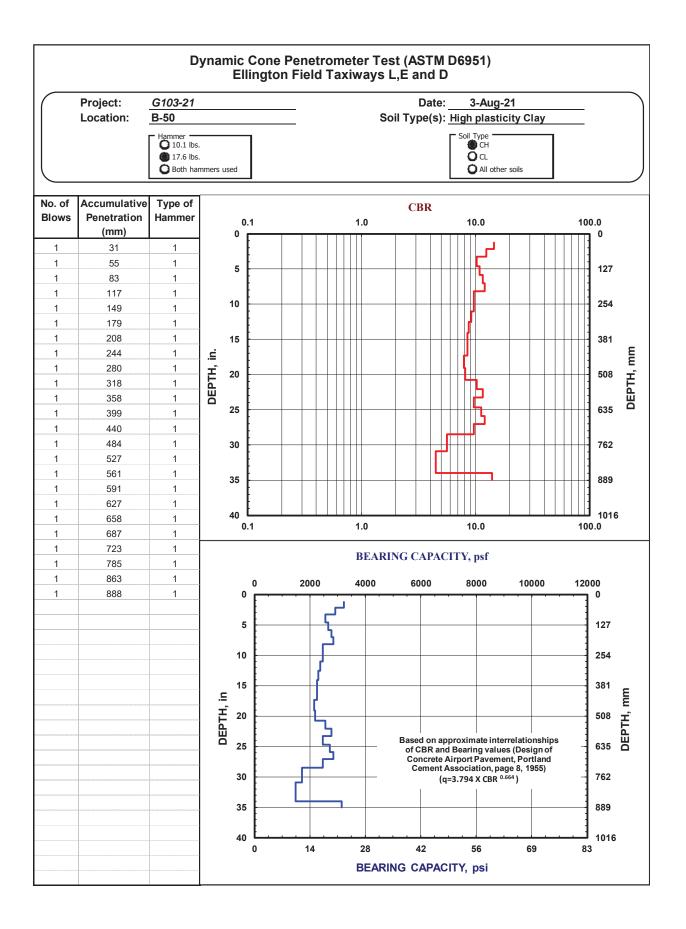


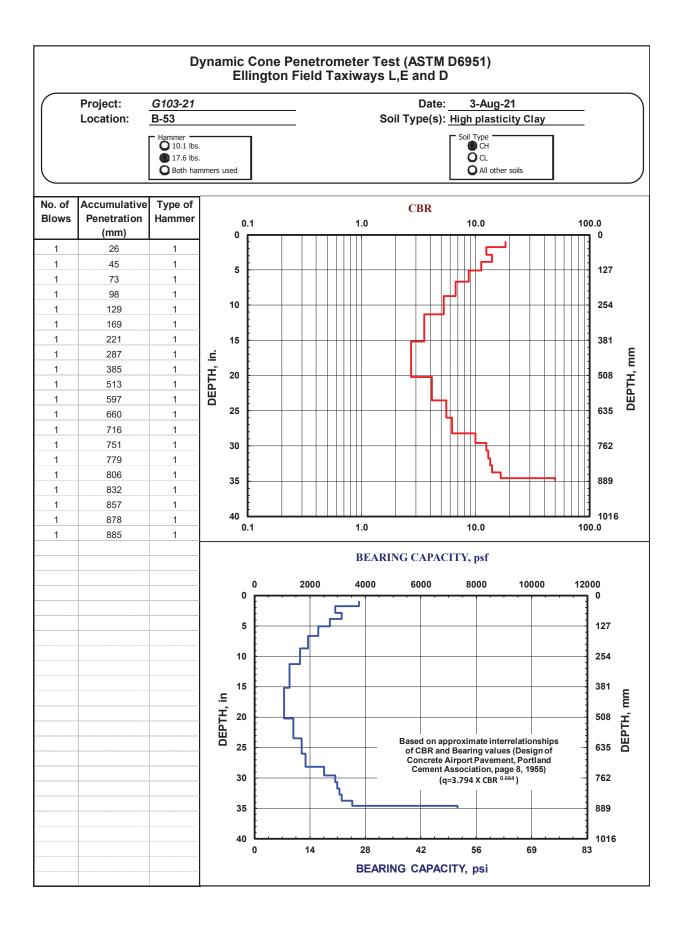


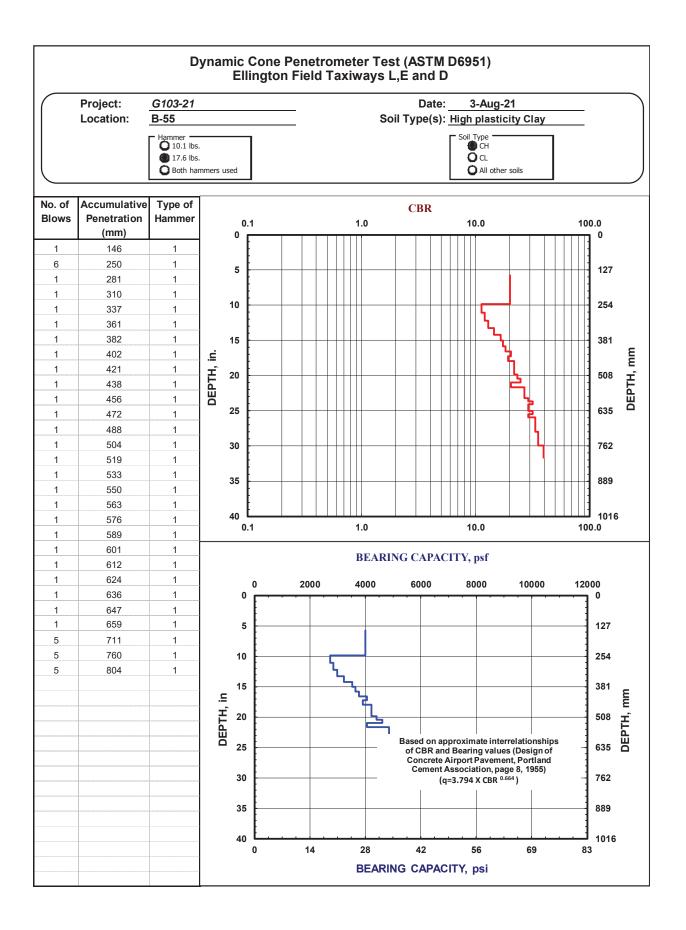


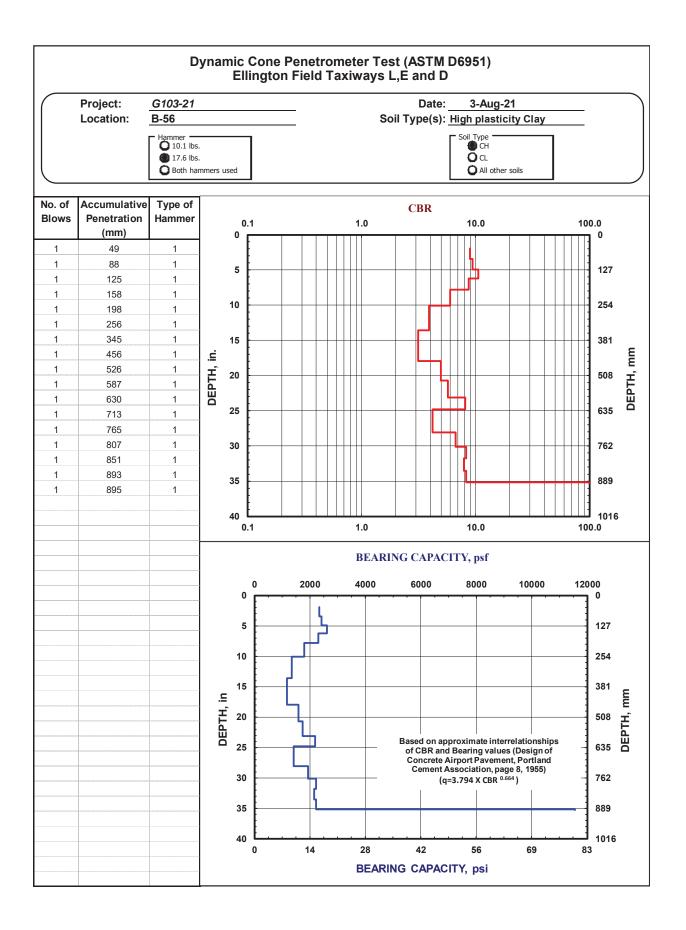


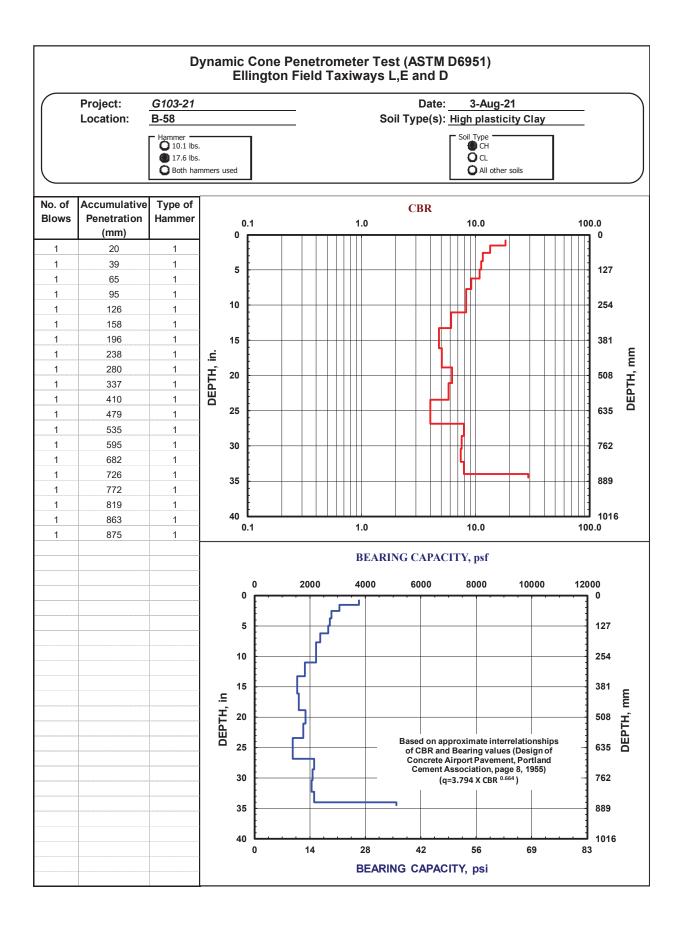


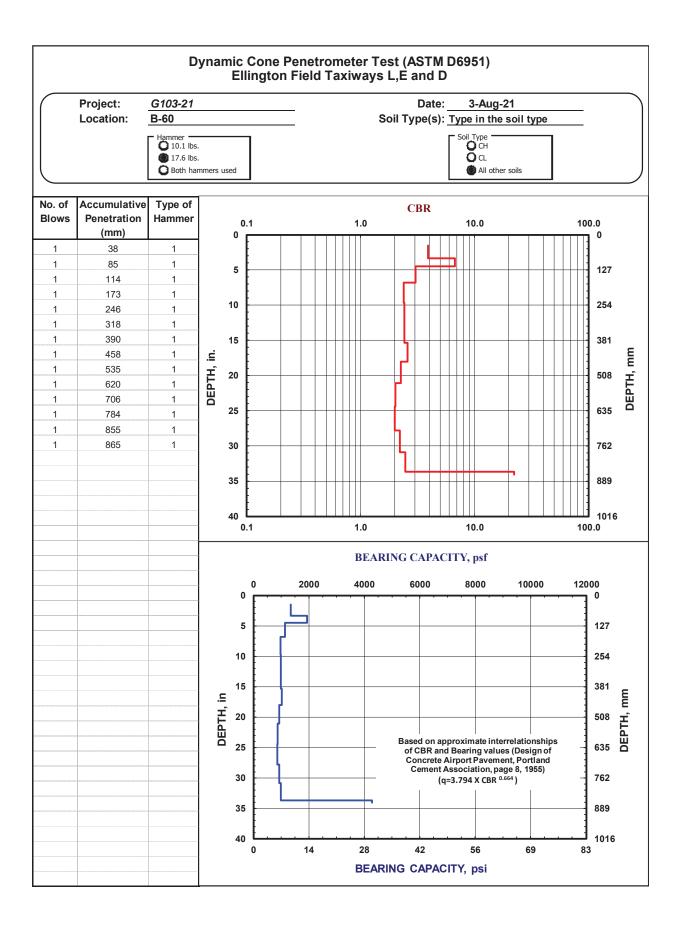


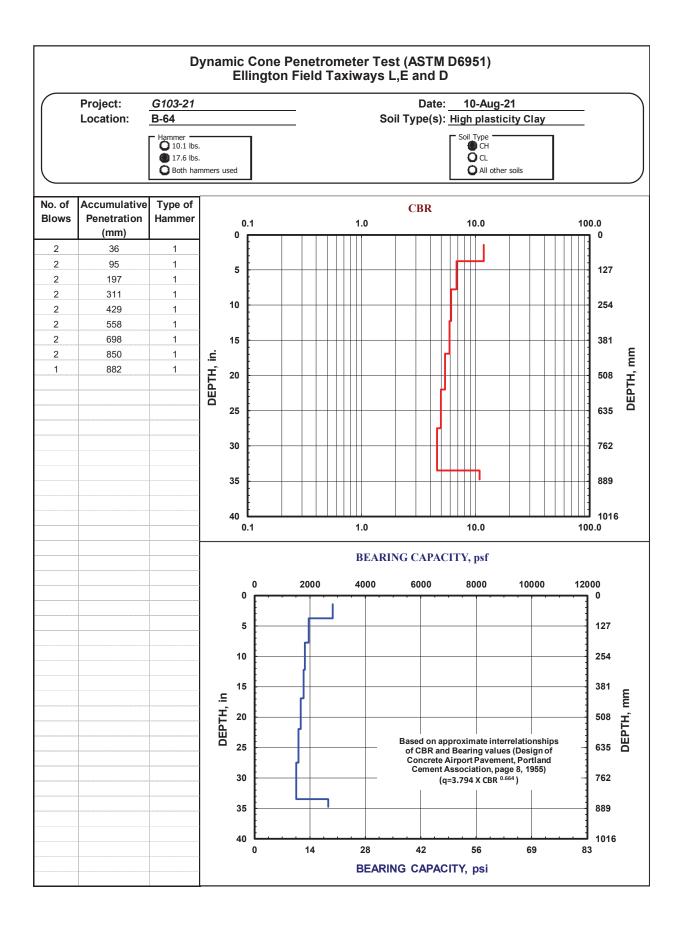


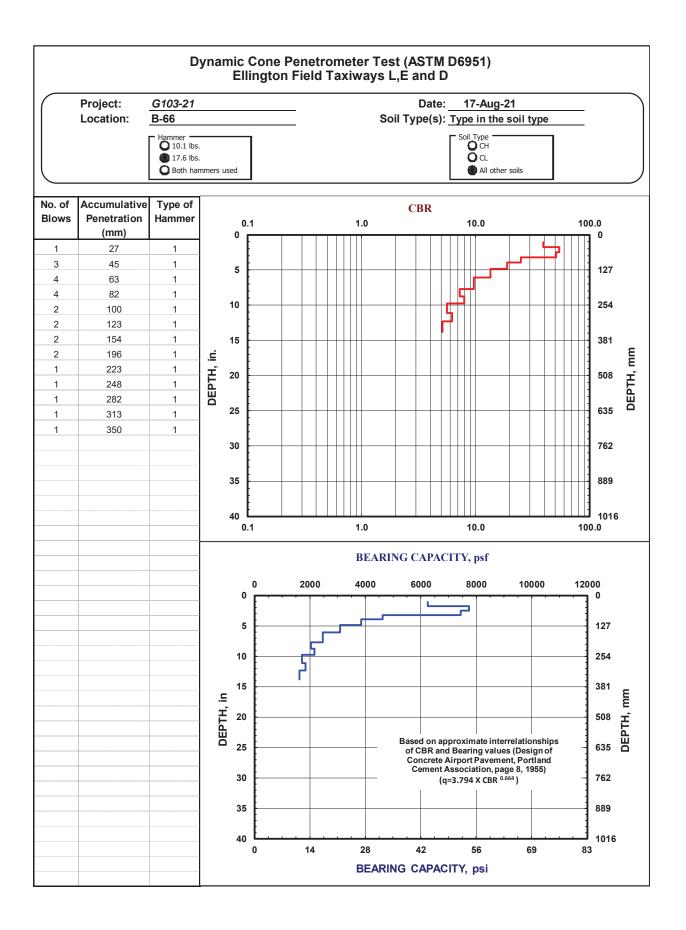


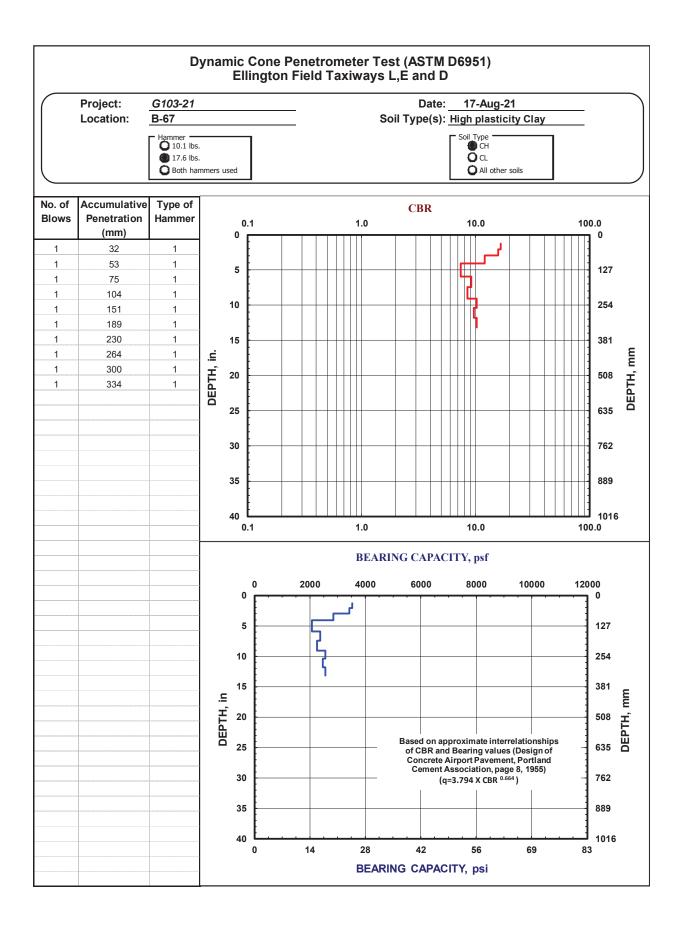


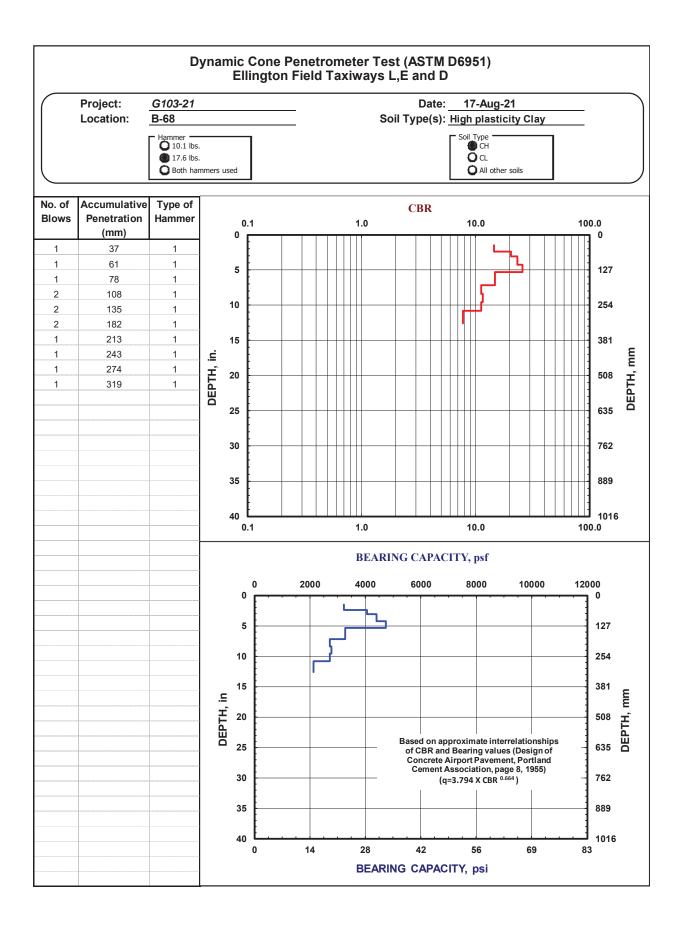


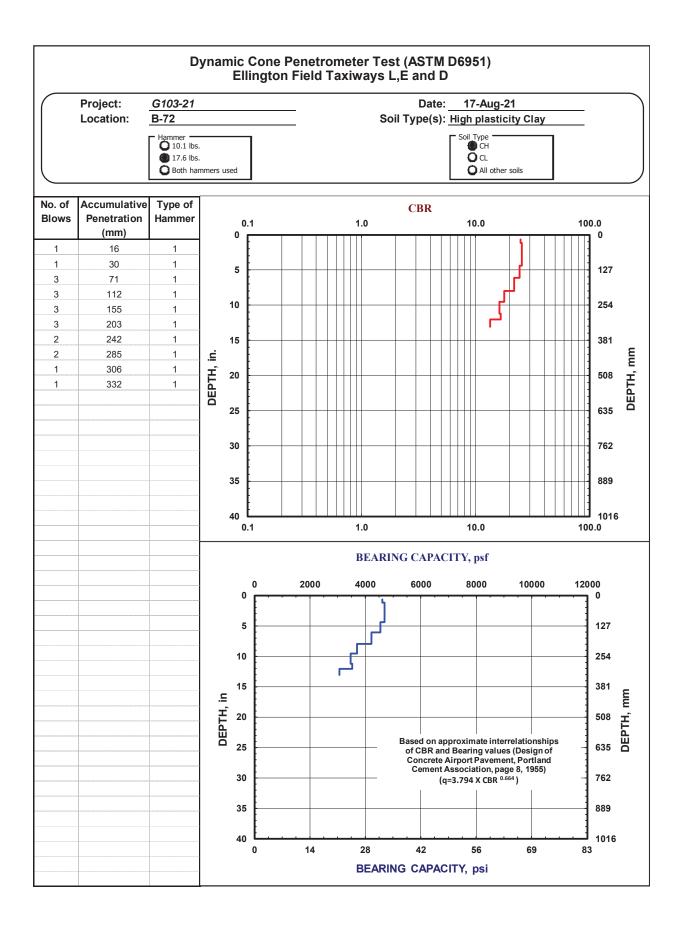


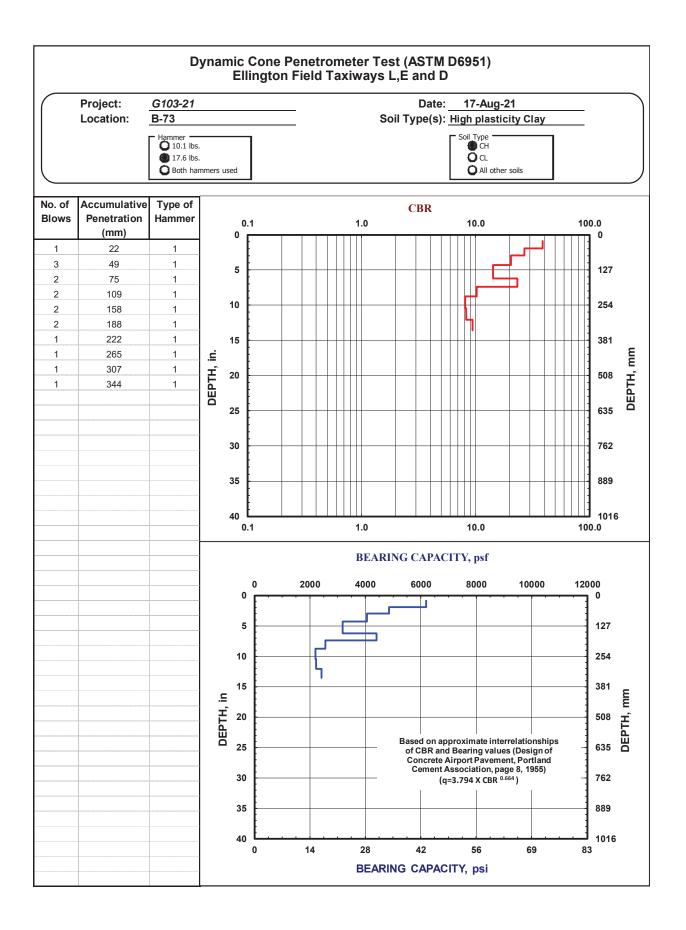


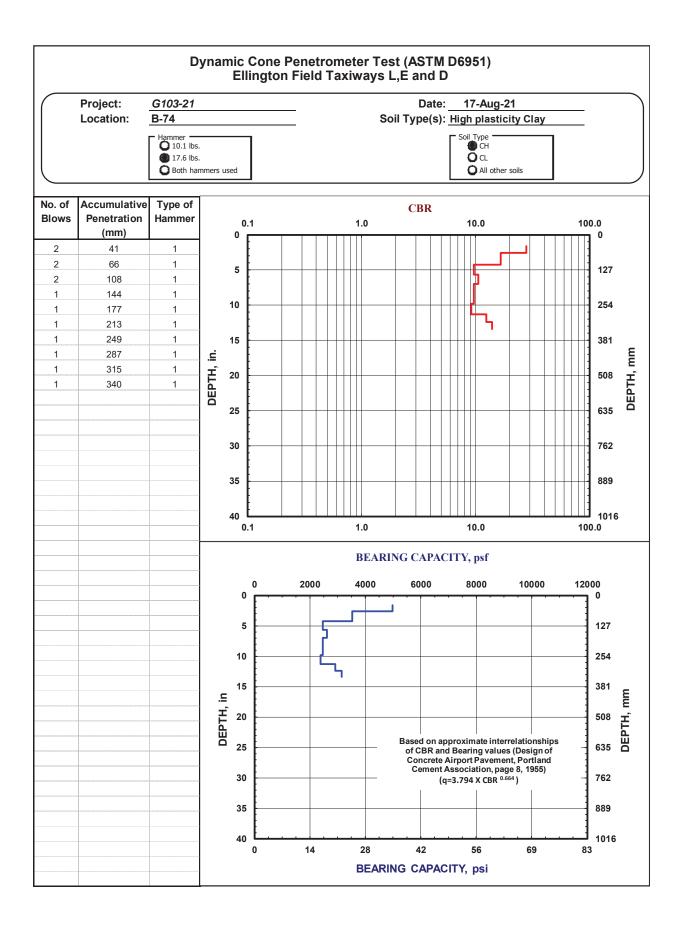














ILLUSTRATIONS

Plates 1 to 4 Pavement Core Photos





Photo 1 - Boring B-7



Photo 2 - Boring B-15





Photo 3 - Boring B-27



Photo 4 - Boring B-43





Photo 5 - Boring B-51



Photo 6 - Boring B-62



Photo 7 - Boring B-63





Photo 8 - Boring B-69



Photo 9 - Boring B-70



Photo 10 - Boring B-71





Appendix B – Fleet Mix Traffic

Taxiway L Fleet Mix

Aircraft Name	ADG	TDG	Entered into FAARFIELD as:	MTOW (lbs)	Average Annual Departures
Aero Spacelines Super Guppy	IV	TBD	D-200	170000	4
Airbus A310-200	IV	5	A310-200	317465	6
Airbus A330-200	V	5	A330-200 std	533519	50
Airbus Beluga XL	TBD	TBD	A330-200 std	500444	2
Boeing 727-200	- 111	4	Adv. B727-200 Option	209500	12
Boeing 747-200	v	5	B747-200B Combi Mixed / Belly	833000	50
Boeing 747-400	V	5	B747-400 / Belly	910000	25
Boeing 747-400 Dreamlifter	V	5	B747-400 / Belly	803001	2
Boeing 757-200	IV	4	B757-200	255500	24
Boeing 757-300	IV	4	B757-300	270000	6
Boeing 767-200	IV	5	B767-200	395000	6
Boeing 767-300	IV	5	B767-300	412000	18
Boeing 777-200	V	5	B777-200 ER	766000	25
Boeing 787-8 Dreamliner	V	5	B787-8	502500	25
Lockheed C-130 Hercules	IV	TBD	C-130	164000	185
Lockheed C-5B	VI	TBD	C-5	837000	75
McDonnell Douglas DC-10-10	IV	TBD	DC10-10	455000	6
Various Single Wheel (12,500 <mtow<=15,000)< td=""><td>VARIOUS</td><td>VARIOUS</td><td>S-15</td><td>15000</td><td>1793</td></mtow<=15,000)<>	VARIOUS	VARIOUS	S-15	15000	1793
Various Dual Wheel (12,500 <mtow<=15,000)< td=""><td>VARIOUS</td><td>VARIOUS</td><td>D-15</td><td>15000</td><td>32</td></mtow<=15,000)<>	VARIOUS	VARIOUS	D-15	15000	32
Various Single Wheel (15,000 <mtow<=25,000)< td=""><td>VARIOUS</td><td>VARIOUS</td><td>S-25</td><td>25000</td><td>455</td></mtow<=25,000)<>	VARIOUS	VARIOUS	S-25	25000	455
Various Dual Wheel (15,000 <mtow<=25,000)< td=""><td>VARIOUS</td><td>VARIOUS</td><td>D-25</td><td>25000</td><td>335</td></mtow<=25,000)<>	VARIOUS	VARIOUS	D-25	25000	335
Various Single Wheel (25,000 <mtow<=50,000)< td=""><td>VARIOUS</td><td>VARIOUS</td><td>S-50</td><td>50000</td><td>2</td></mtow<=50,000)<>	VARIOUS	VARIOUS	S-50	50000	2
Various Dual Wheel (25,000 <mtow<=50,000)< td=""><td>VARIOUS</td><td>VARIOUS</td><td>D-50</td><td>50000</td><td>529</td></mtow<=50,000)<>	VARIOUS	VARIOUS	D-50	50000	529
Various Dual Wheel (50,000 <mtow<=75,000)< td=""><td>VARIOUS</td><td>VARIOUS</td><td>D-75</td><td>75000</td><td>58</td></mtow<=75,000)<>	VARIOUS	VARIOUS	D-75	75000	58
Various Dual Wheel (75,000 <mtow<=100,000)< td=""><td>VARIOUS</td><td>VARIOUS</td><td>D-100</td><td>100000</td><td>113</td></mtow<=100,000)<>	VARIOUS	VARIOUS	D-100	100000	113
Various Dual Wheel (100,000 <mtow<=150,000)< td=""><td>VARIOUS</td><td>VARIOUS</td><td>D-150</td><td>150000</td><td>3</td></mtow<=150,000)<>	VARIOUS	VARIOUS	D-150	150000	3
Various Dual Wheel (150,000 <mtow<=200,000)< td=""><td>VARIOUS</td><td>VARIOUS</td><td>D-200</td><td>200000</td><td>73</td></mtow<=200,000)<>	VARIOUS	VARIOUS	D-200	200000	73





Appendix C – FAARFIELD Reports

EFD Taxiway L - Preliminary Pavement Design Memo

Federal Aviation Administration FAARFIELD 2.0 Section Report

FAARFIELD 2.0.3 (Build 04/30/2021)

Job Name: EFD Taxiway L - Pavement Options_Updated

Section: Option 1 - CBR = 1

Analysis Type: New Rigid

Last Run: Thickness Design 2021-10-28 15:02:00

Design Life = 30 Years

Total thickness to the top of the subgrade = 47.4in.

Pavement Structure Information by Layer

No.	Туре	Thickness in.	Modulus psi	Poisson's Ratio	Strength R psi
1	P-501 PCC Surface	17.4	4000000	0.15	700.0
2	User Defined	6.0	250000	0.35	0
3	P-304 Cement Treated Base	12.0	500000	0.35	0
4	User Defined	12.0	1500	0.35	0
5	Subgrade	0	1500	0.4	0

Airplane Information

No.	Name	Gross Wt. Ibs	Annual Departures	% Annual Growth
1	D-200	200000	5	0
2	A310-200	315041	10	0
3	A330-200 WV020	509050	50	0
4	A330-300 std	509050	50	0
5	B727-200 Advanced Option	210000	15	0
6	B747-200/300	836000	50	0
7	B747-200/300 Belly	836000	50	0
8	B747-400	877000	25	0
9	B747-400 Belly	877000	25	0
10	B757-200	256000	25	0
11	B757-300	271000	10	0
12	B767-200	368000	10	0
13	B767-300	352000	20	0
14	B777-200 ER	658000	25	0
15	B787-8	503500	25	0
16	C-130	155000	200	0
17	C-5	769000	75	0
18	DC/MD-10-10/10F	458000	10	0
19	MD-11	633000	10	0
20	MD-11 Belly	633000	10	0
21	S-15	15000	1800	0
22	S-25	25000	35	0
23	S-50	50000	500	0
24	D-15	15000	350	0
25	D-25	25000	5	0
26	D-50	50000	530	0
27	D-75	75000	60	0
28	D-100	100000	115	0
29	D-150	150000	5	0
30	D-200	200000	75	0

Additional Airplane Information

No.	Name	CDF Contribution	CDF Max for Airplane	P/C Ratio
1	D-200	0.00	0.00	3.29
2	A310-200	0.00	0.00	3.69
3	A330-200 WV020	0.23	0.23	1.98
4	A330-300 std	0.23	0.23	1.88
5	B727-200 Advanced Option	0.00	0.00	2.97
6	B747-200/300	0.03	0.03	3.46
7	B747-200/300 Belly	0.00	0.03	3.47
8	B747-400	0.03	0.03	3.47
9	B747-400 Belly	0.00	0.03	3.47
10	B757-200	0.00	0.00	3.92
11	B757-300	0.00	0.00	3.93
12	B767-200	0.00	0.00	3.73
13	B767-300	0.00	0.00	3.86
14	B777-200 ER	0.20	0.20	4.05
15	B787-8	0.19	0.20	3.77
16	C-130	0.00	0.00	4.67
17	C-5	0.00	0.00	1.41
18	DC/MD-10-10/10F	0.01	0.01	3.8
19	MD-11	0.07	0.07	3.67
20	MD-11 Belly	0.00	0.00	3.01
21	S-15	0.00	0.00	3.6
22	S-25	0.00	0.00	3.94
23	S-50	0.00	0.00	2.73
24	D-15	0.00	0.00	5.48
25	D-25	0.00	0.00	5.03
26	D-50	0.00	0.00	3.73
27	D-75	0.00	0.00	3.6
28	D-100	0.00	0.00	3.55
29	D-150	0.00	0.00	3.28
30	D-200	0.00	0.00	3.29

User Is responsible For checking frost protection requirements.

P-501 PCC Surface	T=17.4 inches 🔂 R=700 psi
Z	
~ ⊿.	Р
User Defined	T=6.0 inches E=250000 psi
P-304 Cement Treated Base	T=12.0 inches E=500000 psi
User Defined	T=12.0 inches E=1500 psi
Subgrade	k=28.7 pci E=1500 psi

Federal Aviation Administration FAARFIELD 2.0 Section Report

FAARFIELD 2.0.3 (Build 04/30/2021)

Job Name: EFD Taxiway L - Pavement Options_Updated

Section: Option 1 - CBR = 5

Analysis Type: New Rigid

Last Run: Thickness Design 2021-10-28 15:18:25

Design Life = 30 Years

Total thickness to the top of the subgrade = 43.6in.

Pavement Structure Information by Layer

No.	Туре	Thickness in.	Modulus psi	Poisson's Ratio	Strength R psi
1	P-501 PCC Surface	13.6	4000000	0.15	700.0
2	User Defined	6.0	250000	0.35	0
3	P-304 Cement Treated Base	12.0	500000	0.35	0
4	User Defined	12.0	7500	0.35	0
5	Subgrade	0	7500	0.4	0

Airplane Information

No.	Name	Gross Wt. lbs	Annual Departures	% Annual Growth
1	D-200	200000	5	0
2	A310-200	315041	10	0
3	A330-200 WV020	509050	50	0
4	A330-300 std	509050	50	0
5	B727-200 Advanced Option	210000	15	0
6	B747-200/300	836000	50	0
7	B747-200/300 Belly	836000	50	0
8	B747-400	877000	25	0
9	B747-400 Belly	877000	25	0
10	B757-200	256000	25	0
11	B757-300	271000	10	0
12	B767-200	368000	10	0
13	B767-300	352000	20	0
14	B777-200 ER	658000	25	0
15	B787-8	503500	25	0
16	C-130	155000	200	0
17	C-5	769000	75	0
18	DC/MD-10-10/10F	458000	10	0
19	MD-11	633000	10	0
20	MD-11 Belly	633000	10	0
21	S-15	15000	1800	0
22	S-25	25000	35	0
23	S-50	50000	500	0
24	D-15	15000	350	0
25	D-25	25000	5	0
26	D-50	50000	530	0
27	D-75	75000	60	0
28	D-100	100000	115	0
29	D-150	150000	5	0
30	D-200	200000	75	0

Additional Airplane Information

No.	Name	CDF Contribution	CDF Max for Airplane	P/C Ratio
1	D-200	0.00	0.00	3.29
2	A310-200	0.00	0.00	3.69
3	A330-200 WV020	0.18	0.18	1.98
4	A330-300 std	0.14	0.14	1.88
5	B727-200 Advanced Option	0.00	0.00	2.97
6	B747-200/300	0.03	0.03	3.46
7	B747-200/300 Belly	0.00	0.03	3.47
8	B747-400	0.04	0.04	3.47
9	B747-400 Belly	0.00	0.04	3.47
10	B757-200	0.00	0.00	3.92
11	B757-300	0.00	0.00	3.93
12	B767-200	0.00	0.00	3.73
13	B767-300	0.00	0.00	3.86
14	B777-200 ER	0.24	0.24	4.05
15	B787-8	0.29	0.30	3.77
16	C-130	0.00	0.00	4.67
17	C-5	0.00	0.00	1.41
18	DC/MD-10-10/10F	0.01	0.01	3.8
19	MD-11	0.07	0.07	3.67
20	MD-11 Belly	0.00	0.00	3.01
21	S-15	0.00	0.00	3.6
22	S-25	0.00	0.00	3.94
23	S-50	0.00	0.00	2.73
24	D-15	0.00	0.00	5.48
25	D-25	0.00	0.00	5.03
26	D-50	0.00	0.00	3.73
27	D-75	0.00	0.00	3.6
28	D-100	0.00	0.00	3.55
29	D-150	0.00	0.00	3.28
30	D-200	0.00	0.01	3.29

User Is responsible For checking frost protection requirements.

P-501 PCC Surface	T=13.6 inches	R=700 psi
<i>d</i> .		7
User Defined	T=6.0 inches	E=250000 psi
P-304 Cement Treated Base	T=12.0 inches	E=500000 psi
User Defined	T=12.0 inches	E=7500 psi
Subgrade	k=100.5 pci	E=7500 psi

Federal Aviation Administration FAARFIELD 2.0 Section Report

FAARFIELD 2.0.3 (Build 04/30/2021)

Job Name: EFD Taxiway L - Pavement Options_Updated

Section: Option 2 - CBR = 1

Analysis Type: New Rigid

Last Run: Thickness Design 2021-10-28 17:56:01

Design Life = 30 Years

Total thickness to the top of the subgrade = 50.9in.

Pavement Structure Information by Layer

No.	Туре	Thickness in.	Modulus psi	Poisson's Ratio	Strength R psi
1	P-501 PCC Surface	16.9	4000000	0.15	700.0
2	User Defined	6.0	250000	0.35	0
3	P-304 Cement Treated Base	16.0	500000	0.35	0
4	User Defined	12.0	1500	0.35	0
5	Subgrade	0	1500	0.4	0

Airplane Information

No.	Name	Gross Wt. lbs	Annual Departures	% Annual Growth
1	D-200	200000	5	0
2	A310-200	315041	10	0
3	A330-200 WV020	509050	50	0
4	A330-300 std	509050	50	0
5	B727-200 Advanced Option	210000	15	0
6	B747-200/300	836000	50	0
7	B747-200/300 Belly	836000	50	0
8	B747-400	877000	25	0
9	B747-400 Belly	877000	25	0
10	B757-200	256000	25	0
11	B757-300	271000	10	0
12	B767-200	368000	10	0
13	B767-300	352000	20	0
14	B777-200 ER	658000	25	0
15	B787-8	503500	25	0
16	C-130	155000	200	0
17	C-5	769000	75	0
18	DC/MD-10-10/10F	458000	10	0
19	MD-11	633000	10	0
20	MD-11 Belly	633000	10	0
21	S-15	15000	1800	0
22	S-25	25000	35	0
23	S-50	50000	500	0
24	D-15	15000	350	0
25	D-25	25000	5	0
26	D-50	50000	530	0
27	D-75	75000	60	0
28	D-100	100000	115	0
29	D-150	150000	5	0
30	D-200	200000	75	0

Additional Airplane Information

No.	Name	CDF Contribution	CDF Max for Airplane	P/C Ratio	
1	D-200	0.00	0.00	3.29	
2	A310-200	0.00	0.00	3.69	
3	A330-200 WV020	0.23	0.23	1.98	
4	A330-300 std	0.23	0.23	1.88	
5	B727-200 Advanced Option	0.00	0.00	2.97	
6	B747-200/300	0.03	0.03	3.46	
7	B747-200/300 Belly	0.00	0.03	3.47	
8	B747-400	0.03	0.03	3.47	
9	B747-400 Belly	0.00	0.03	3.47	
10	B757-200	0.00	0.00	3.92	
11	B757-300	0.00	0.00	3.93	
12	B767-200	0.00	0.00	3.73	
13	B767-300	0.00	0.00	3.86	
14	B777-200 ER	0.22	0.22	4.05	
15	B787-8	0.18	0.18	3.77	
16	C-130	0.00	0.00	4.67	
17	C-5	0.00	0.00	1.41	
18	DC/MD-10-10/10F	0.01	0.01	3.8	
19	MD-11	0.07	0.07	3.67	
20	MD-11 Belly	0.00	0.00	3.01	
21	S-15	0.00	0.00	3.6	
22	S-25	0.00	0.00	3.94	
23	S-50	0.00	0.00	2.73	
24	D-15	0.00	0.00	5.48	
25	D-25	0.00	0.00	5.03	
26	D-50	0.00	0.00	3.73	
27	D-75	0.00	0.00	3.6	
28	D-100	0.00	0.00	3.55	
29	D-150	0.00	0.00	3.28	
30	D-200	0.00	0.00	3.29	

User Is responsible For checking frost protection requirements.

		(1 5 700 1
P-501 PCC Surface 	T=16.9 inches ✓	∠ <u>R=700 psi</u>
User Defined	T=6.0 inches	E=250000 psi
P-304 Cement Treated Base	T=16.0 inches	E=500000 psi
User Defined	T=12.0 inches	E=1500 psi
Subgrade	k=28.7 pci	E=1500 psi

Federal Aviation Administration FAARFIELD 2.0 Section Report

FAARFIELD 2.0.3 (Build 04/30/2021)

Job Name: EFD Taxiway L - Pavement Options_Updated

Section: Option 2 - CBR = 5

Analysis Type: New Rigid

Last Run: Thickness Design 2021-10-28 18:12:32

Design Life = 30 Years

Total thickness to the top of the subgrade = 46.3in.

Pavement Structure Information by Layer

No.	Туре	Thickness in.	Modulus psi	Poisson's Ratio	Strength R psi
1	P-501 PCC Surface	12.3	4000000	0.15	700.0
2	User Defined	6.0	250000	0.35	0
3	P-304 Cement Treated Base	16.0	500000	0.35	0
4	User Defined	12.0	7500	0.35	0
5	Subgrade	0	7500	0.4	0

Airplane Information

No.	Name	Gross Wt. lbs	Annual Departures	% Annual Growth
1	D-200	200000	5	0
2	A310-200	315041	10	0
3	A330-200 WV020	509050	50	0
4	A330-300 std	509050	50	0
5	B727-200 Advanced Option	210000	15	0
6	B747-200/300	836000	50	0
7	B747-200/300 Belly	836000	50	0
8	B747-400	877000	25	0
9	B747-400 Belly	877000	25	0
10	B757-200	256000	25	0
11	B757-300	271000	10	0
12	B767-200	368000	10	0
13	B767-300	352000	20	0
14	B777-200 ER	658000	25	0
15	B787-8	503500	25	0
16	C-130	155000	200	0
17	C-5	769000	75	0
18	DC/MD-10-10/10F	458000	10	0
19	MD-11	633000	10	0
20	MD-11 Belly	633000	10	0
21	S-15	15000	1800	0
22	S-25	25000	35	0
23	S-50	50000	500	0
24	D-15	15000	350	0
25	D-25	25000	5	0
26	D-50	50000	530	0
27	D-75	75000	60	0
28	D-100	100000	115	0
29	D-150	150000	5	0
30	D-200	200000	75	0

Additional Airplane Information

No.	Name	CDF Contribution	CDF Max for Airplane	P/C Ratio	
1	D-200	0.00	0.00	3.29	
2	A310-200	0.00	0.00	3.69	
3	A330-200 WV020	0.21	0.21	1.98	
4	A330-300 std	0.15	0.15	1.88	
5	B727-200 Advanced Option	0.00	0.00	2.97	
6	B747-200/300	0.03	0.03	3.46	
7	B747-200/300 Belly	0.00	0.03	3.47	
8	B747-400	0.04	0.04	3.47	
9	B747-400 Belly	0.00	0.04	3.47	
10	B757-200	0.00	0.00	3.92	
11	B757-300	0.00	0.00	3.93	
12	B767-200	0.00	0.00	3.73	
13	B767-300	0.00	0.00	3.86	
14	B777-200 ER	0.20	0.20	4.05	
15	B787-8	0.29	0.30	3.77	
16	C-130	0.00	0.00	4.67	
17	C-5	0.00	0.00	1.41	
18	DC/MD-10-10/10F	0.01	0.01	3.8	
19	MD-11	0.07	0.07	3.67	
20	MD-11 Belly	0.00	0.00	3.01	
21	S-15	0.00	0.00	3.6	
22	S-25	0.00	0.00	3.94	
23	S-50	0.00	0.00	2.73	
24	D-15	0.00	0.00	5.48	
25	D-25	0.00	0.00	5.03	
26	D-50	0.00	0.00	3.73	
27	D-75	0.00	0.00	3.6	
28	D-100	0.00	0.00	3.55	
29	D-150	0.00	0.00	3.28	
30	D-200	0.00	0.01	3.29	

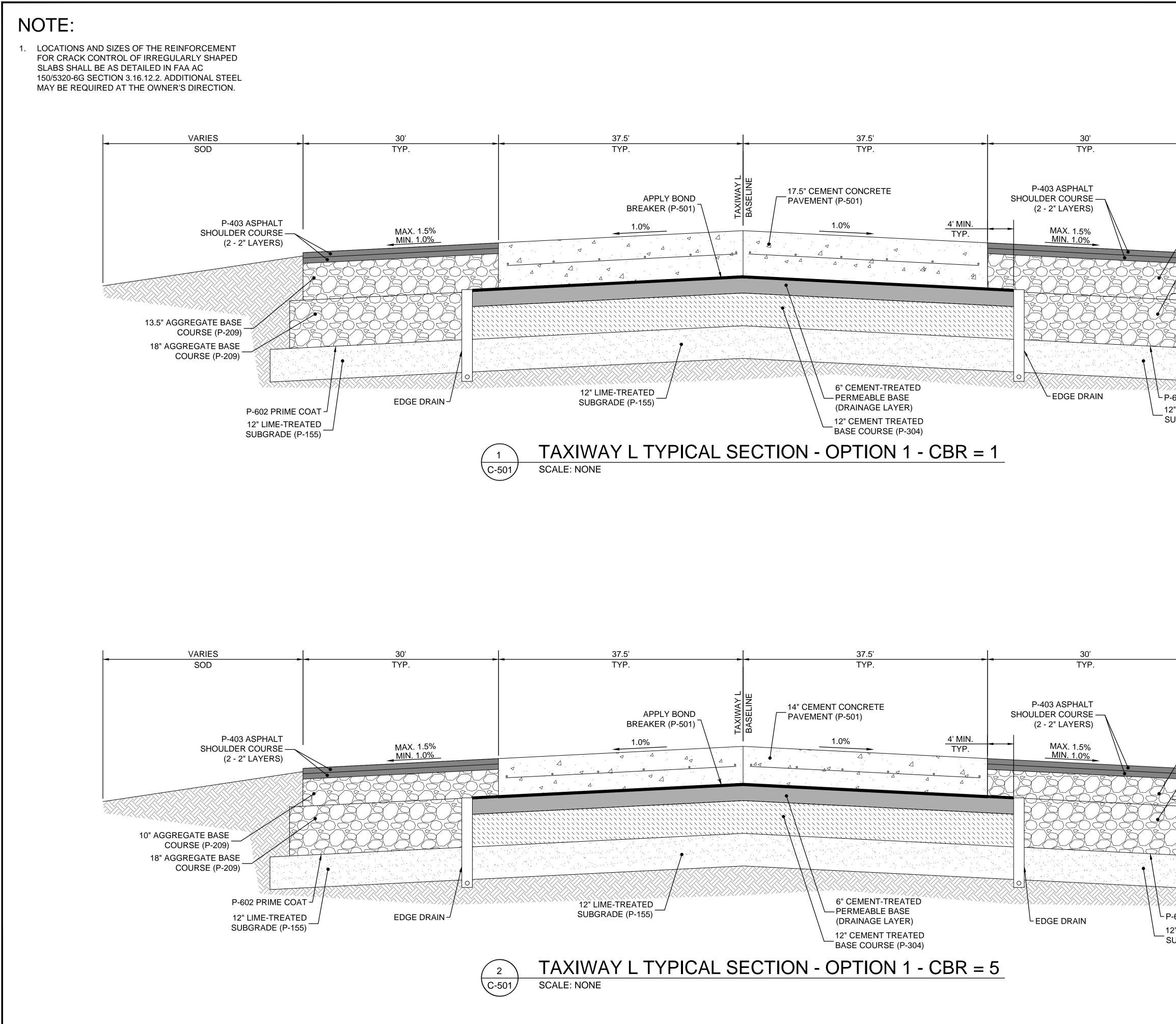
User Is responsible For checking frost protection requirements.

P-501 PCC Surface		T=12.3 inches		R=700 ps	i
7	•			* .	
Z, Z		. 4	- 		
User Defined		T=6.0 inches		E=25000	0 psi
P-304 Cement Treated Base	////	T=16.0 inches		E=50000	0 psi
User Defined		T=12.0 inches		E=7500 p	si
Subgrade		k=100.5 pci		E=7500 p	si



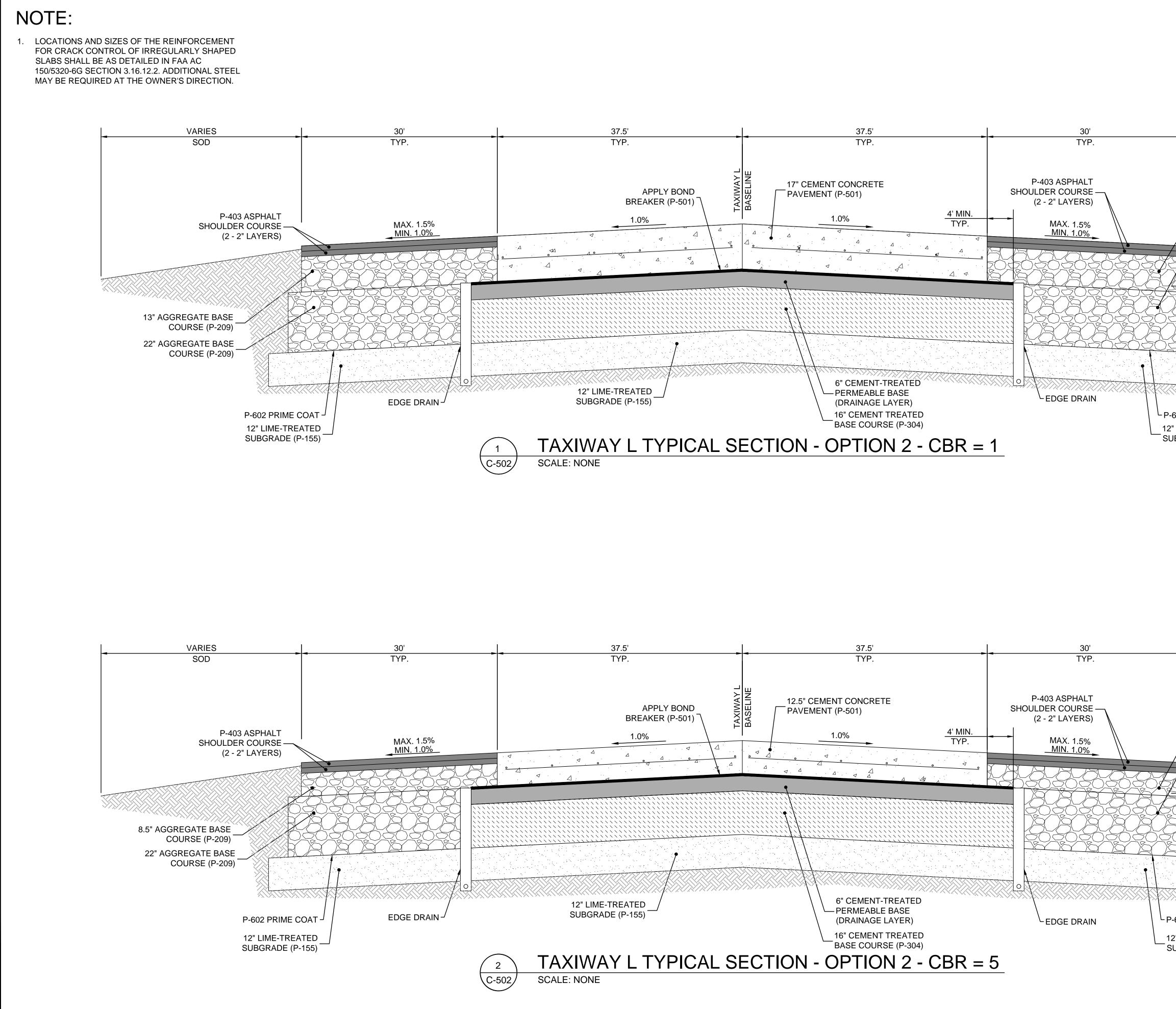


Appendix D – Preliminary Typical Pavement Sections



HAS FILE: C: \PW_WOR PLOT DATE: 2021-10-

	HOUSTON AIRPORT SYSTEM GEORGE BUSH INTERCONTINENTAL AIRPORT / HOUSTON, TX
VARIES SOD 13.5" AGGREGATE BASE	LOCAL OFFICE: 200 WESTLAKE PARK BLVD., STE. 1100 HOUSTON, TX 77079 TEL: (713) 576-8500 ATKINS NORTH AMERICA PE FIRM REG. #F-000474 WWW.ATKINSGLOBALCOM REVISIONS NO. DESCRIPTION DATE BY
COURSE (P-209) 18" AGGREGATE BASE COURSE (P-209) 2' MIN. TYP.	
-602 PRIME COAT 2' LIME-TREATED 3'BGRADE (P-155)	EFD TAXIWAY L TYPICAL SECTIONS
VARIES SOD 10" AGGREGATE BASE COURSE (P-209) 18" AGGREGATE BASE COURSE (P-209) 2' MIN. TYP.	PROJECT MGR: JLV DESIGNER: EW DRAWN BY: KJV CHECK BY: JLV SCALE: DATE: 10/28/2021
P-602 PRIME COAT 2" LIME-TREATED SUBGRADE (P-155)	APPROVED BY: DIRECTOR HOUSTON AIRPORT SYSTEM PROJECT NO. 100073798 A.I.P. NO. C.I.P. NO. H.A.S. NO. SHEET NO. C-501



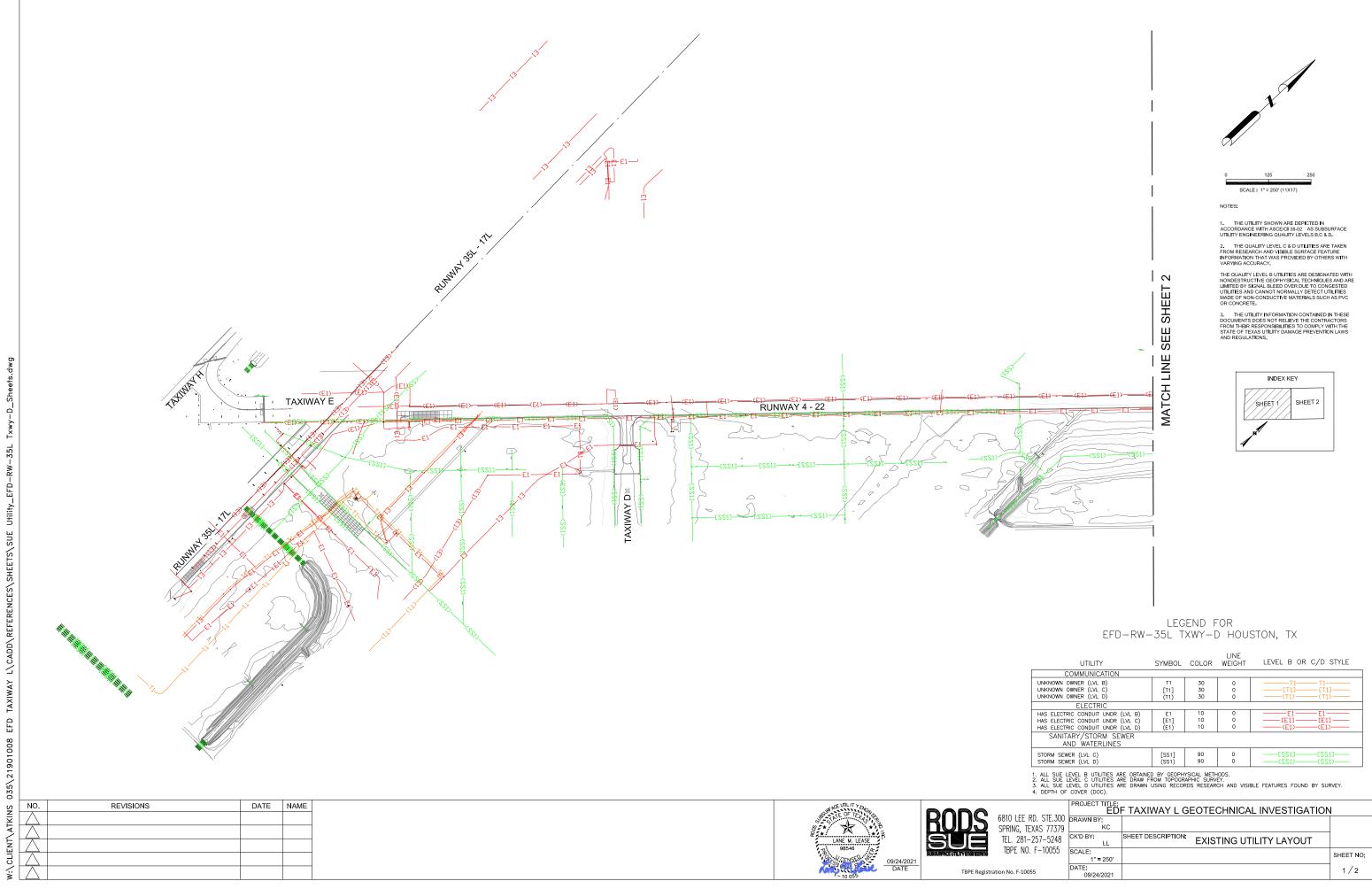
	HOUSTON AIRPORT SYSTEM GEORGE BUSH INTERCONTINENTAL AIRPORT / MOUSTON, TX CAL OFFICE: 200 WESTLAKE PARK BLVD., STE. 1100
VARIES SOD	 HOUSTON, TX 77079 TEL: (713) 576-8500 ATKINS NORTH AMERICA PE FIRM REG.
300	#F-000474 www.atkinsglobal.com
	REVISIONS NO. DESCRIPTION DATE BY
13" AGGREGATE BASE COURSE (P-209)	
22" AGGREGATE BASE COURSE (P-209)	
<u>2' MIN.</u> TYP.	
5' MIN. TYP.	0
-602 PRIME COAT 2" LIME-TREATED	NA) VA) CTI
JBGRADE (P-155)	EFD TAXIWAY I FPICAL SECTIO
	D T, CAL
	EFD TAXIWAY L TYPICAL SECTIONS
VARIES	
SOD	 PROJECT MGR: JLV DESIGNER: EW
	DRAWN BY: KJV CHECK BY: JLV SCALE:
8.5" AGGREGATE BASE	DATE: 10/28/2021
COURSE (P-209) 22" AGGREGATE BASE COURSE (P-209)	
2' MIN. TYP.	
	APPROVED BY:
5' MIN. TYP.	DIRECTOR HOUSTON AIRPORT SYSTEM
	PROJECT NO.
P-602 PRIME COAT	100073798 A.I.P. NO.
2" LIME-TREATED SUBGRADE (P-155)	C.I.P. NO.
	H.A.S. NO.
	SHEET NO.
	C-502

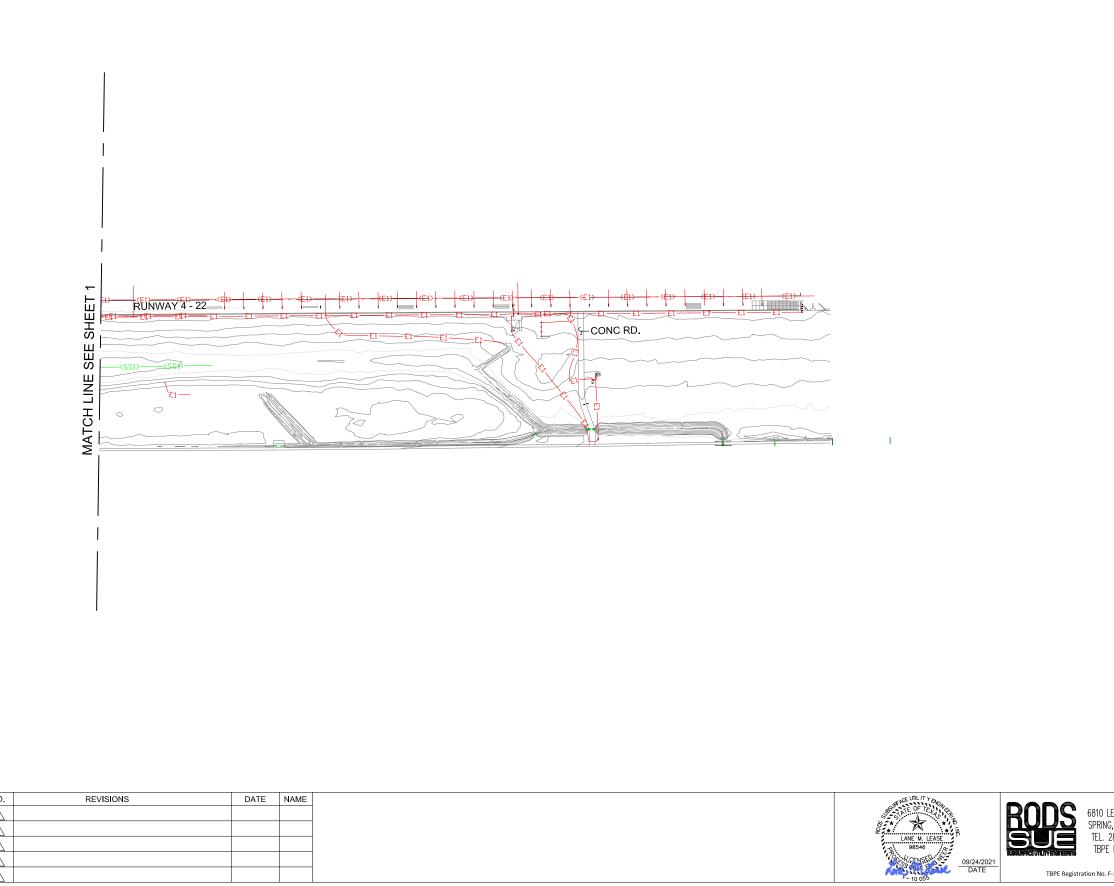




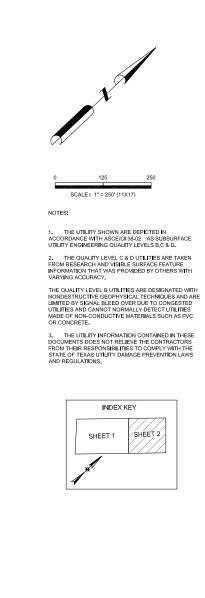
Appendix F – Existing Utilities Layout

EFD Taxiway L - Preliminary Pavement Design Memo





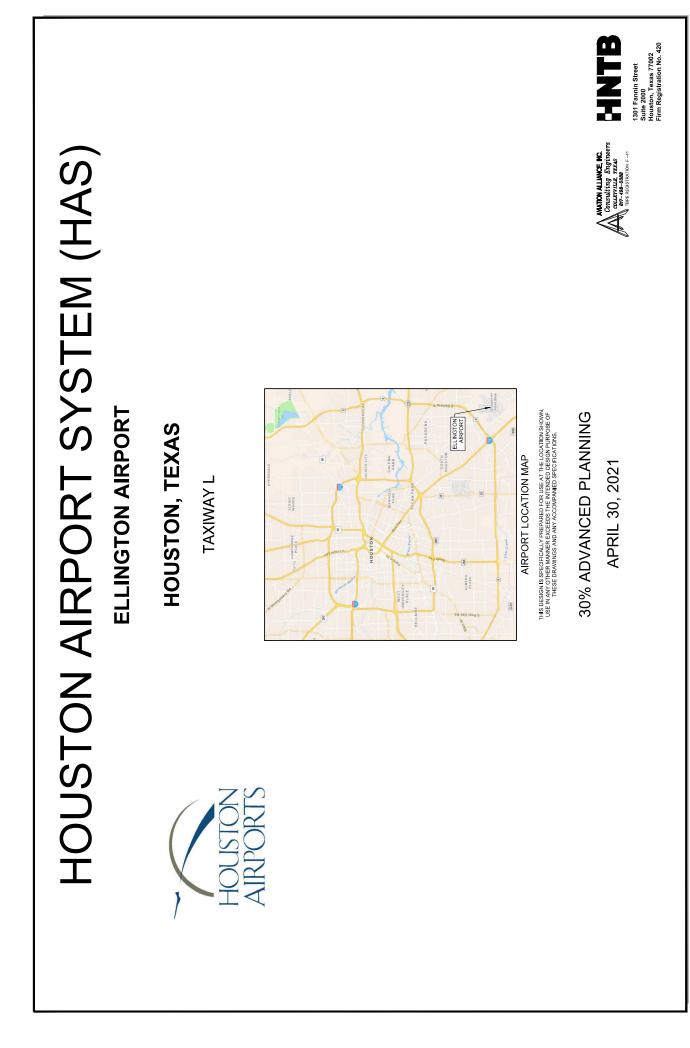
TBPE Registration No. F-



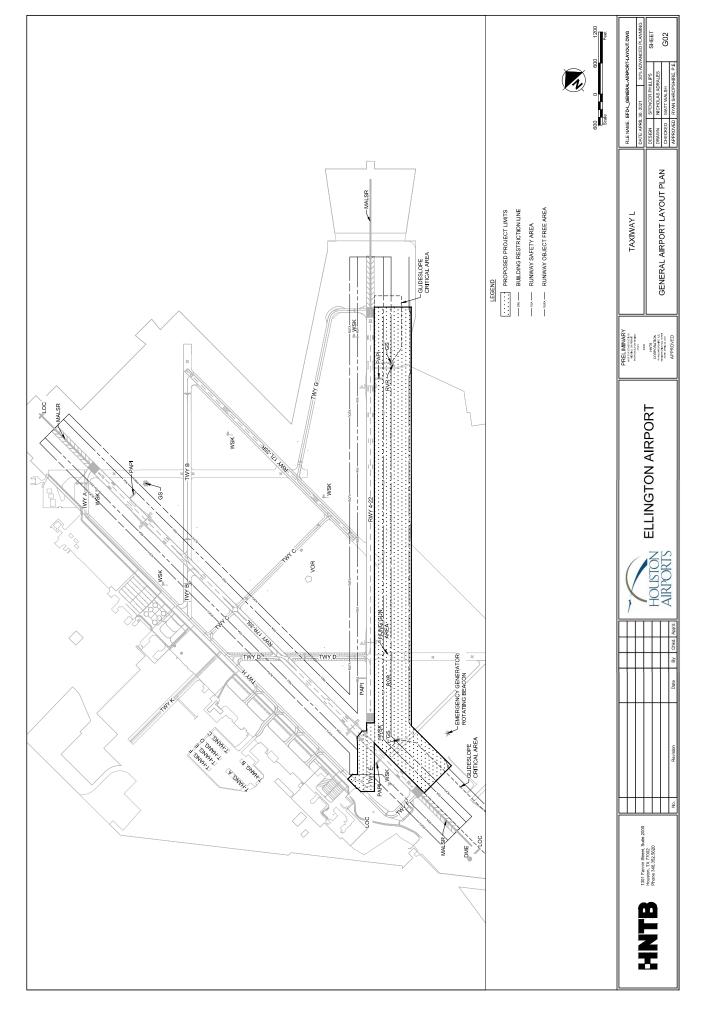
LEGEND FOR EFD-RW-35L TXWY-D HOUSTON, TX

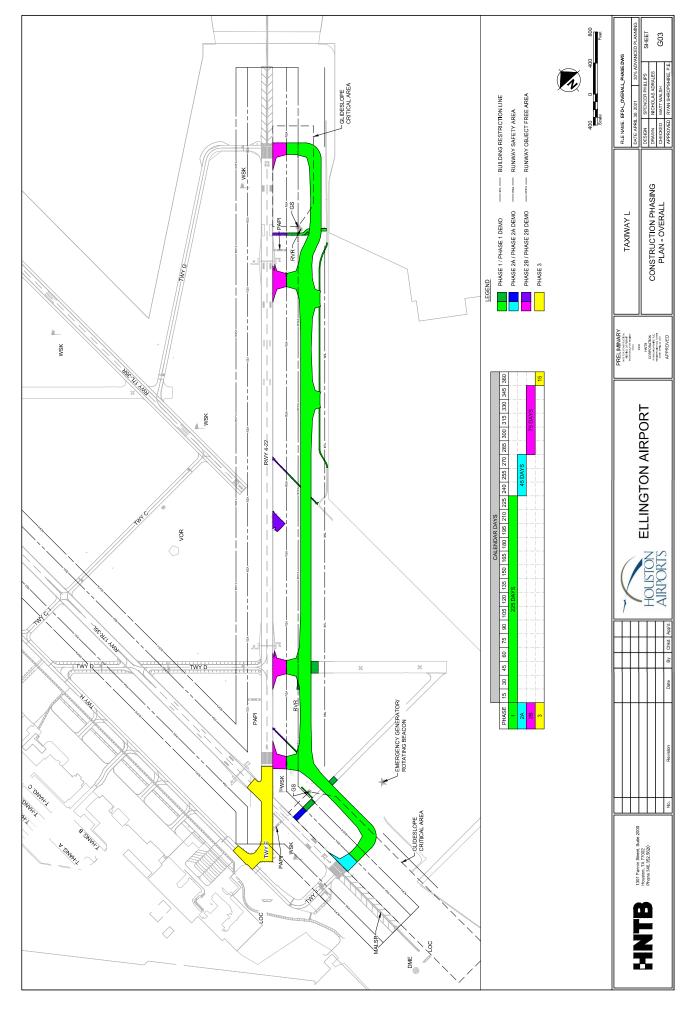
			0.4.001	001.00	LINE	LEVEL B OR C/D	STVI E
	UTILITY		SYMBOL	COLOR	WEIGHT	LEVEL B OK C/D	STILE
C	OMMUNICATION						
	WNER (LVL B)		T1	30	0	T1T1	
	WNER (LVL C)		[T1]	30	0	[1][1]	
UNKNOWN	WNER (LVL D)		(T1)	30	0	(T1)(T1)
	ELECTRIC				-		
	IC CONDUIT UNDR		E1	10 10	0	E1-E1-E1-	
	CONDUIT UNDR		[E1] (E1)	10	0	(E1)-(E1)	
	ARY/STORM SE		(E1)	10	v		·
	ND WATERLINES						
STORM SEW	FR (IVI C)		[SS1]	90	0		11
STORM SEW			(SS1)	90	0	22)(122)	D—
3. ALL SUE L	EVEL C UTILITIES AF EVEL D UTILITIES AF COVER (DOC).					BLE FEATURES FOUND BY SU	RVEY.
	PROJECT TITLE: EDI	F TAXI	WAY L (GEOTE	CHNICA	L INVESTIGATION	1
_EE RD. STE.300	DRAWN BY:						
G. TEXAS 77379	KC						
281-257-5248	CK'D BY:	SHEET DE	SCRIPTION			ILITY LAYOUT	
	LL			EVIS	TING UT	ILITY LAYOUT	
NO. F-10055	SCALE:						SHEET NO:
	1" = 250'						
F-10055	DATE:]					2/2
1 10035	09/24/2021						-, -

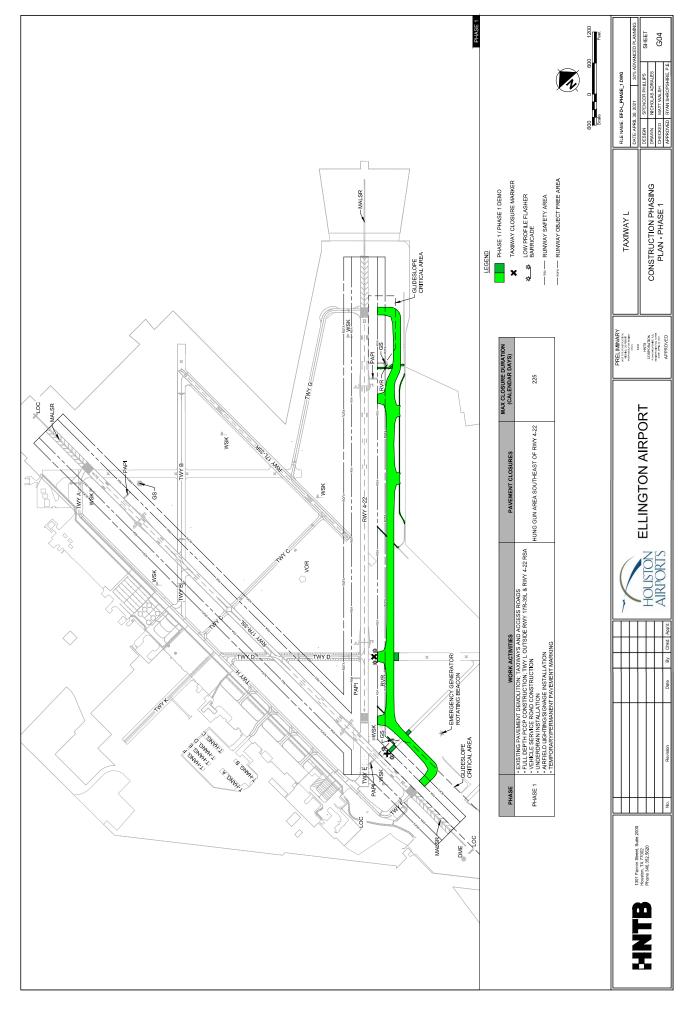
IV. 30% Advanced Planning Drawings (prepared by HNTB)

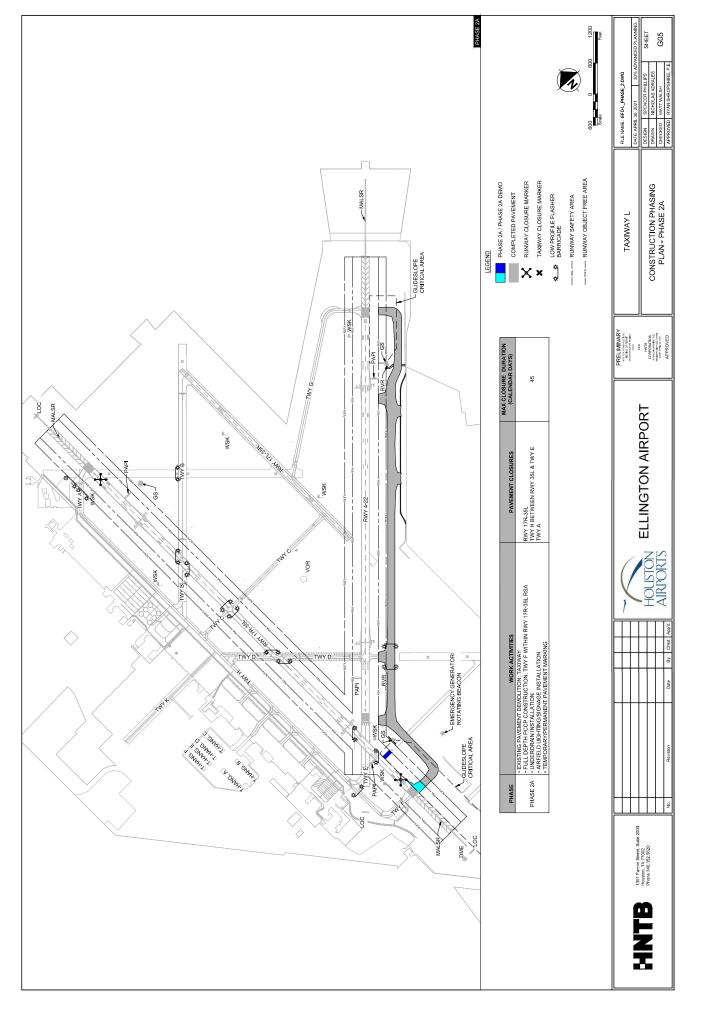


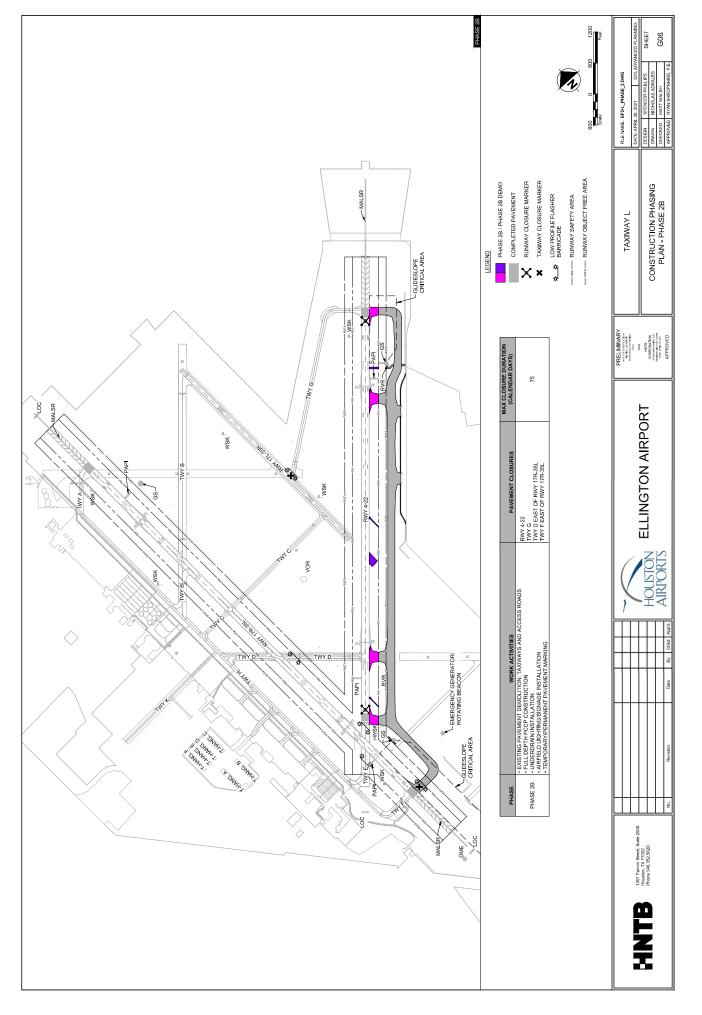
GENERAL AI	GENERAL ABBREVIATIONS	S				
	0	DIGHT	SHEET #	SHEET INDEX	SHEET #	SHEET INDEX
APP APPROVED ASPH ASPHALT ASPH ASPHALT	RCP ROFA	RUNDAR CONCRETE PIPE RUNWAY ON-JECT FREE PIPE		COVER SHEET	CM01	MARKING PLANS
	RSA		G01 GE	GENERAL ABBREVIATIONS AND SHEET INDEX	CM02	MARKING PLANS
BLL BUILDING RESTRICTION LINE	RW, RW?			GENERAL AIRPORT LAYOUT PLAN	CM03	
	s	SOUTH	_	CONSTRUCTION PHASING PLAN - OVERALL	CM04	_
CL CENTEKLINE CMP CORRUGATED METAL PIPE	SE STA	SOUTHEAST STATION	_	CONSTRUCTION PHASING PLAN - PHASE 1	CM05	
	STM SW	STORM SOUTHWEST	605 00	CONSTRUCTION PHASING PLAN - PHASE ZA CONSTRUCTION PHASING PLAN - PHASE 2P	CM06	
	F	TAXILANE	-	CONSTRUCTION PHASING PLAN - PHASE 25 CONSTRUCTION PHASING PLAN - PHASE 3		_
DIA DIAMETER DME DISTANCE MEASURING EQUIPMENT	TOFA TSA	TAXIWAY OBJECT FREE AREA TAXIWAY SAFETY AREA	-	TYPICAL SECTIONS	CM09	_
	λΥ	TAXIWAY TEXAS	-	GEOMETRIC LAYOUT & PLAN SHEET LAYOUT PLAN	ED01	-
EBOX ELECTRICAL BOX FED FILINGTON ARPORT	TYP T-HANG	TYPICAL T HANGAR	CD01 DE	DEMOLITION PLANS	ED02	AIRFIELD LIGHTING, SIGNAGE, AND NAVAID DEMOLITION PLANS
			CD02 DE	DEMOLITION PLANS	ED03	AIRFIELD LIGHTING, SIGNAGE, AND NAVAID DEMOLITION PLANS
	VOR	VERY FIGH-FREQUENCY OMNHURECTIONAL KANGE VEHICLE SERVICE ROAD	CD03 DE	DEMOLITION PLANS	ED04	AIRFIELD LIGHTING, SIGNAGE, AND NAVAID DEMOLITION PLANS
FL FLOWLINE	w	WIDTH, WEST	CD04 DE	DEMOLITION PLANS	ED05	AIRFIELD LIGHTING, SIGNAGE, AND NAVAID DEMOLITION PLANS
GS GLIDESLOPE	WSK W/	WINDSOCK		DEMOLITION PLANS	ED06	
			_	DEMOLITION PLANS	ED07	
HAS HOUSTON AIRPORT SYSTEM			_	DEMOLITION PLANS	ED08	-
ILS INSTRUMENT LANDING SYSTEM			_	DEMOLITION PLANS	ED09	_
			_	DEMOLITION PLANS	ED10	_
L LEFT LOC LOCALIZER			CG01 GR	GRADING AND DRAINAGE PLANS GPANING AND DRAINAGE PLANS	ED11	AIRFIELD LIGHTING, SIGNAGE, AND NAVAID DEMOLITION PLANS AIDELED LIGHTING, SIGNAGE, AND NAVAID LAVOLT DLANS
			-			_
MALSR MEDIUM-INTENSITY APPROACH LIGHTING SYSTEM WITH BUIMMAY ALICAMMENT INDICATOR LIGHTS	Н		_	GRADING AND DRAINAGE PLANS GPADING AND DDAINAGE DLANS	EUZ	_
			_	GRADING AND DRAINAGE PLANS		_
			_	GRADING AND DRAINAGE PLANS	EOS	_
N NORTH, NORTHING NE NORTHEAST			+	GRADING AND DRAINAGE PLANS	E00	-
			+	GRADING AND DRAINAGE PLANS	E07	-
			-	EROSION CONTROL PLANS	E08	-
			CG10 ER	EROSION CONTROL PLANS	E03	AIRFIELD LIGHTING, SIGNAGE, AND NAVAID LAYOUT PLANS
			CG11 ER	EROSION CONTROL PLANS	E10	AIRFIELD LIGHTING, SIGNAGE, AND NAVAID LAYOUT PLANS
			CG12 ER	EROSION CONTROL PLANS	E11	AIRFIELD LIGHTING, SIGNAGE, AND NAVAID LAYOUT PLANS
			CG13 ER	EROSION CONTROL PLANS		
PVIE POINT OF VERTICAL INTERSECTION ELEVATION PVIS POINT OF VERTICAL INTERSECTION STATION			-	EROSION CONTROL PLANS		
			-	EROSION CONTROL PLANS		
				EROSION CONTROL PLANS		
			_	TWY L PAVING PLAN AND PROFILE STA. 99+00.00 TO STA. 109+50.00	09+50.00	
			-	TWY L PAVING PLAN AND PROFILE STA. 109+50.00 TO STA. 118+50.00	118+50.00	
				TWY L PAVING PLAN AND PROFILE STA. 118+50.00 TO STA. 131+50.00	131+50.00	
			CP04 TM	TWY L PAVING PLAN AND PROFILE STA. 131+50.00 TO STA. 144+50.00	144+50.00	
				TWY L PAVING PLAN AND PROFILE STA. 144+50 TO STA. 157+50.00	*+50.00	
			CP06 TM	TWY L PAVING PLAN AND PROFILE STA. 157+50.00 TO 170+50.00	50.00	
				TWY L PAVING PLAN AND PROFILE STA. 170+50.00 TO STA 183+50.00	.83+50.00	
			-	TWY L PAVING PLAN AND PROFILE STA. 183+50.00 TO STA. 194+34.00	194+34.00	
				TWY F PAVING PLAN AND PROFILE		
			CP10 TV	TWY L5 AND TWY D PAVING PLAN AND PROFILE		
			CP11 TW	TWY L1 AND TWY L2 PAVING PLAN AND PROFILE		
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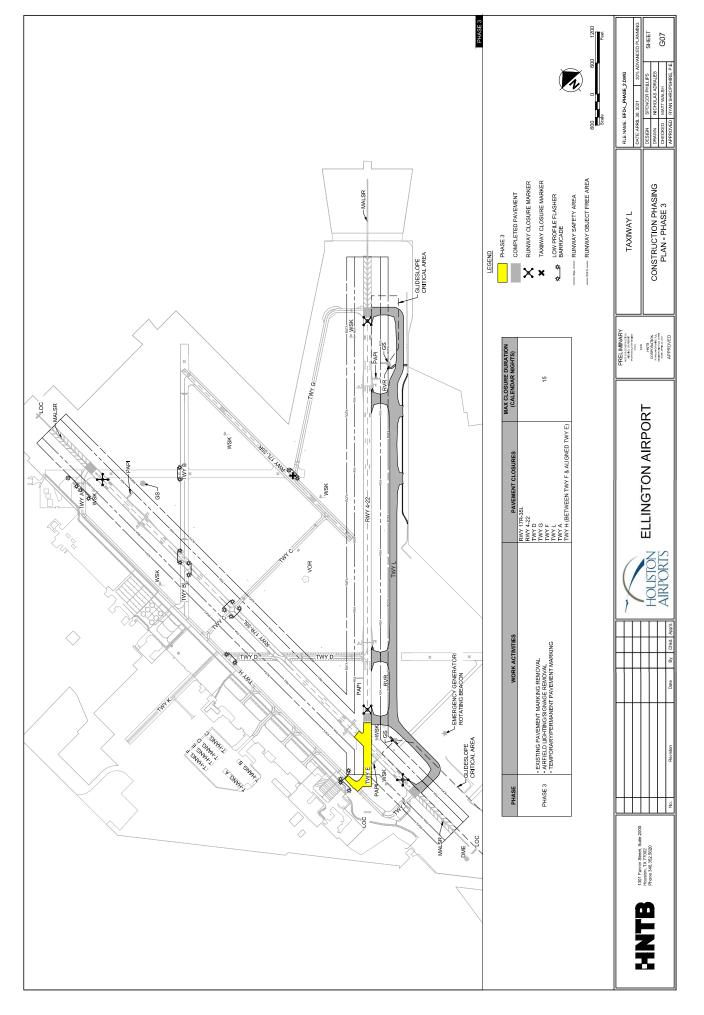


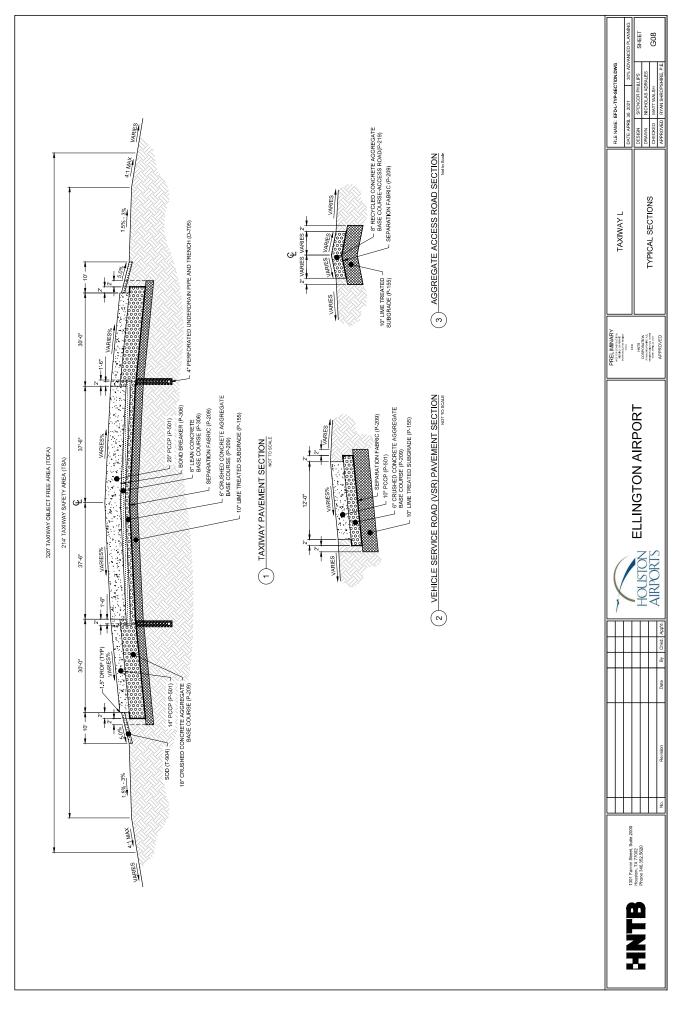


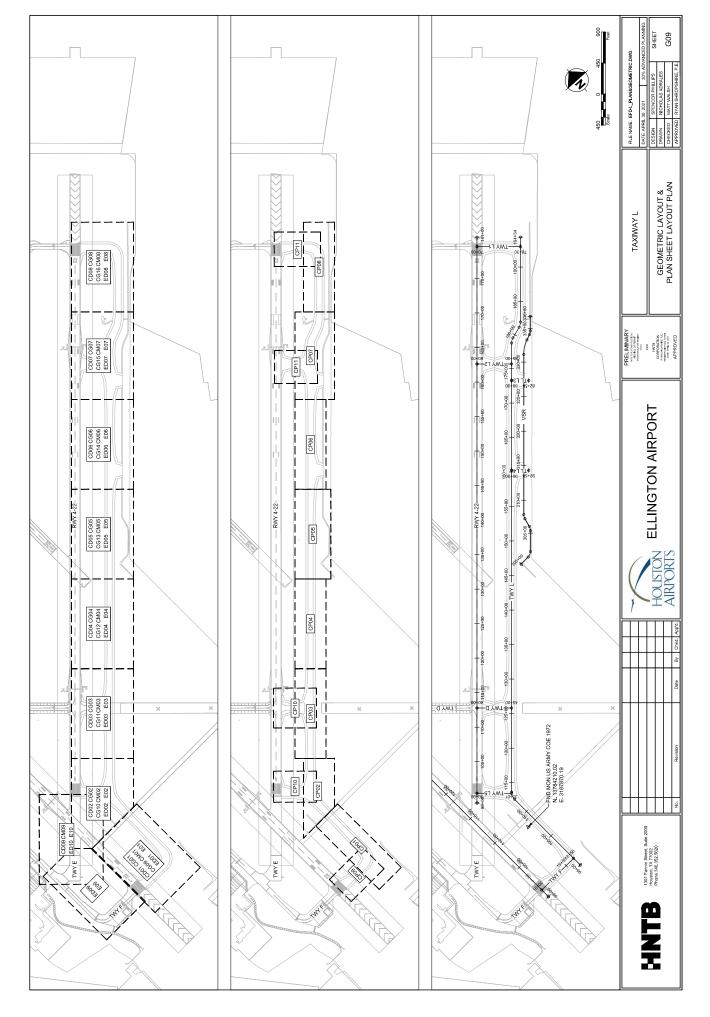


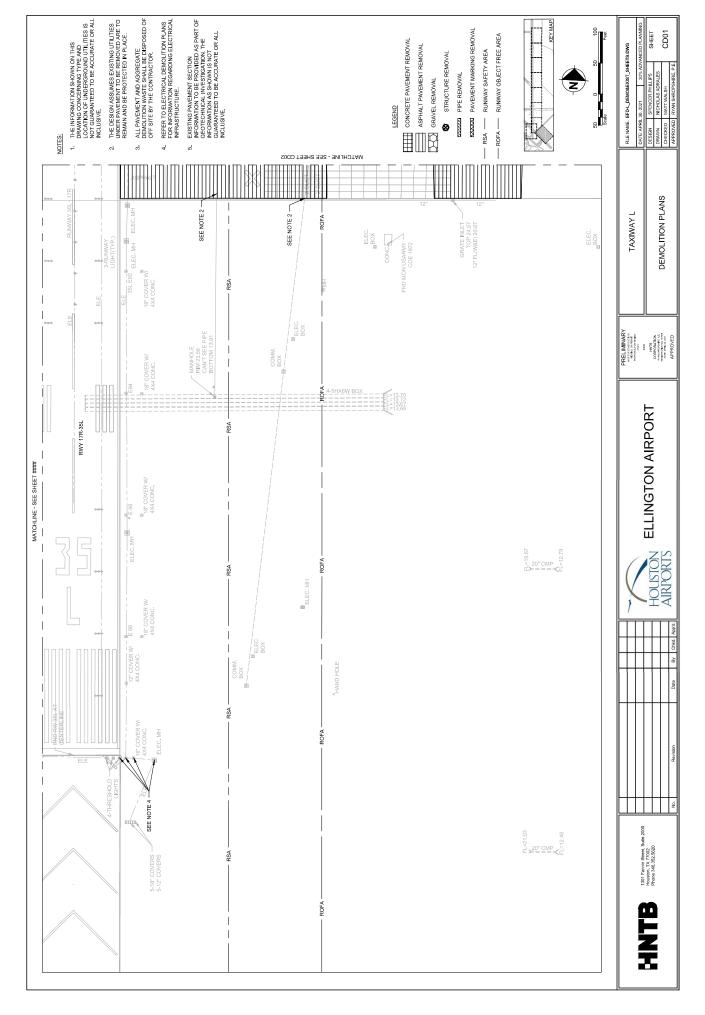


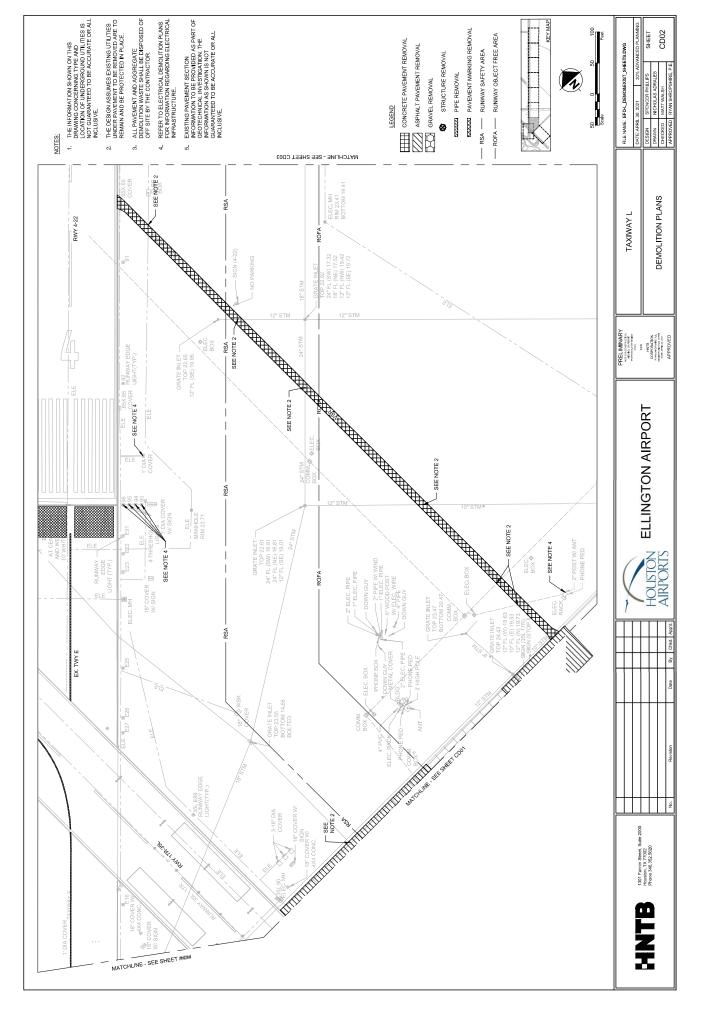


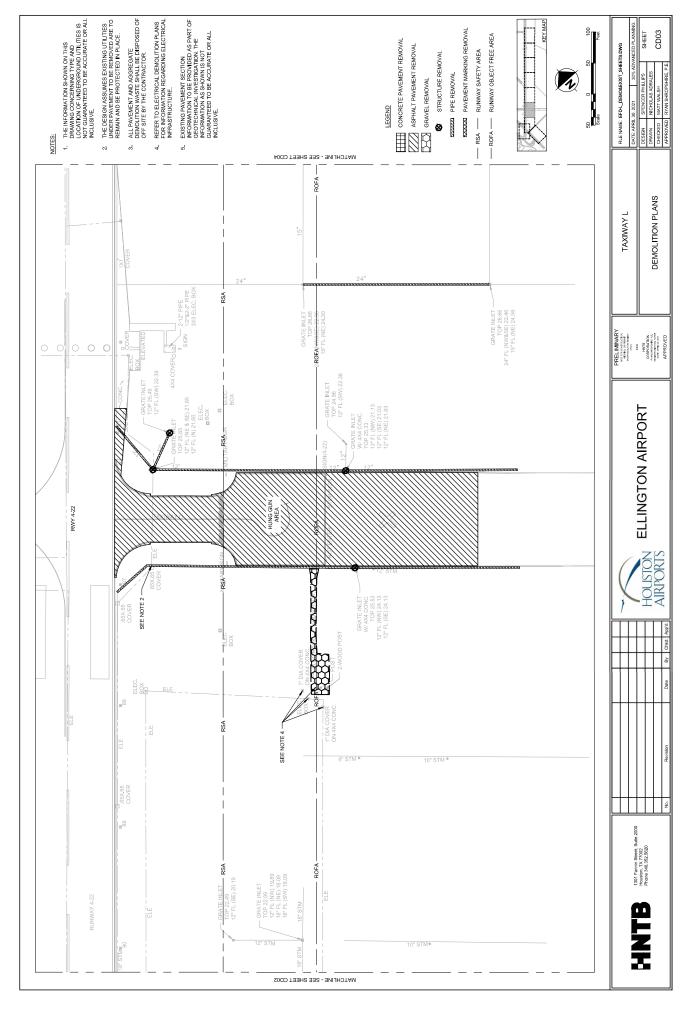


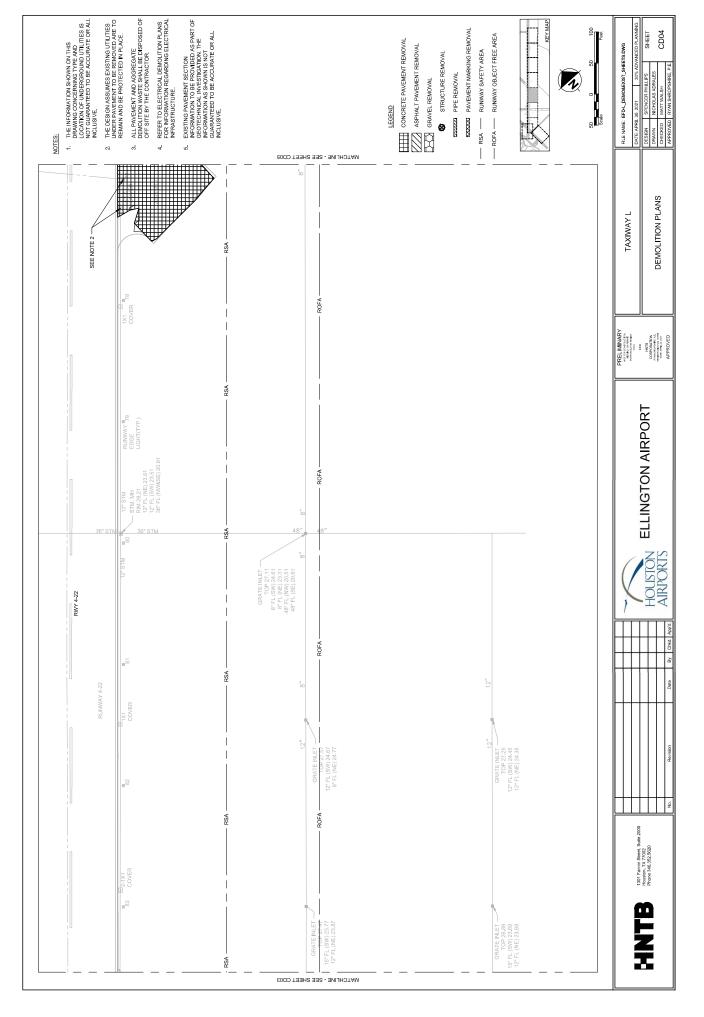


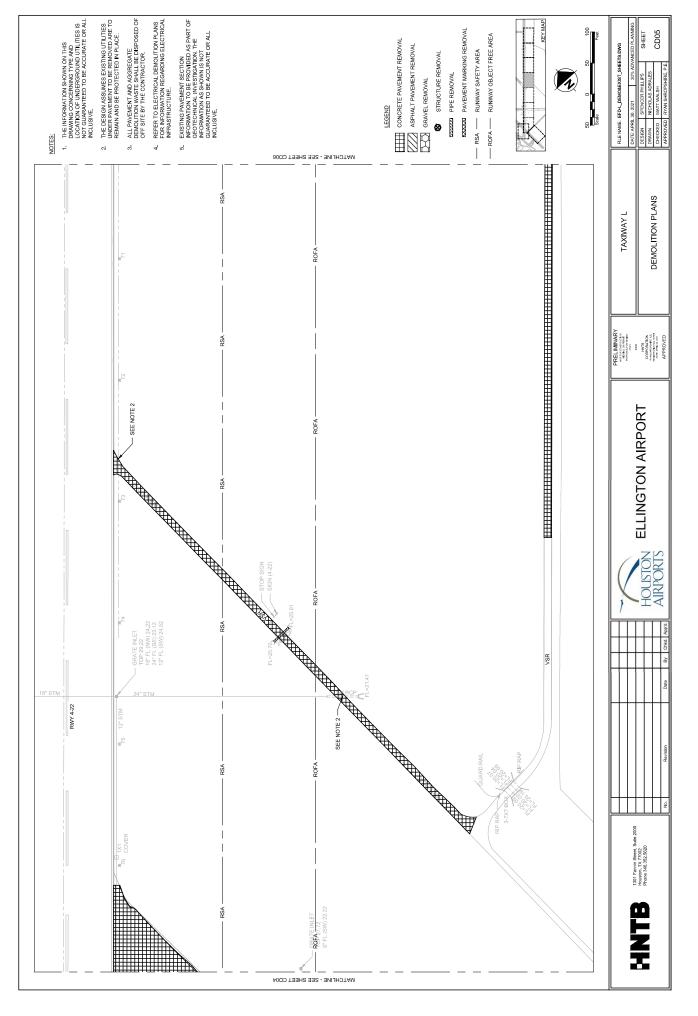


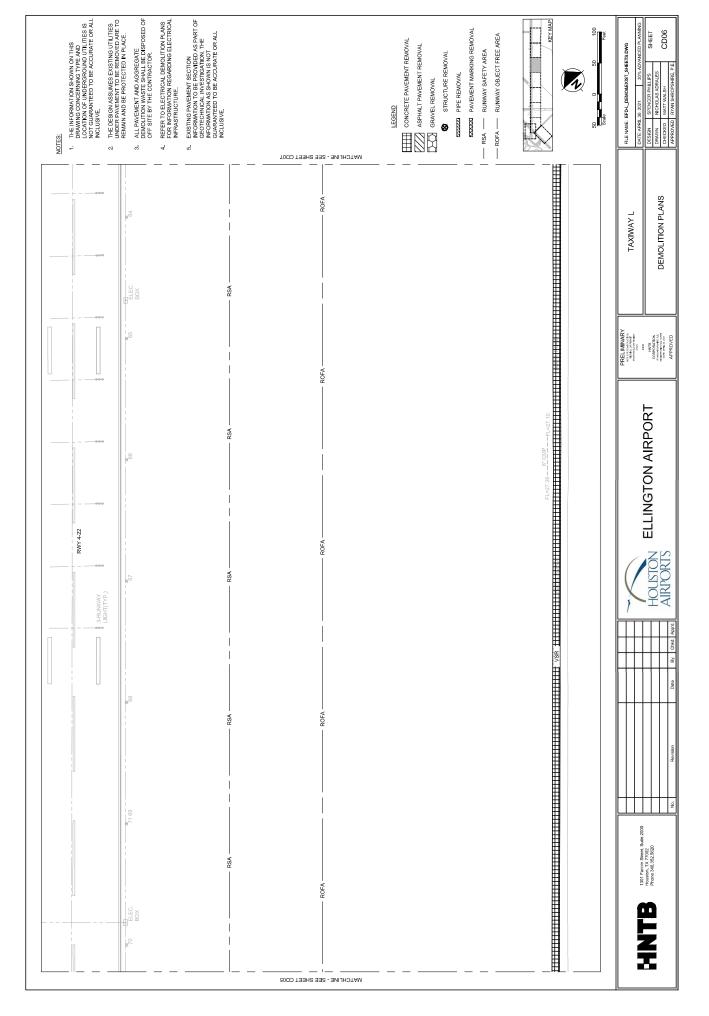


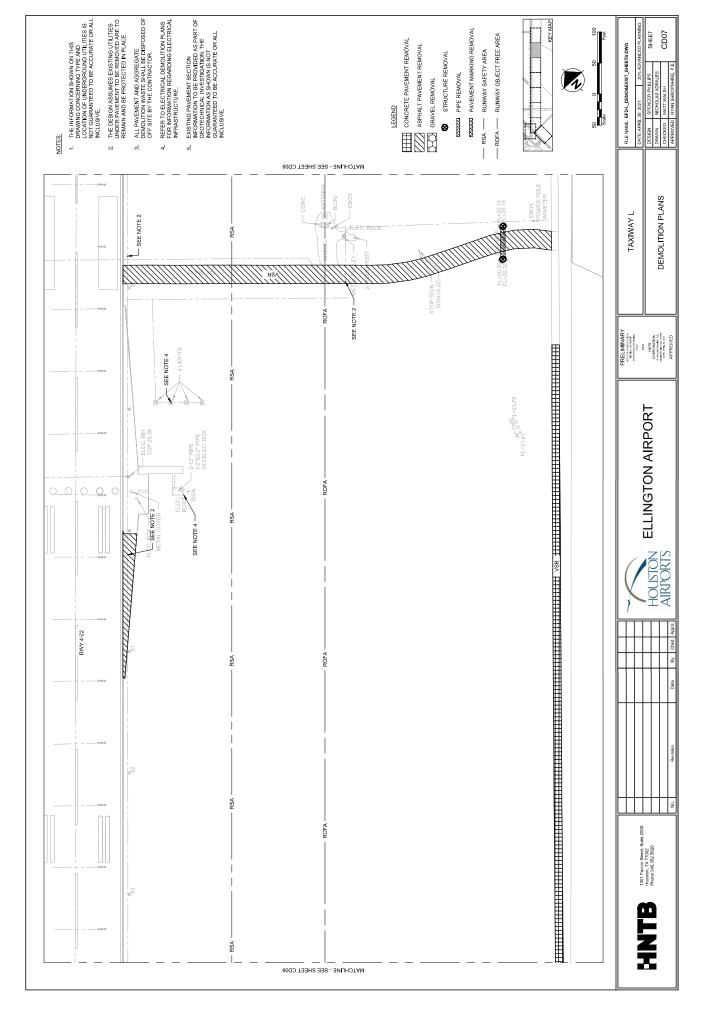


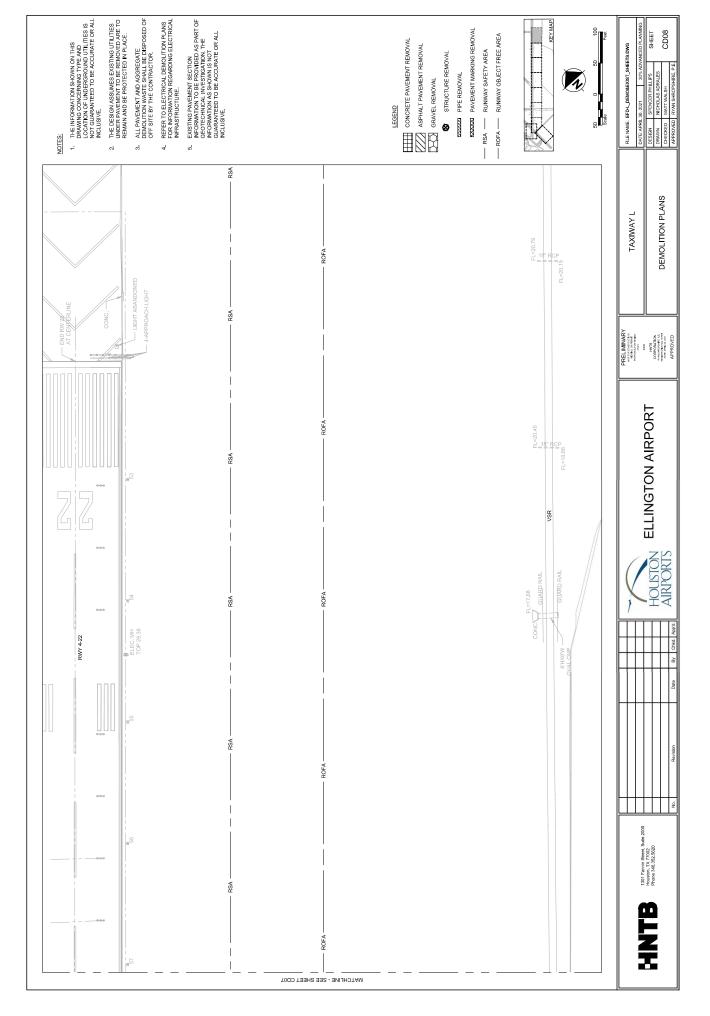


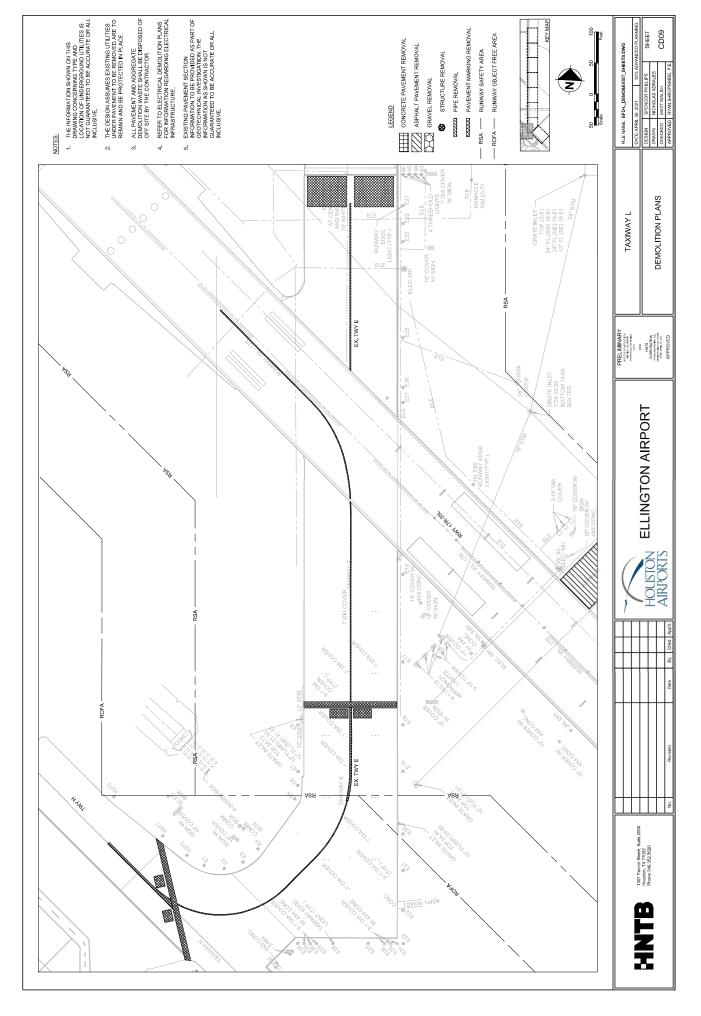


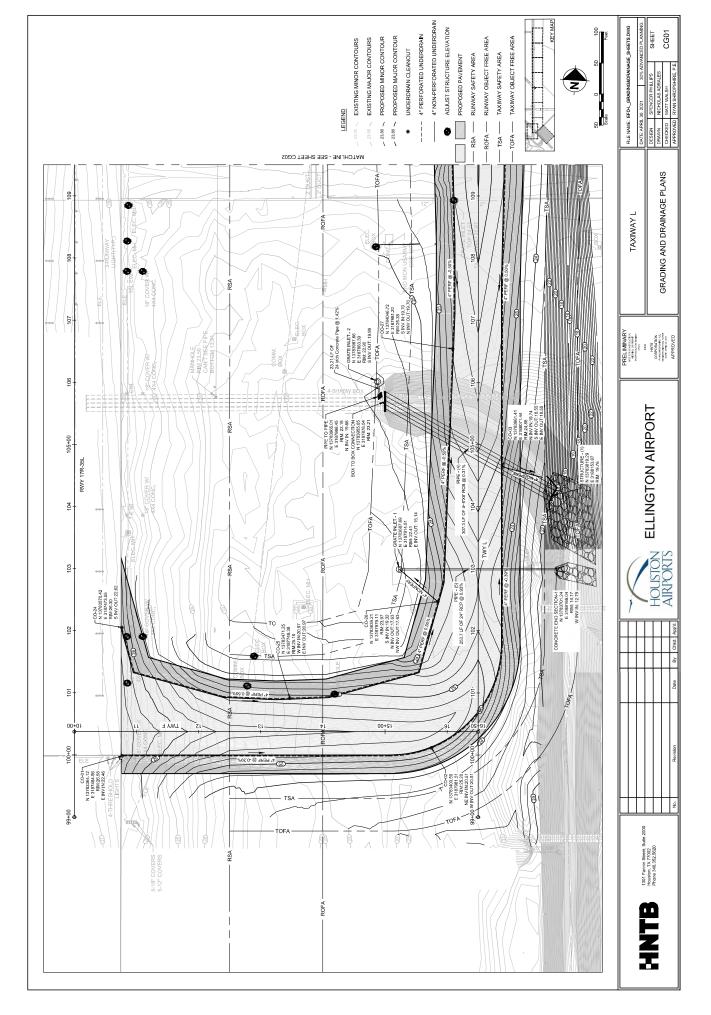


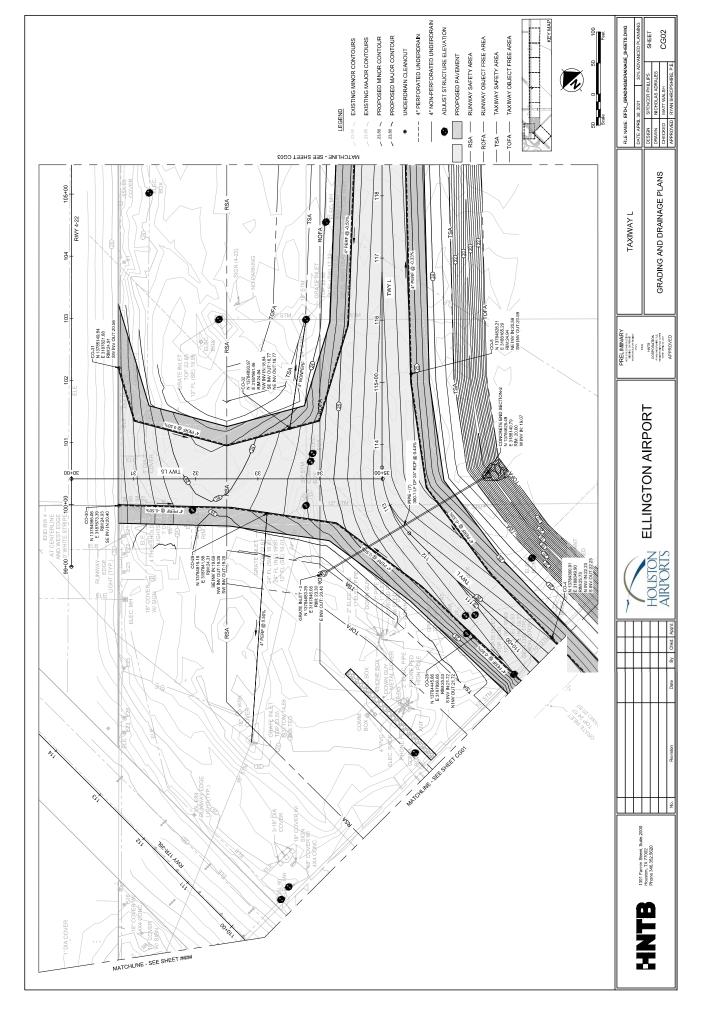


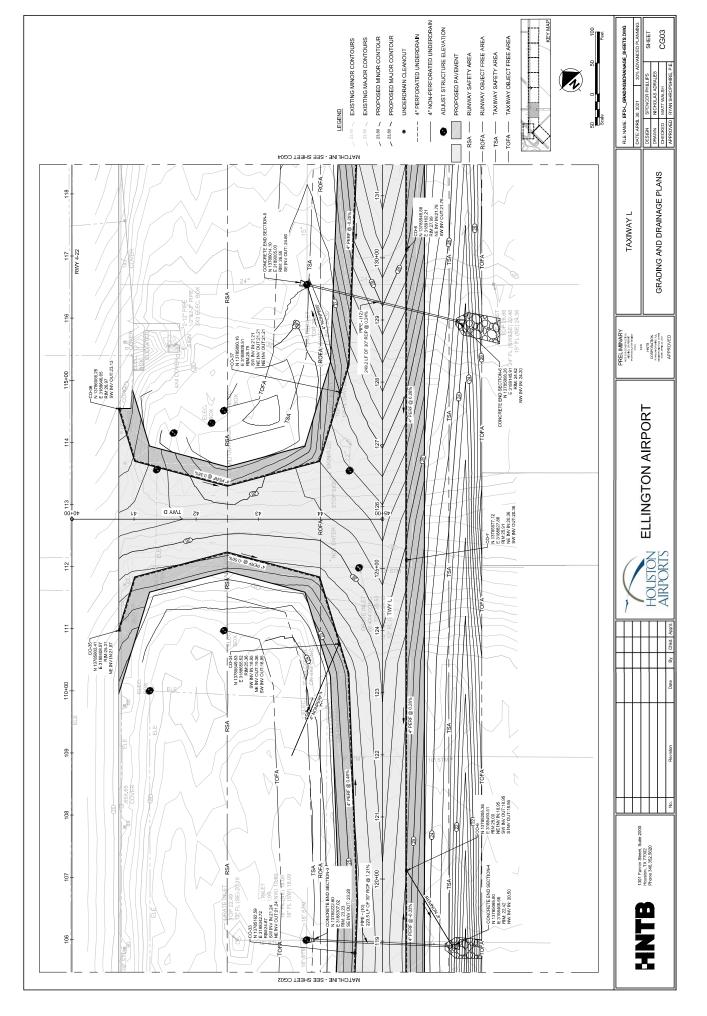


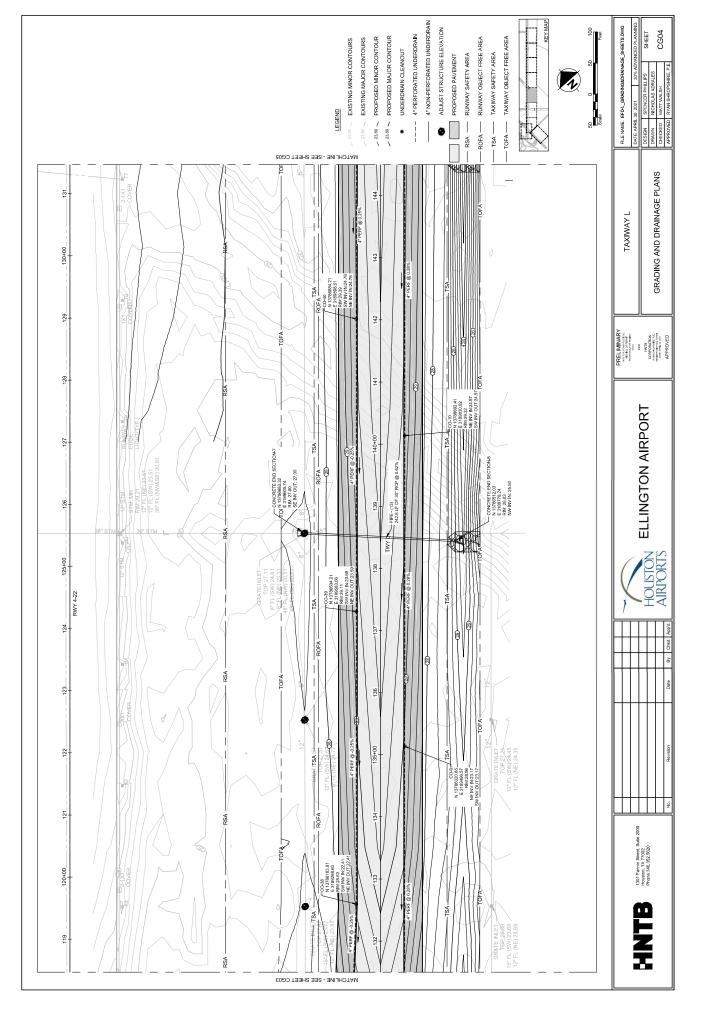




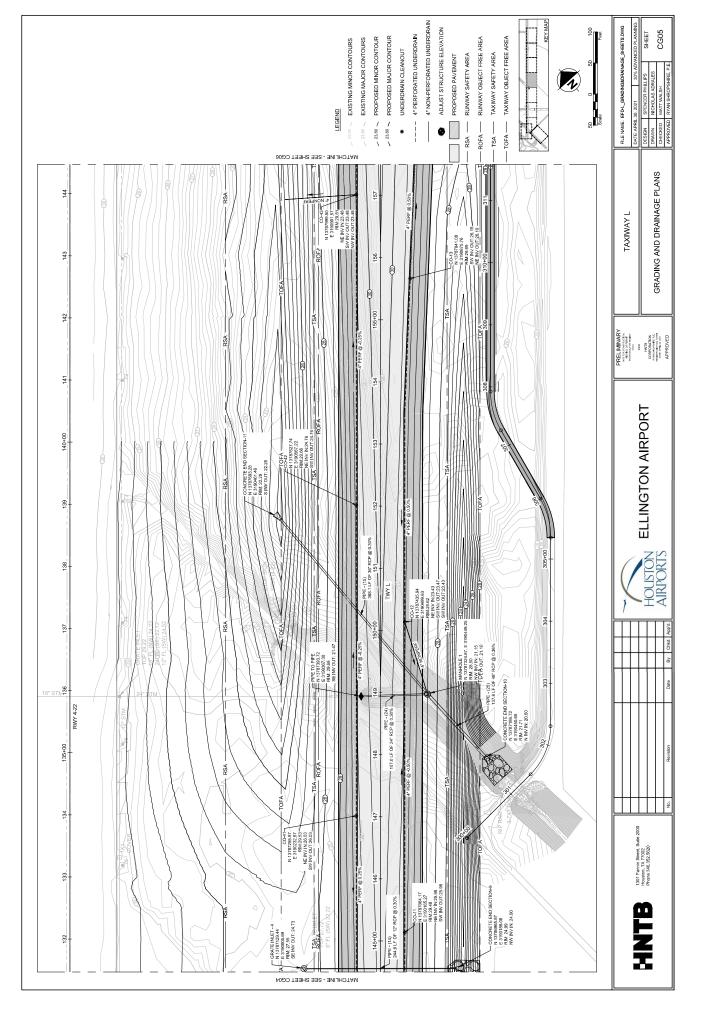


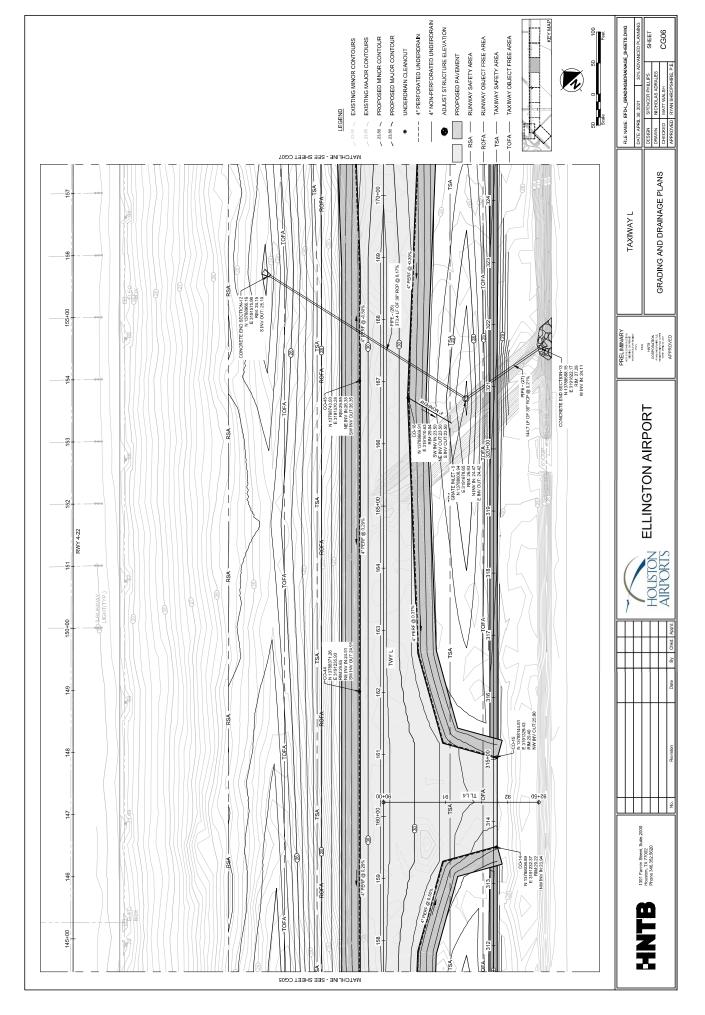


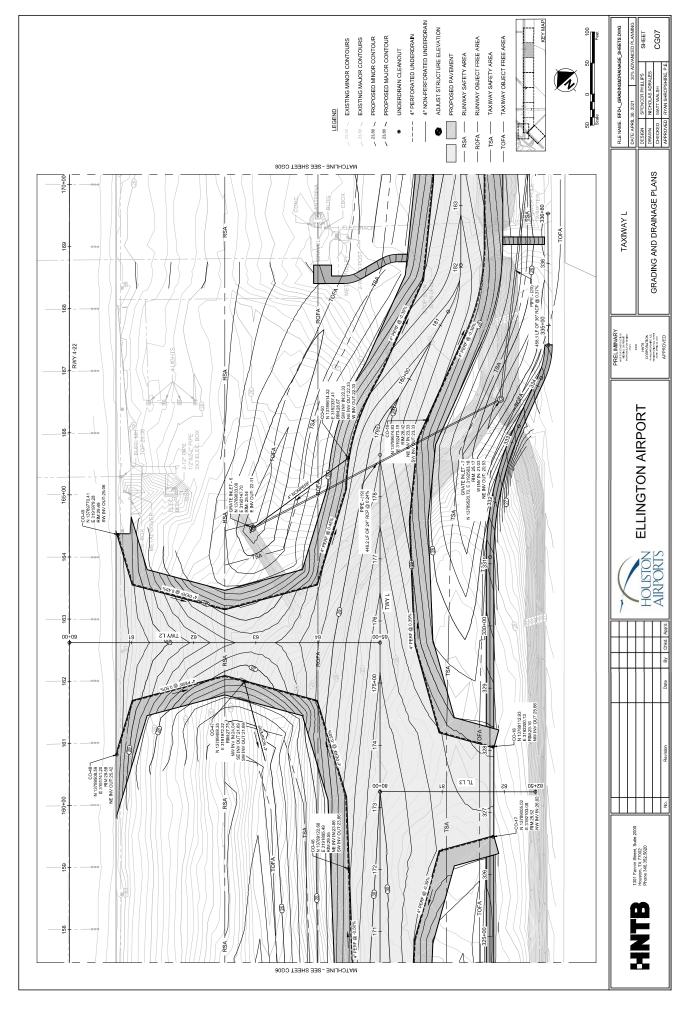


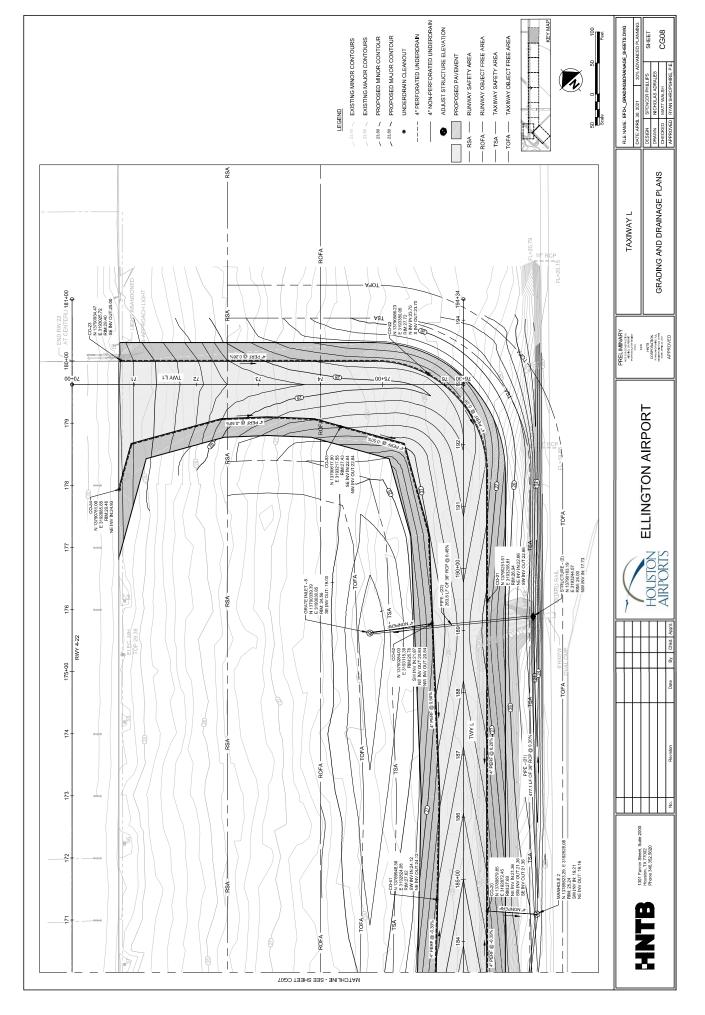


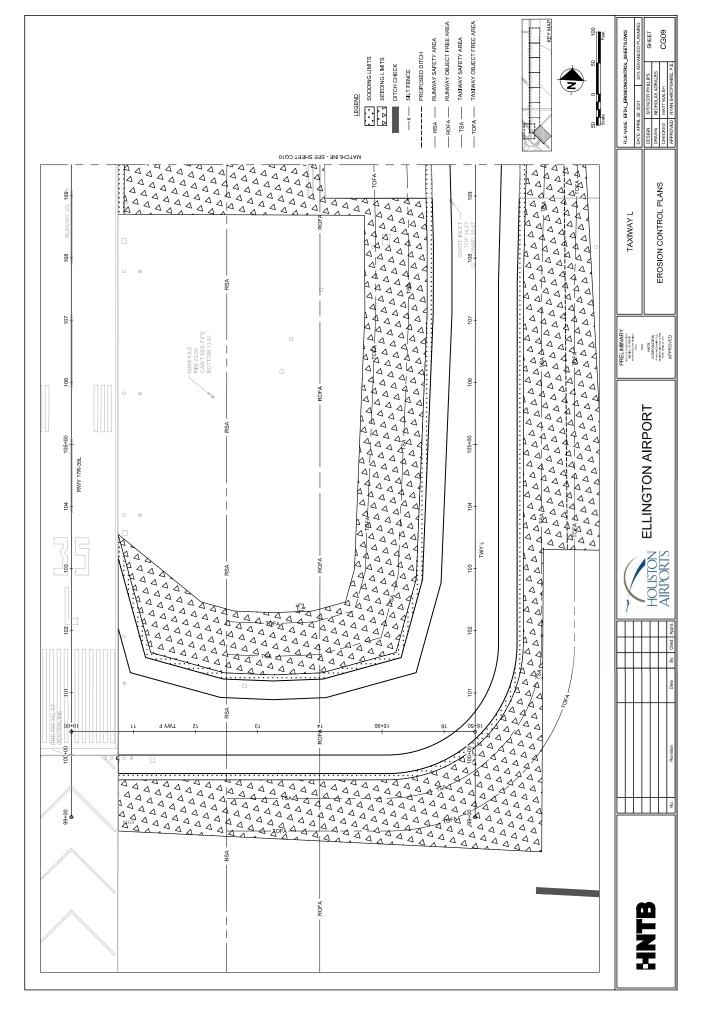
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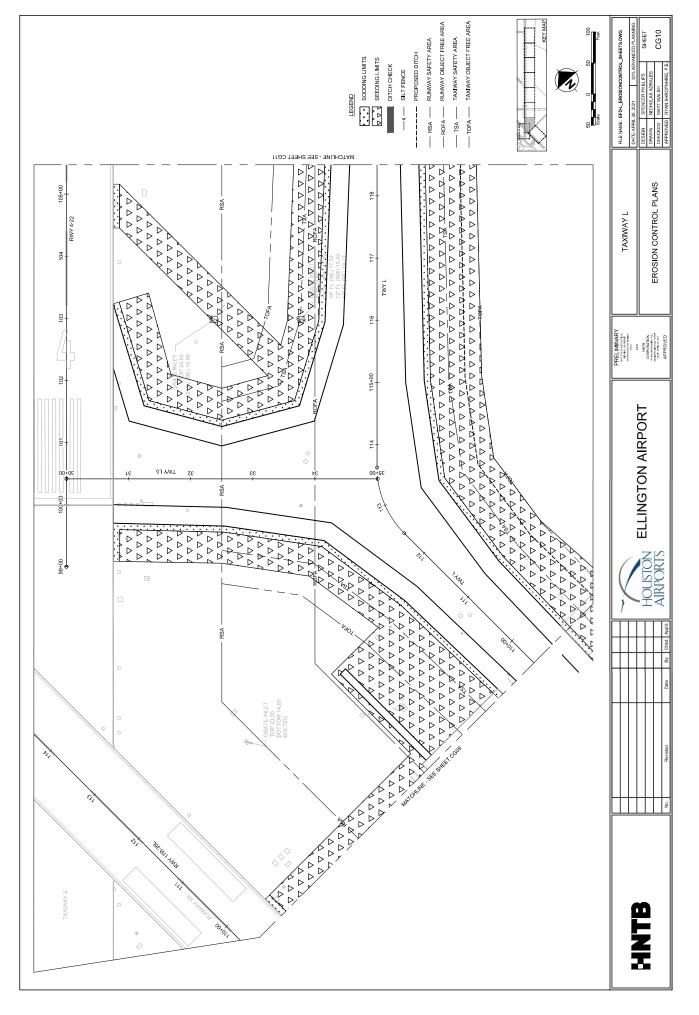


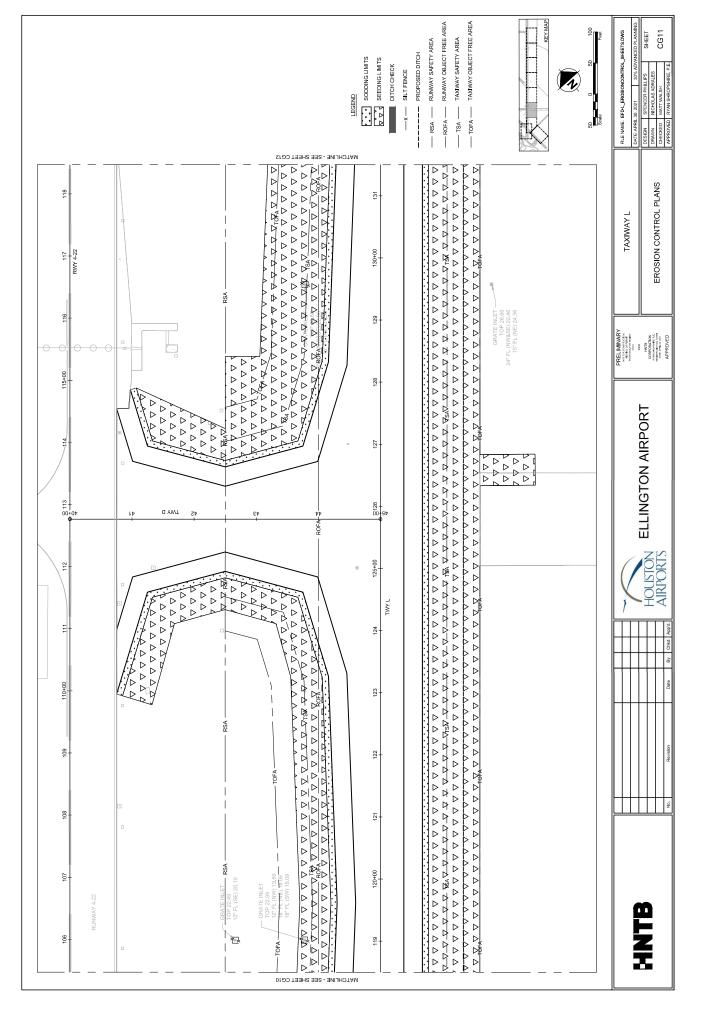






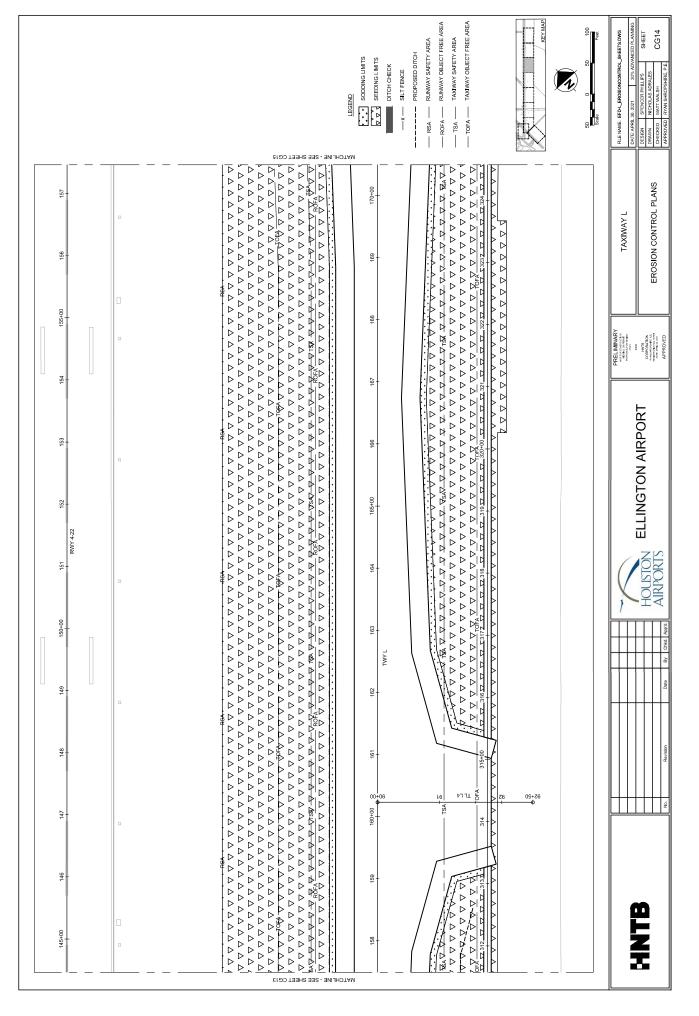


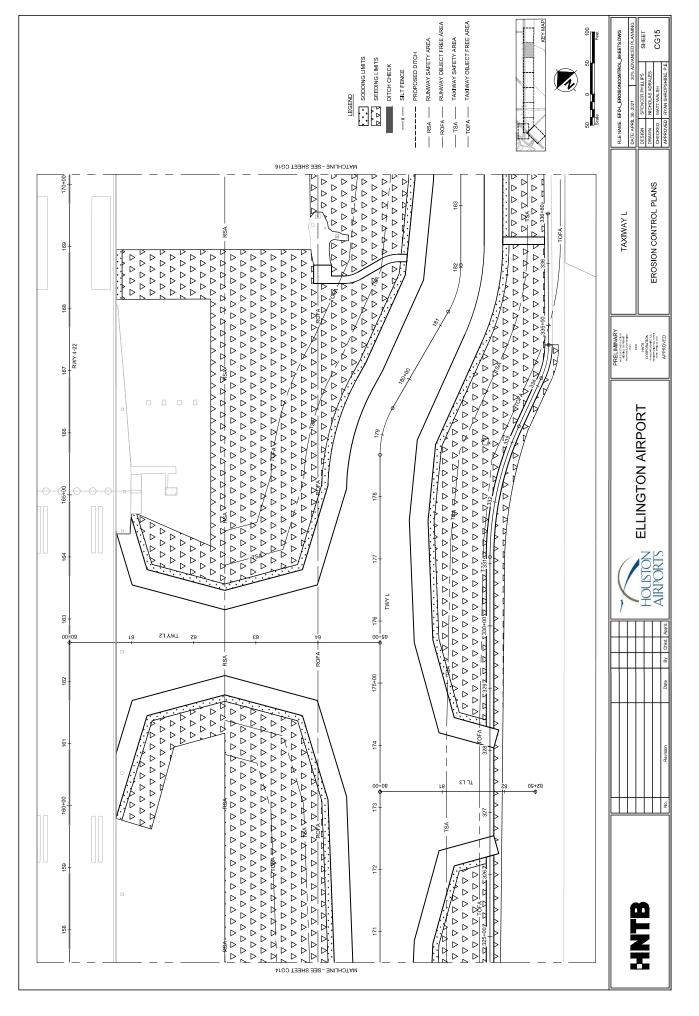


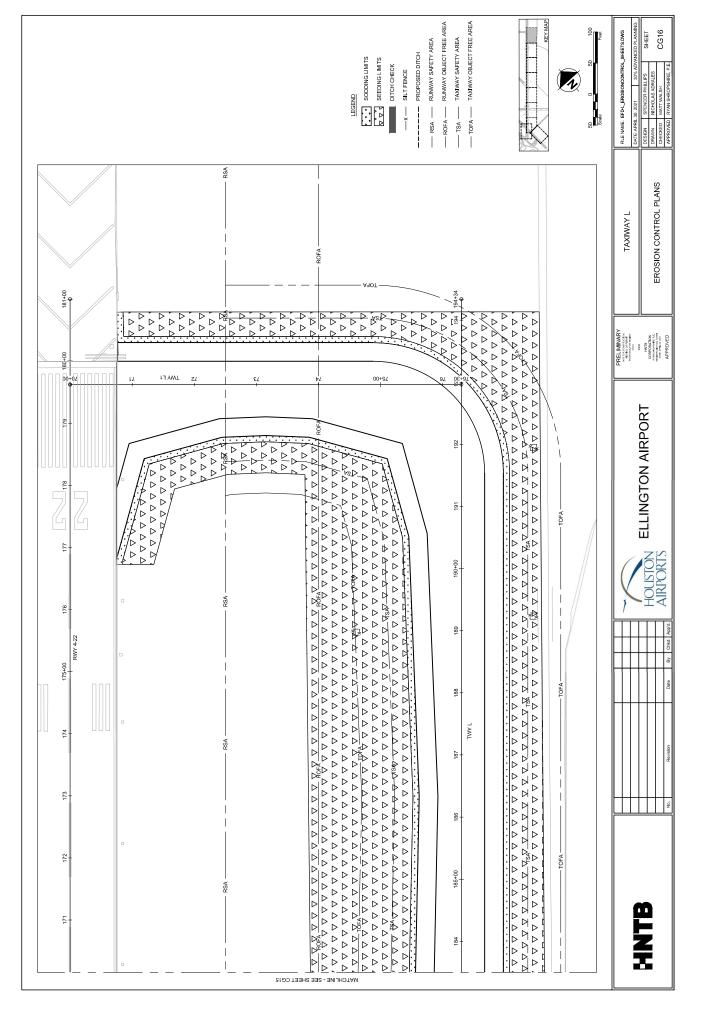


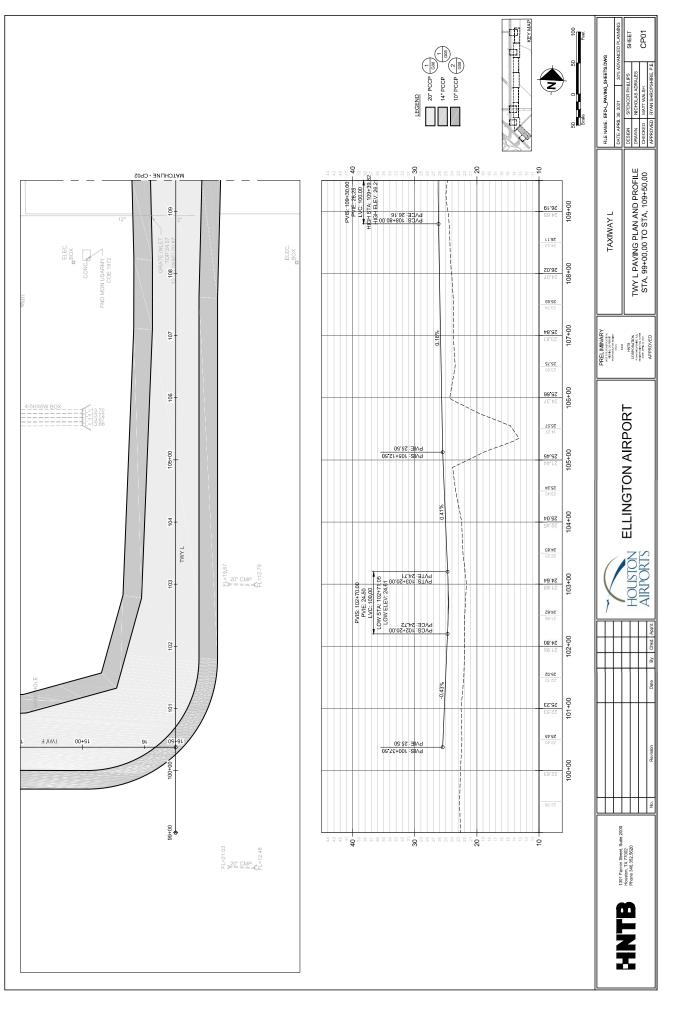
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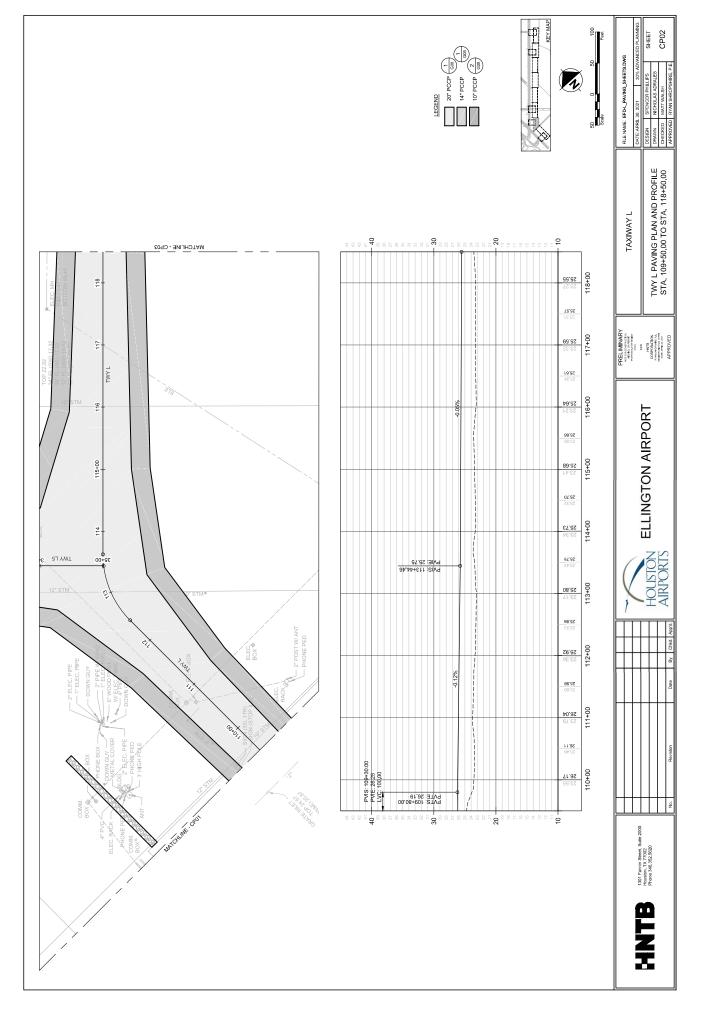


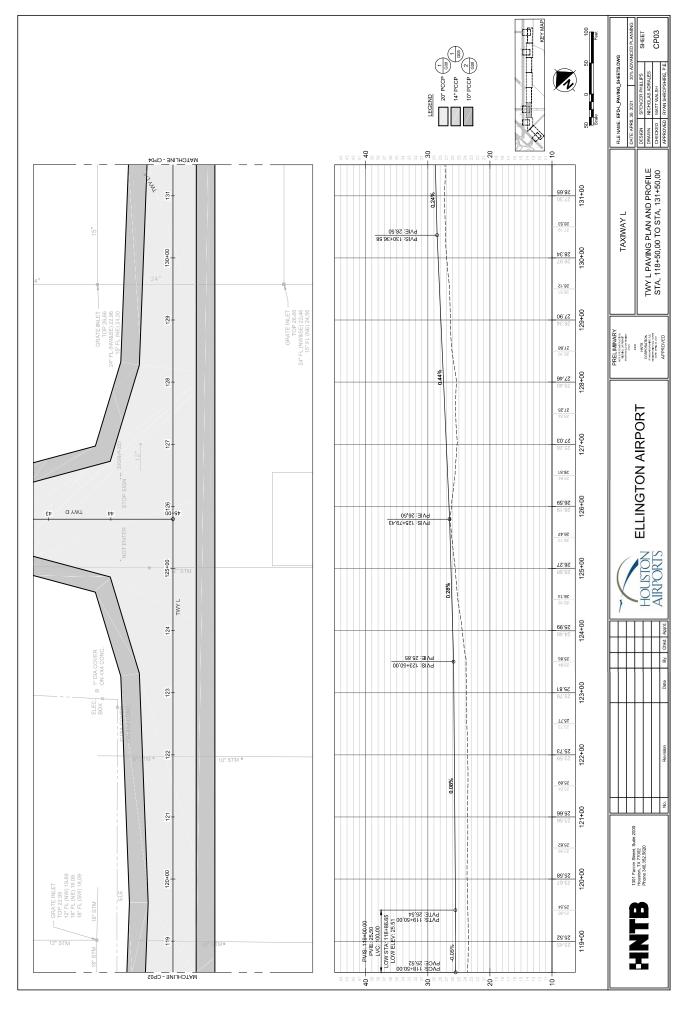


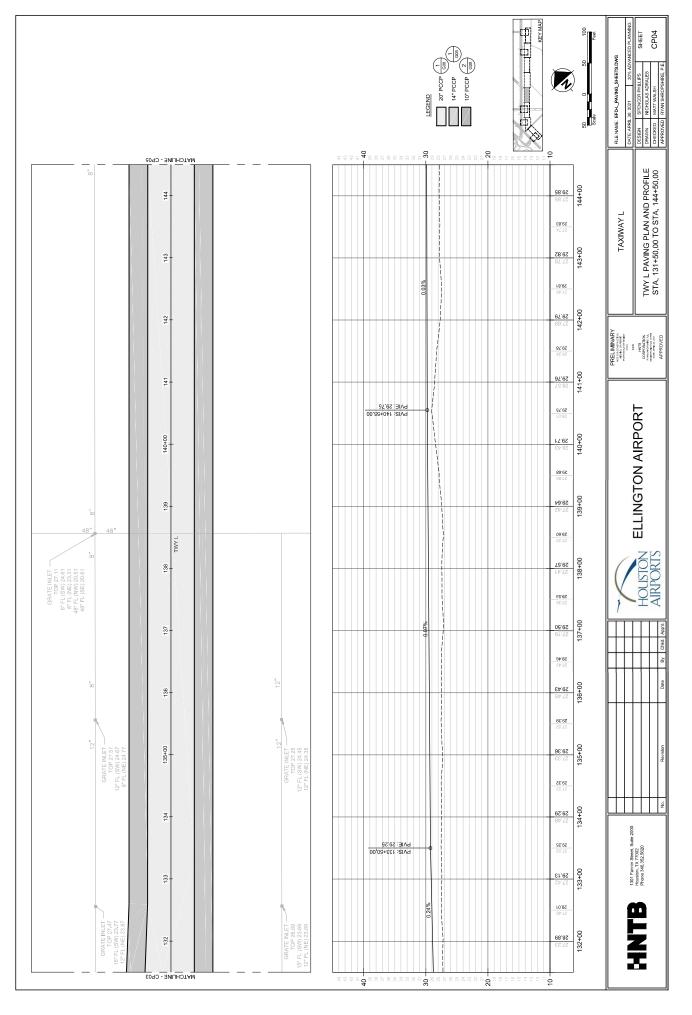


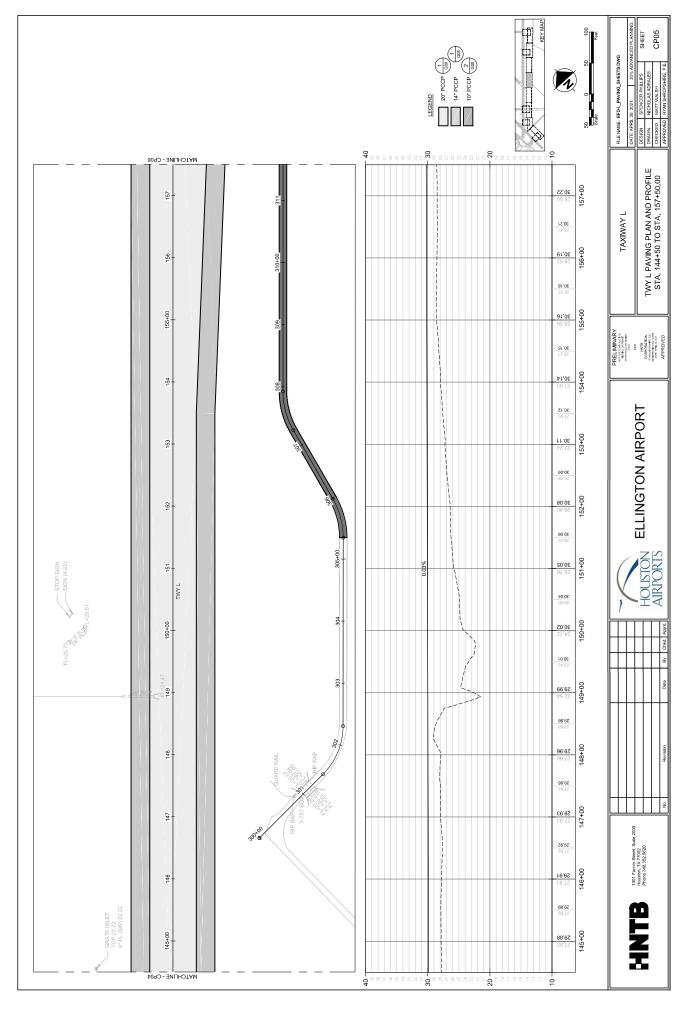


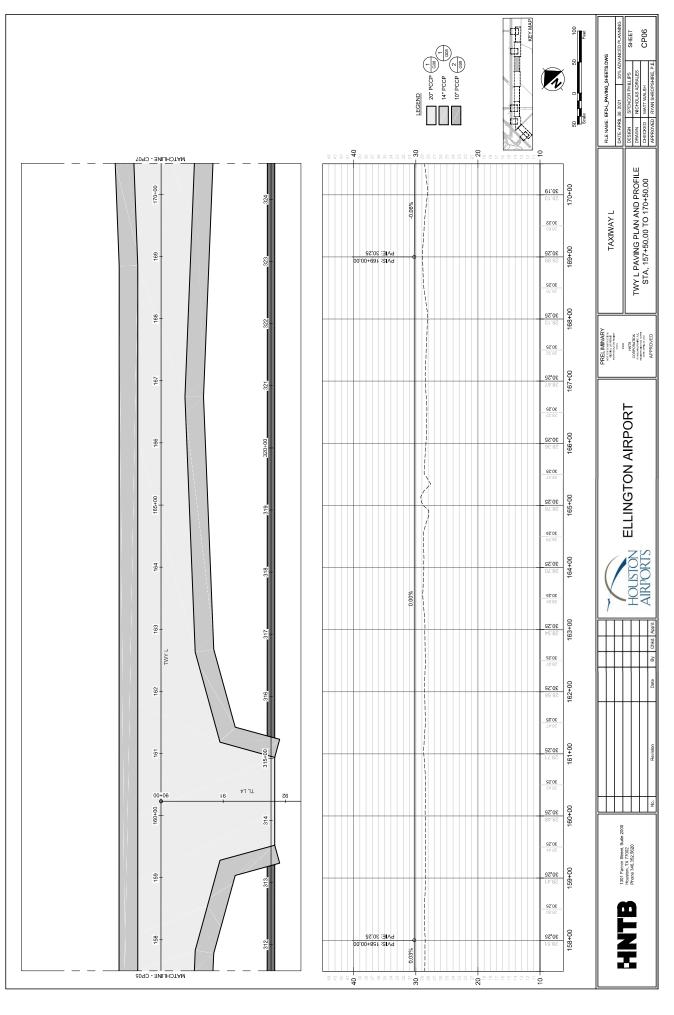
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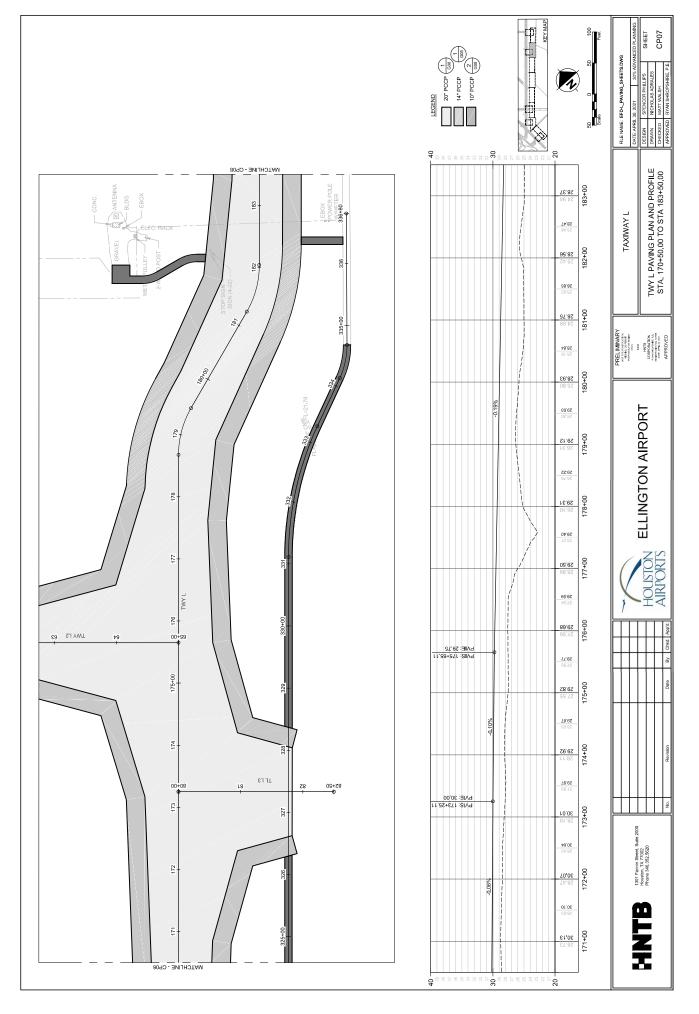


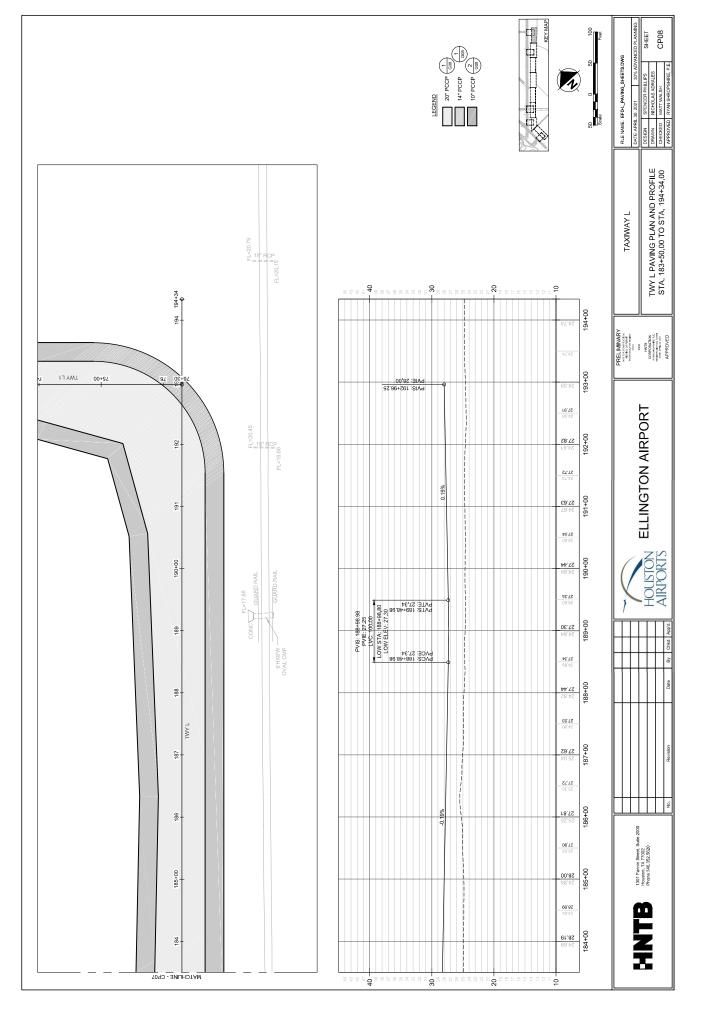


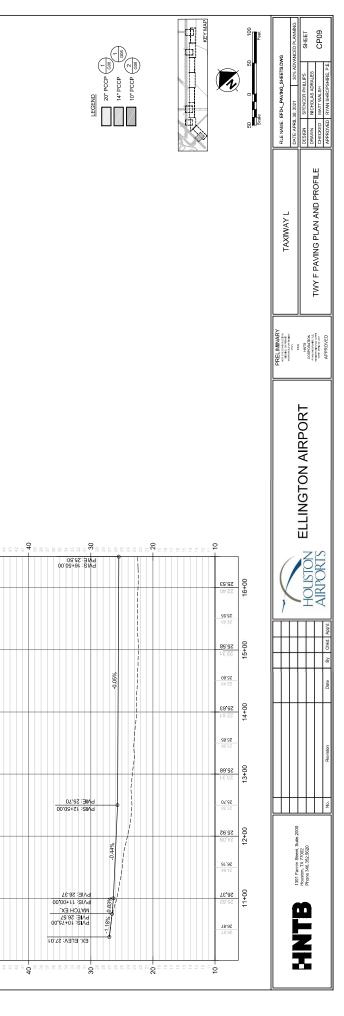


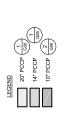












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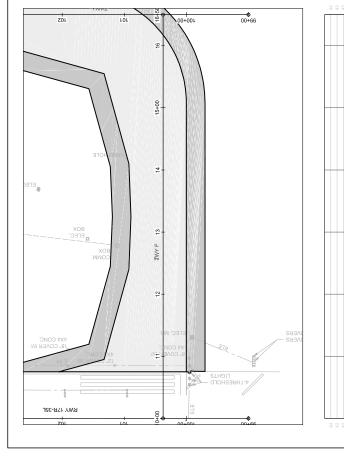
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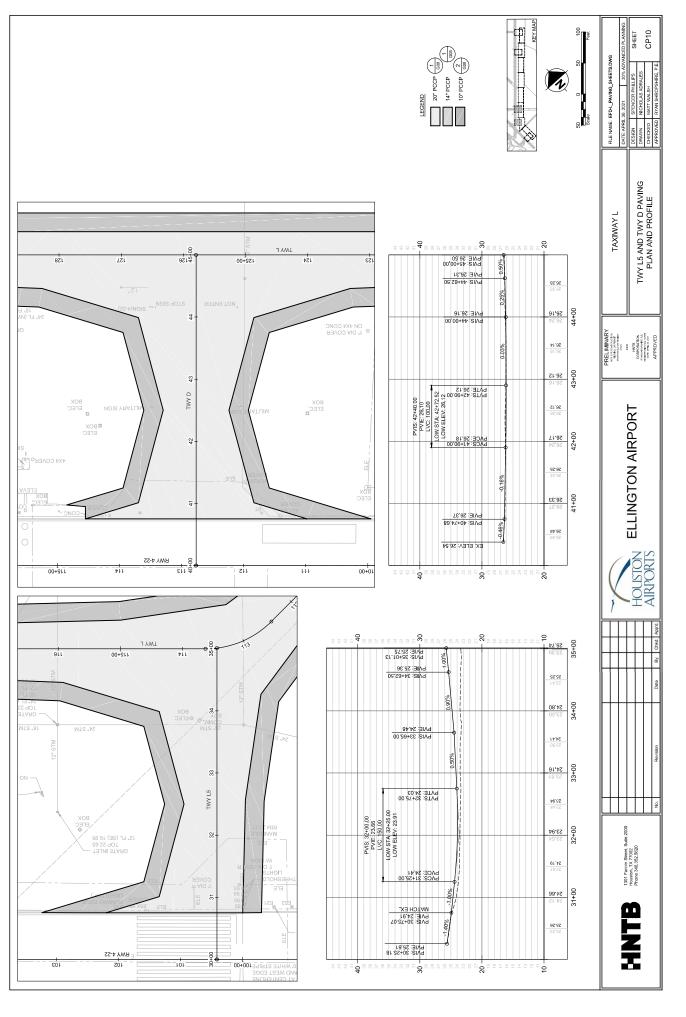
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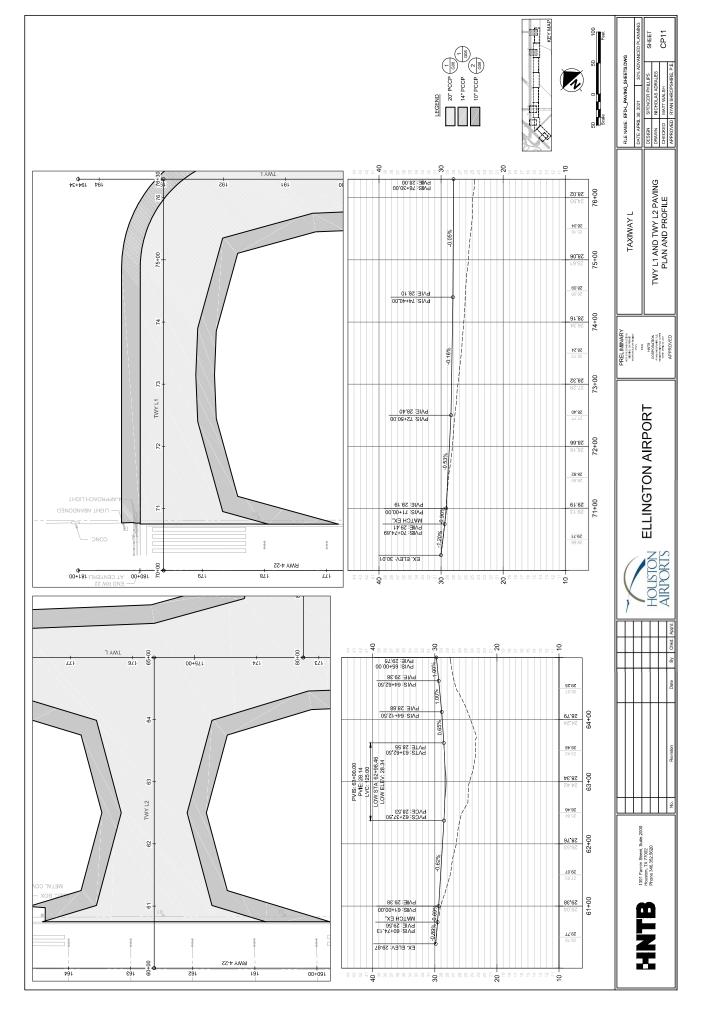
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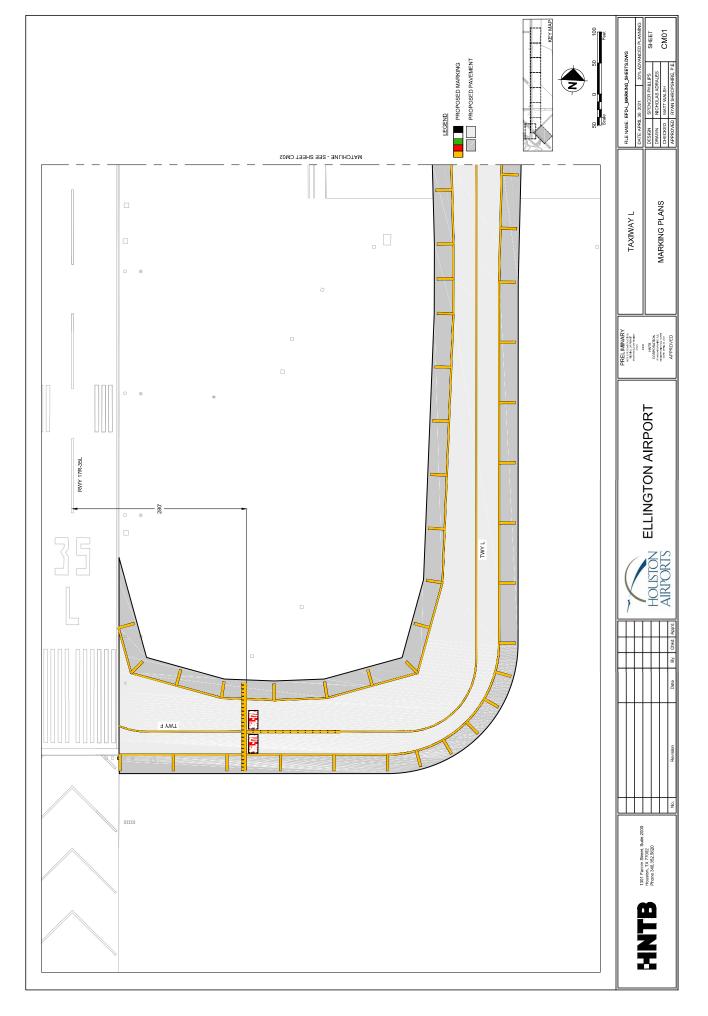
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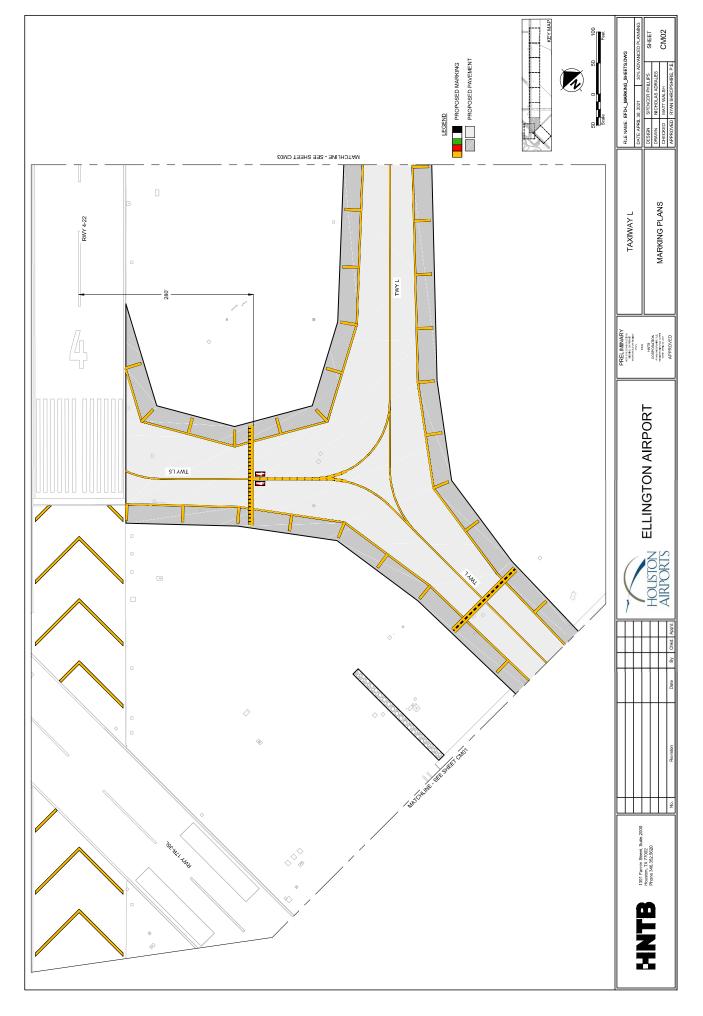
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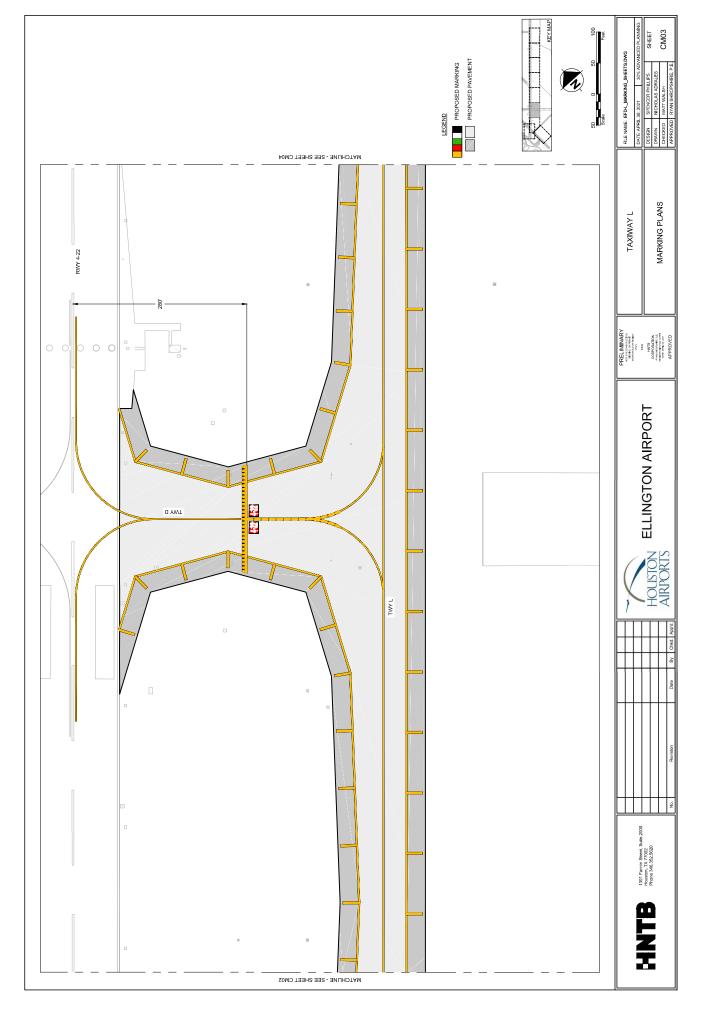


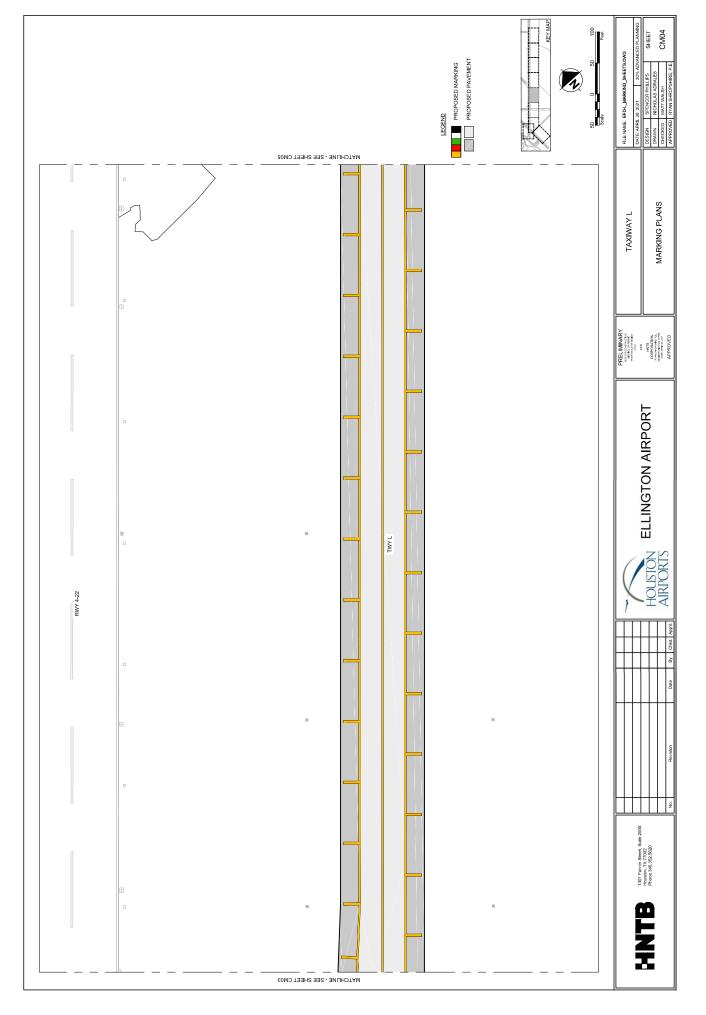


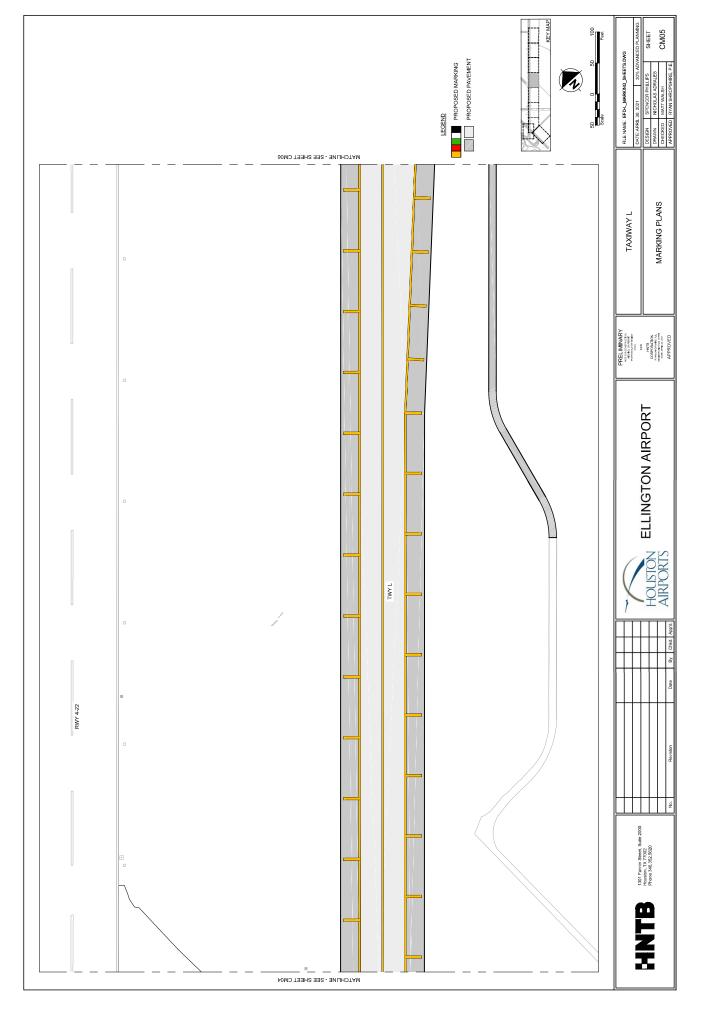


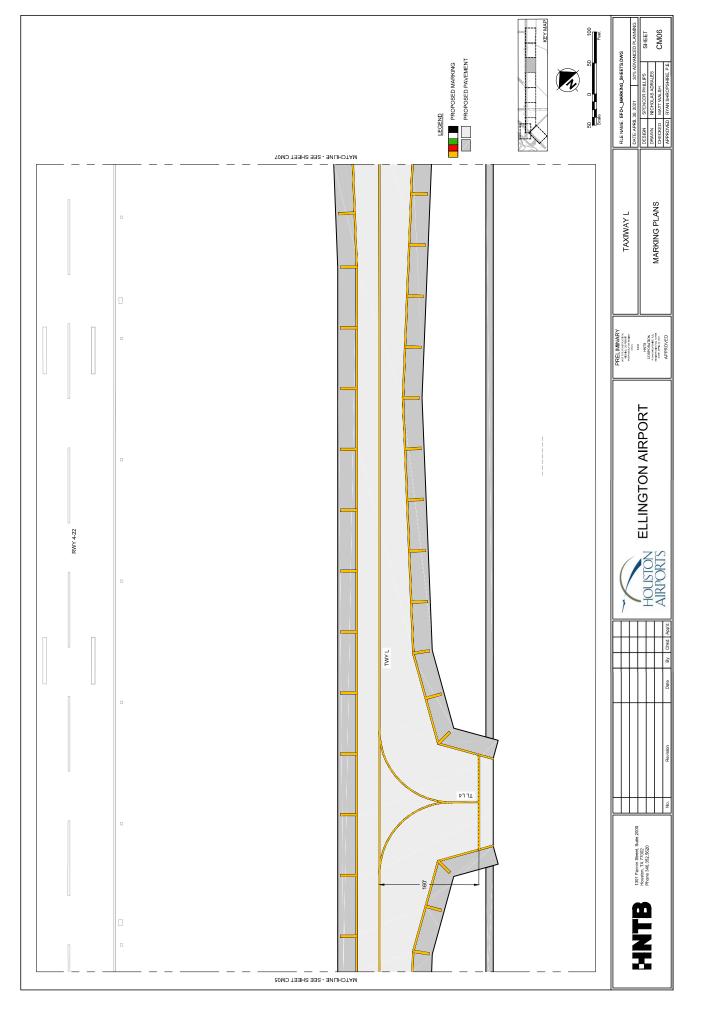


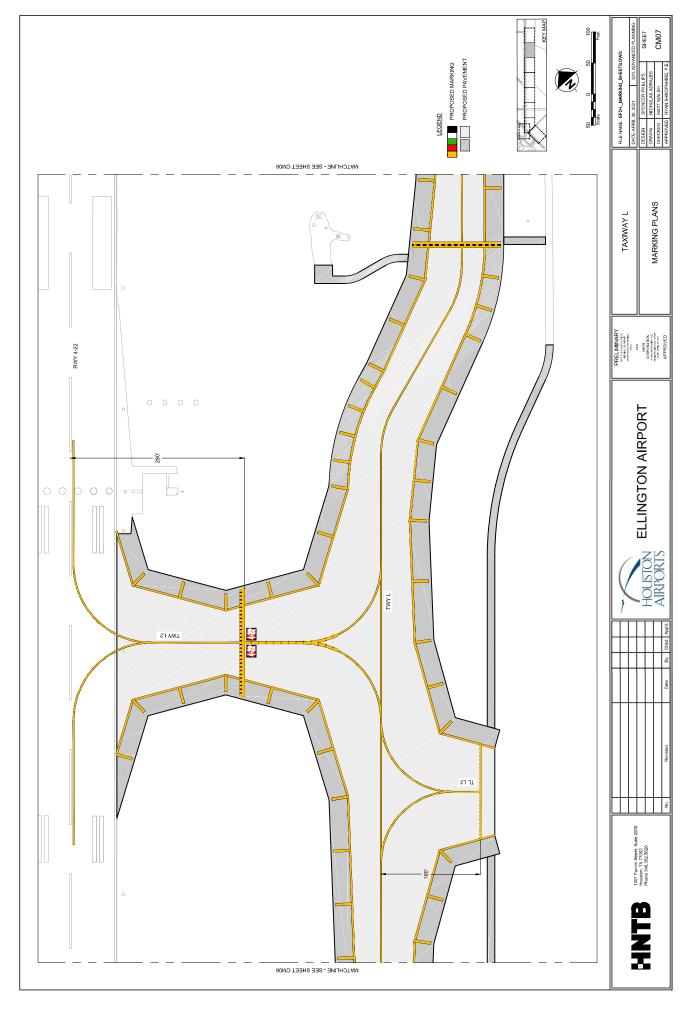


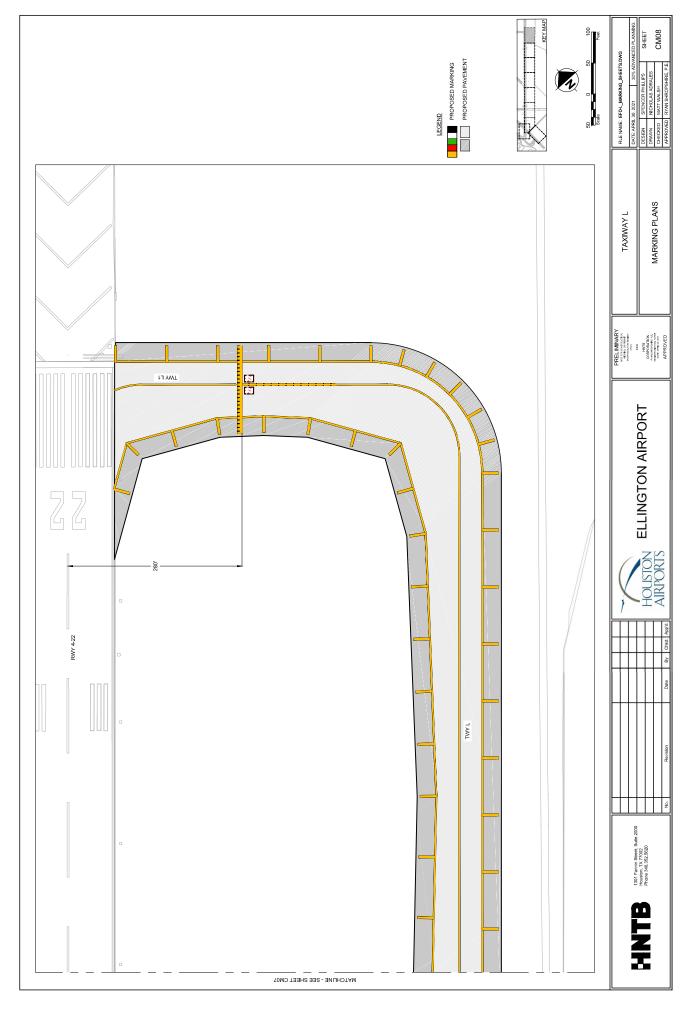


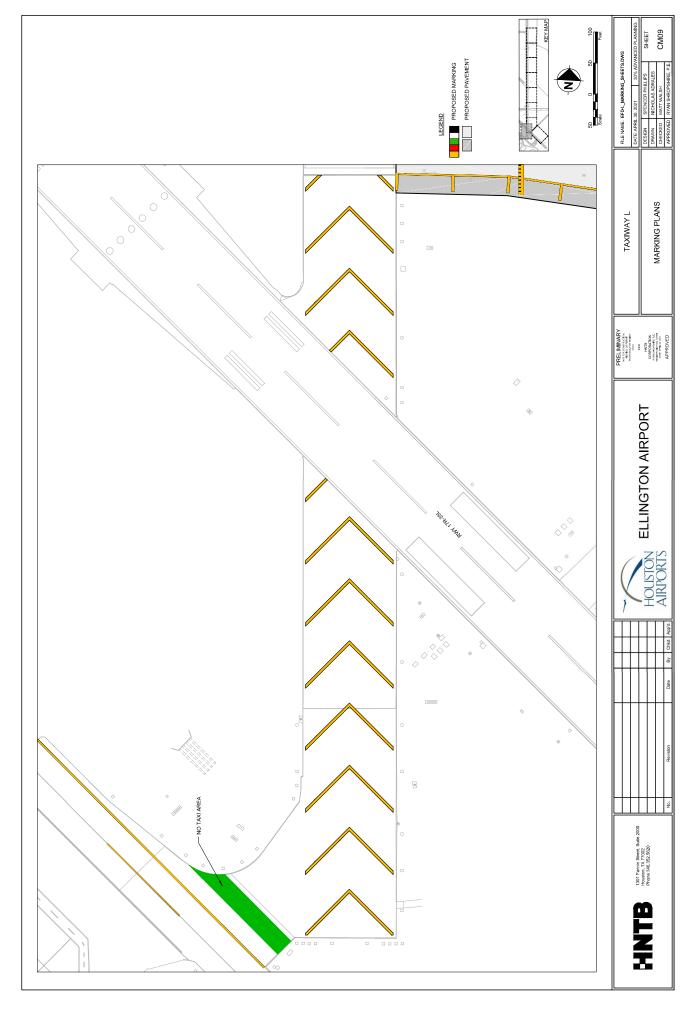


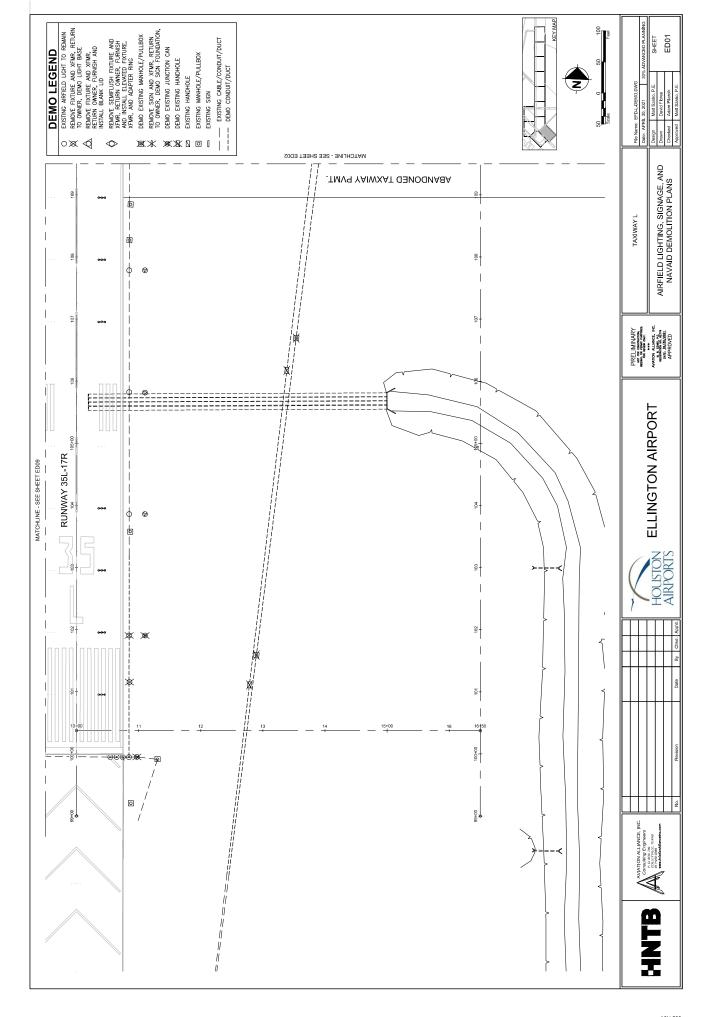


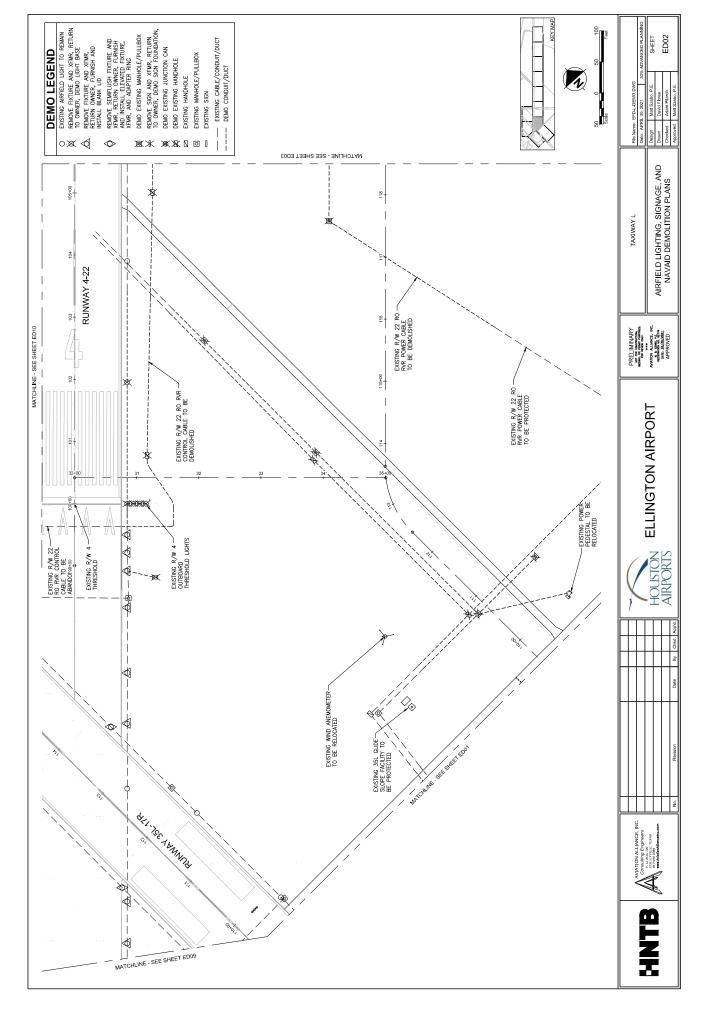


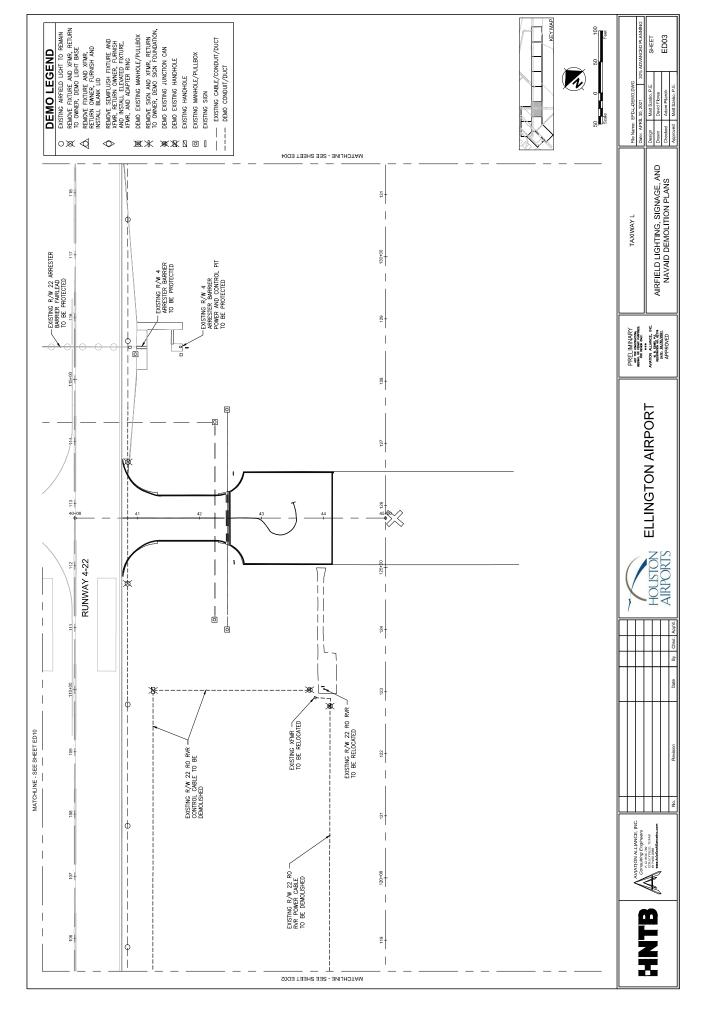


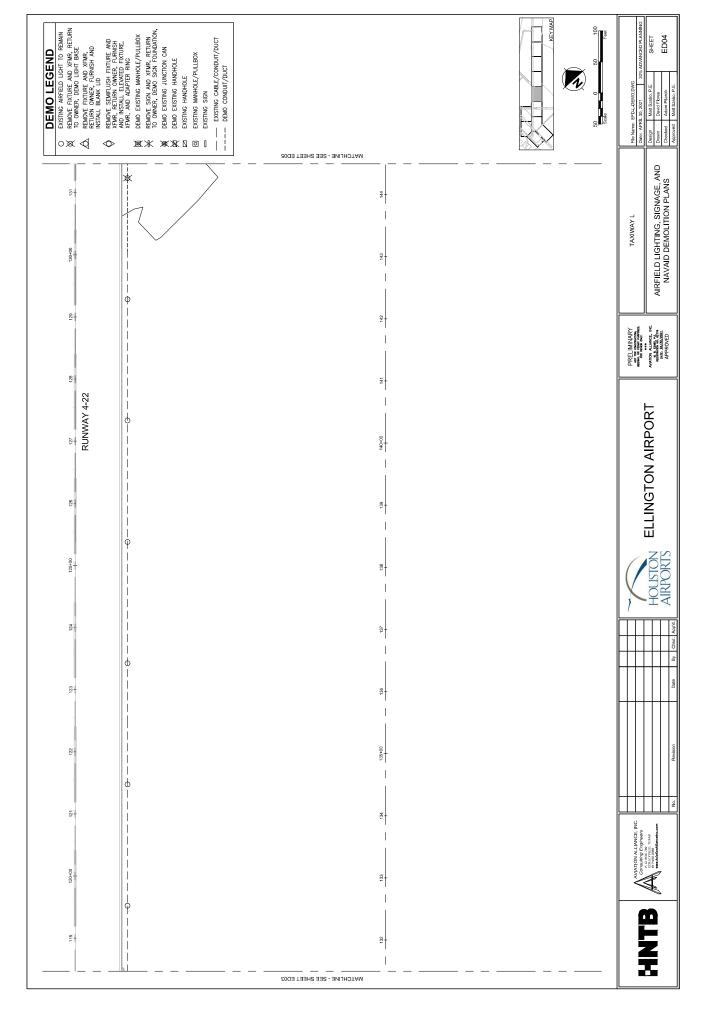


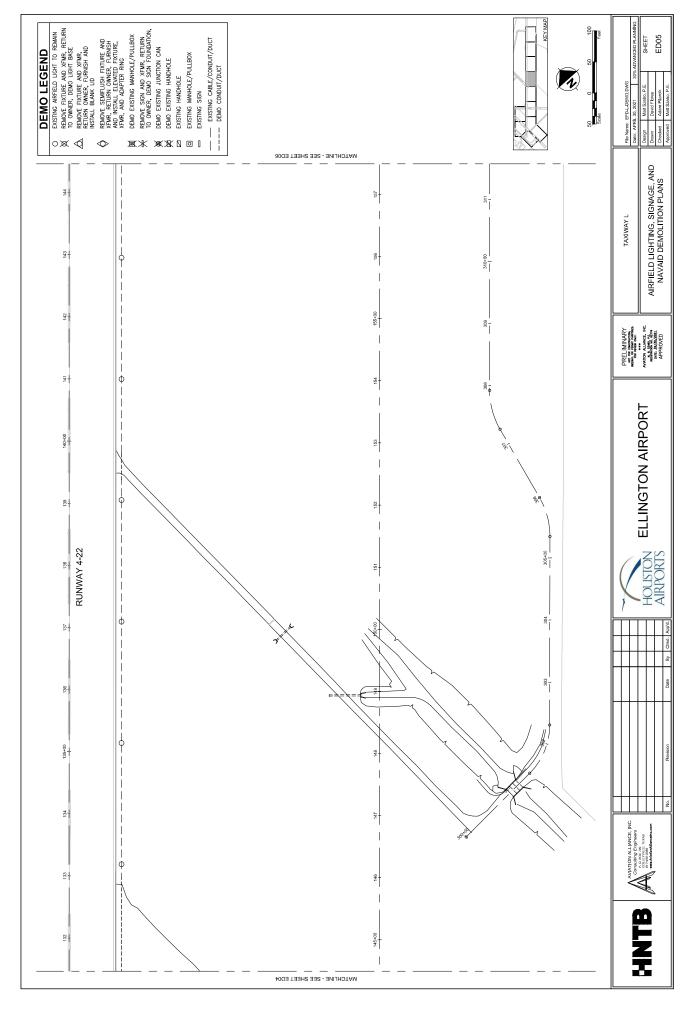


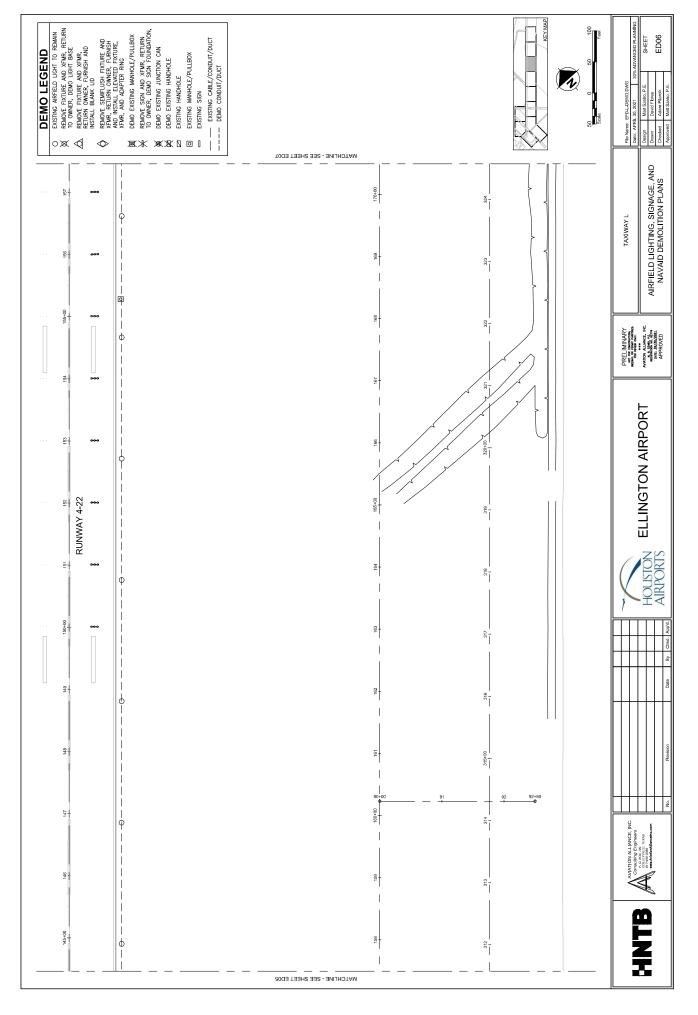


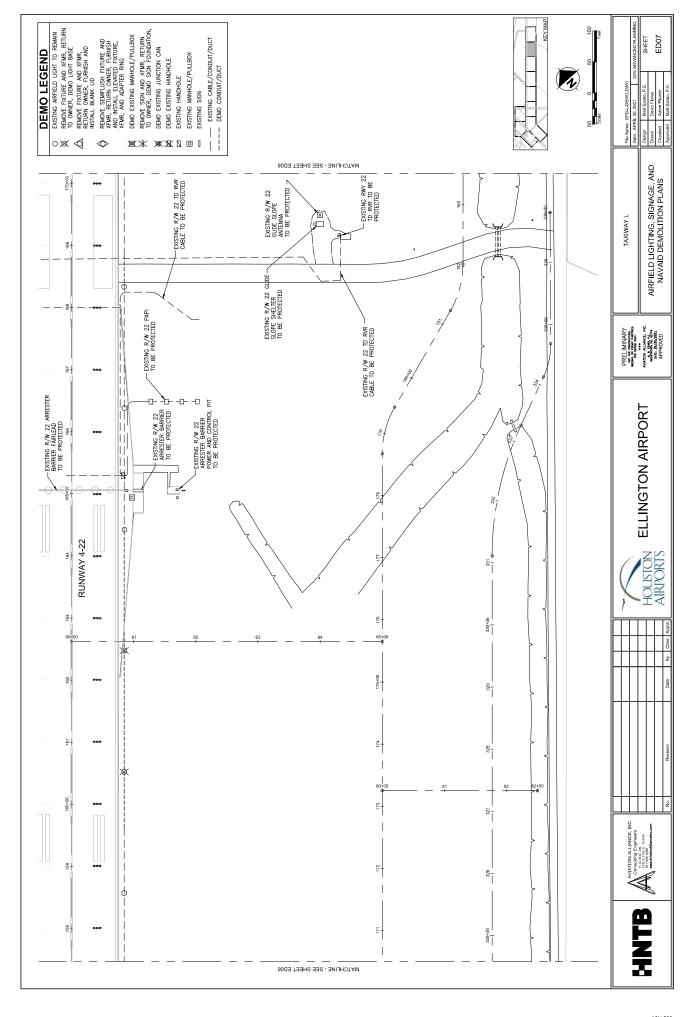


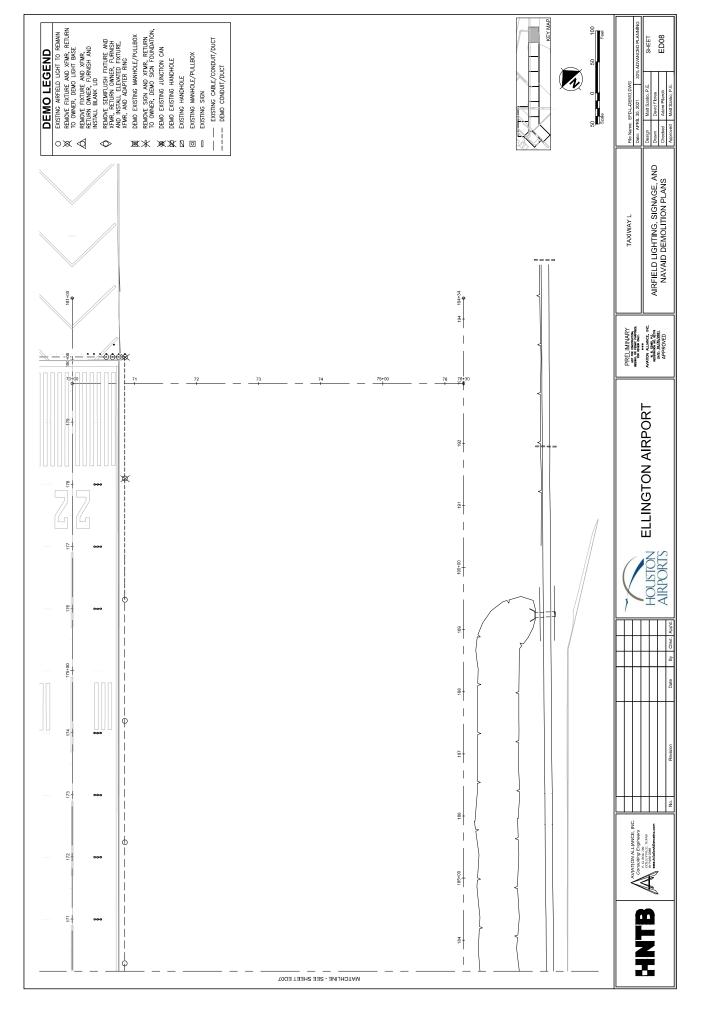


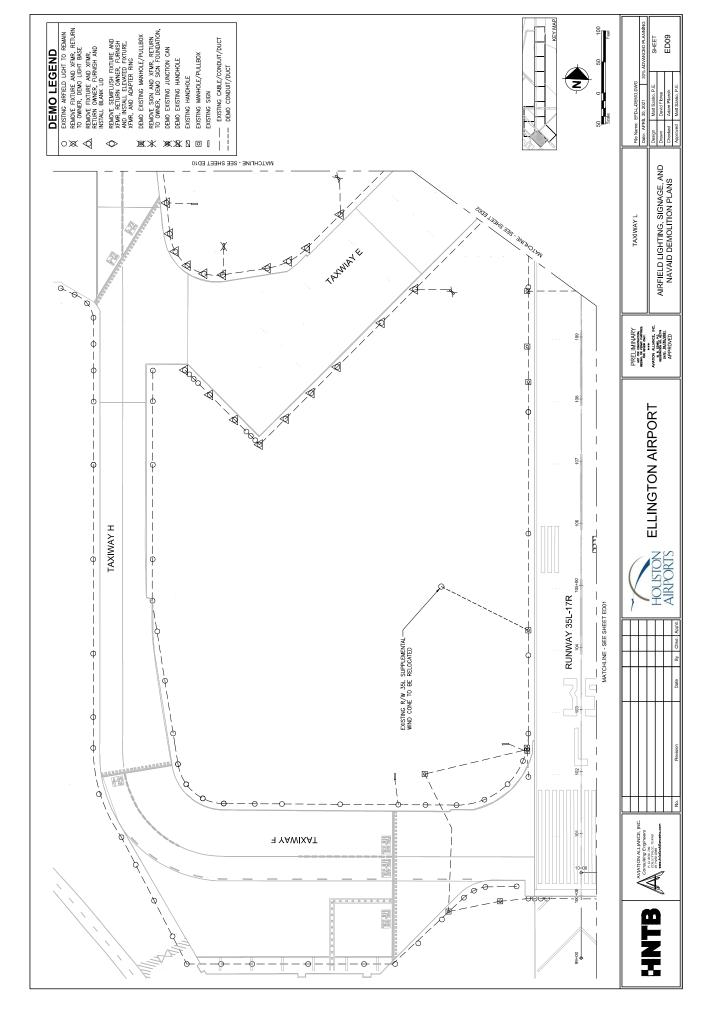


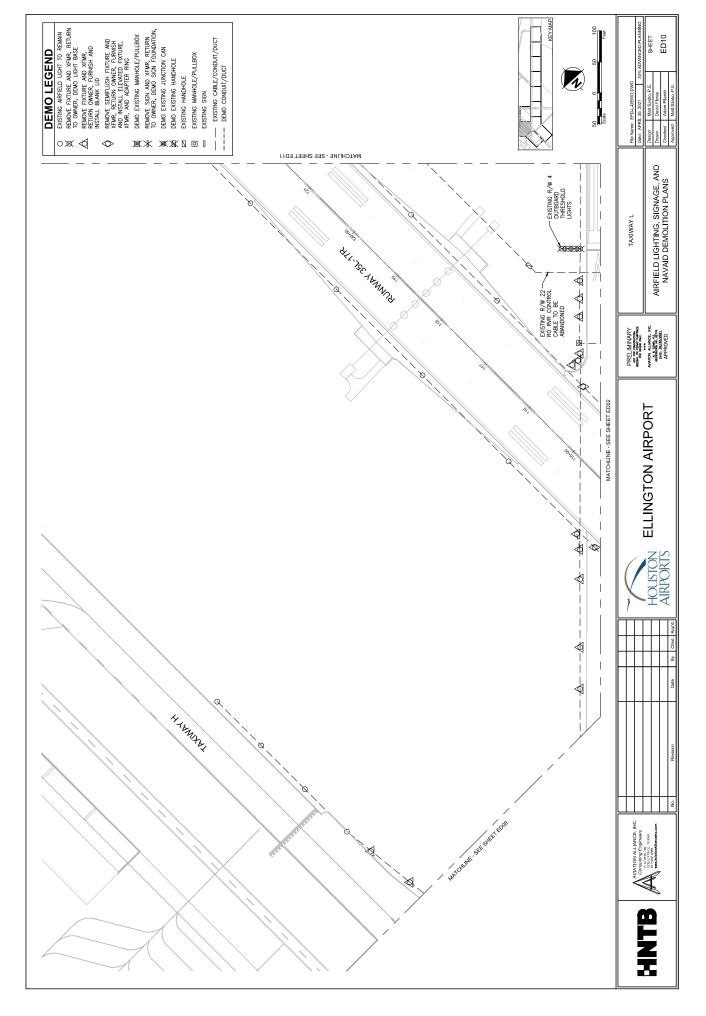


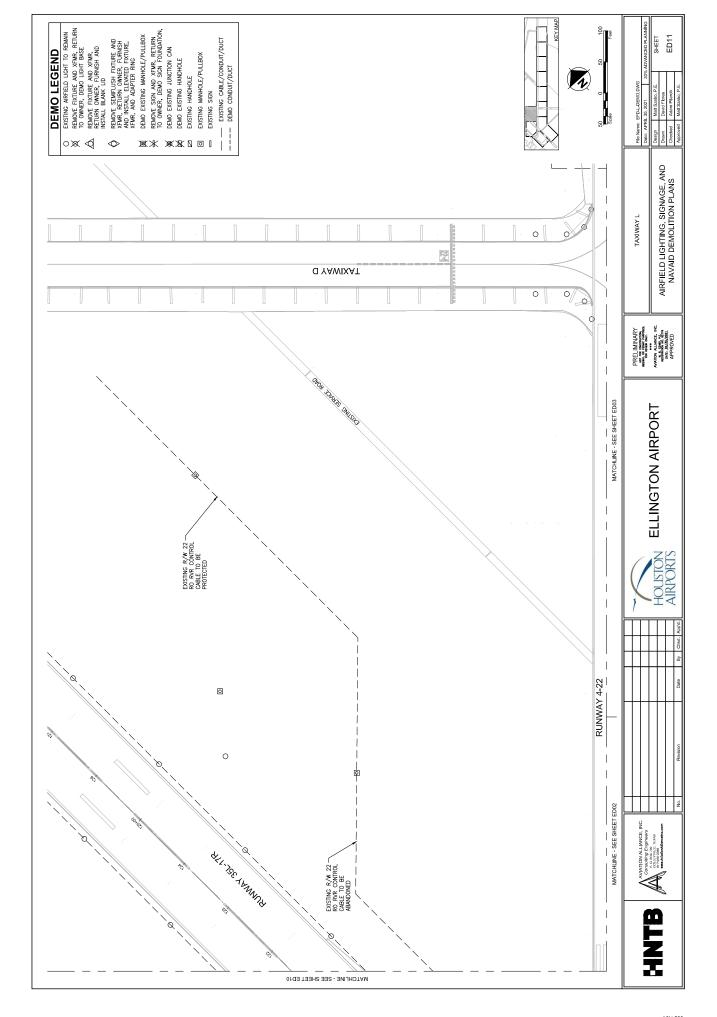


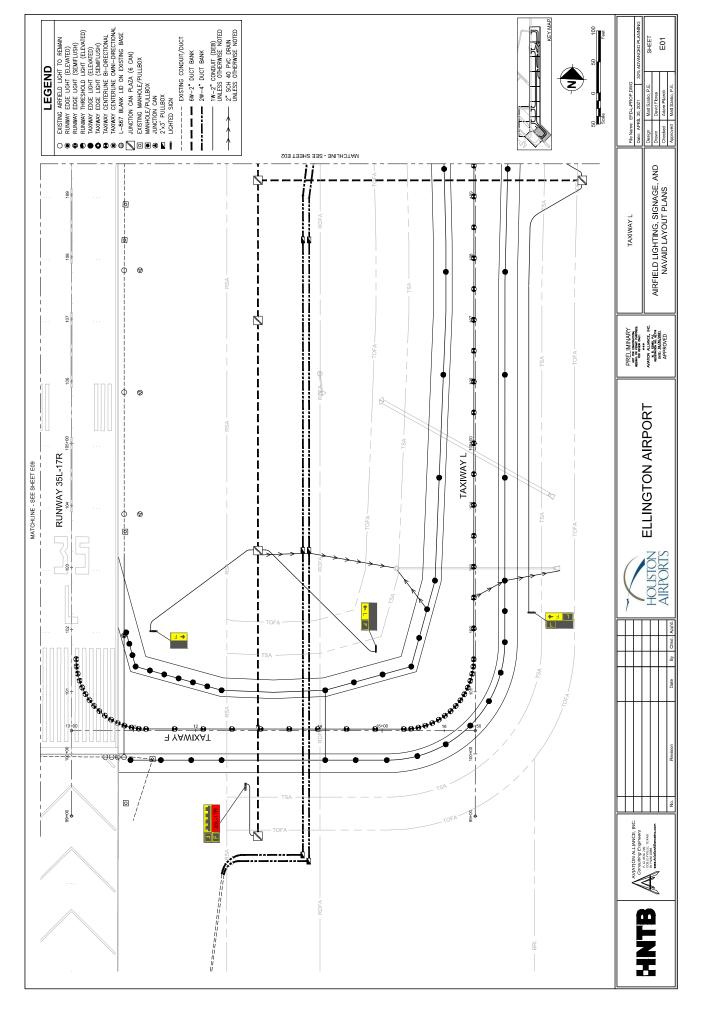


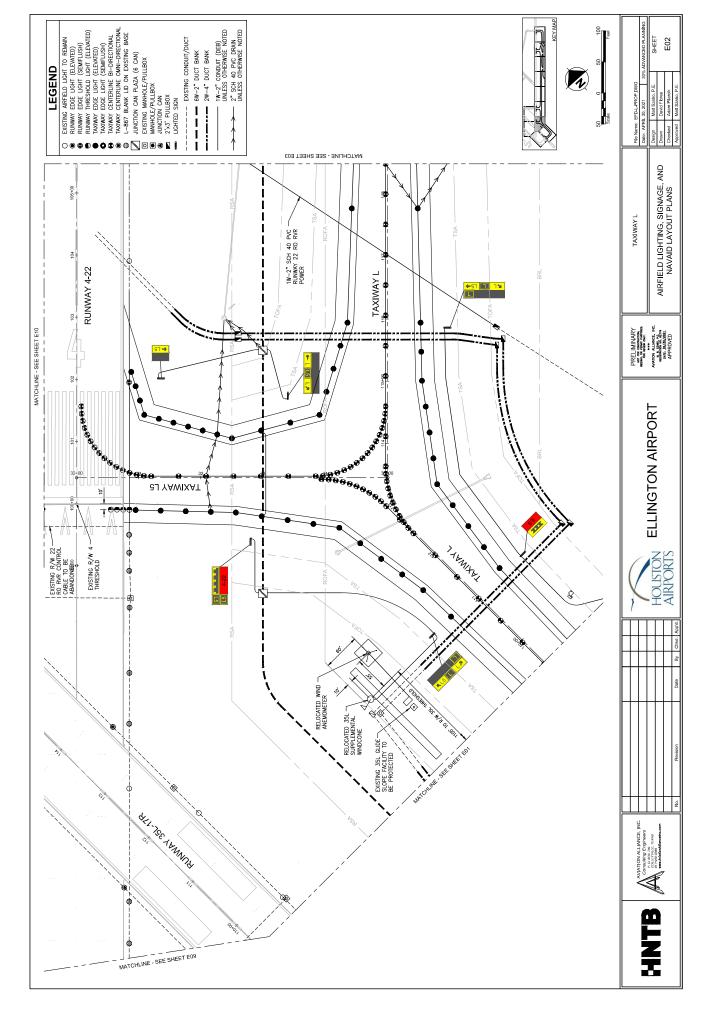




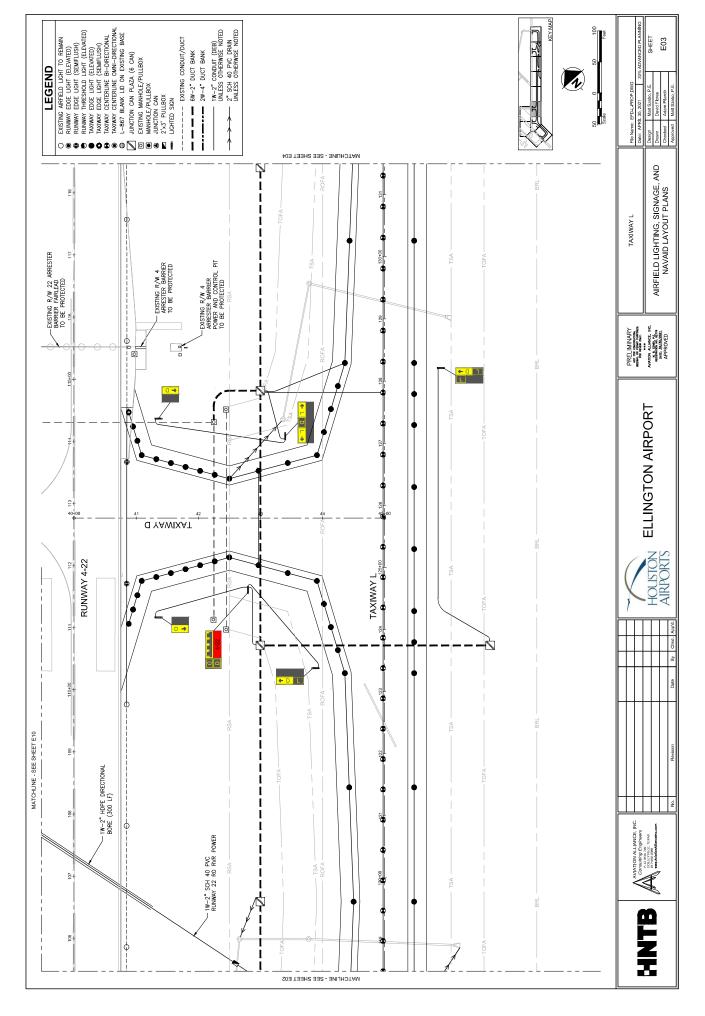


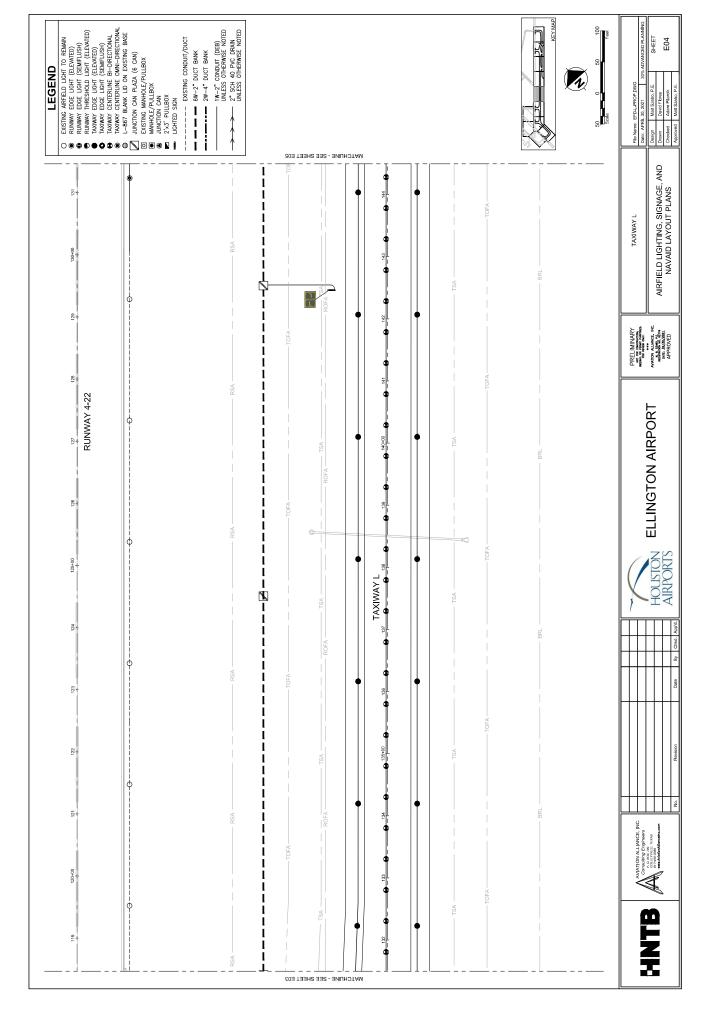


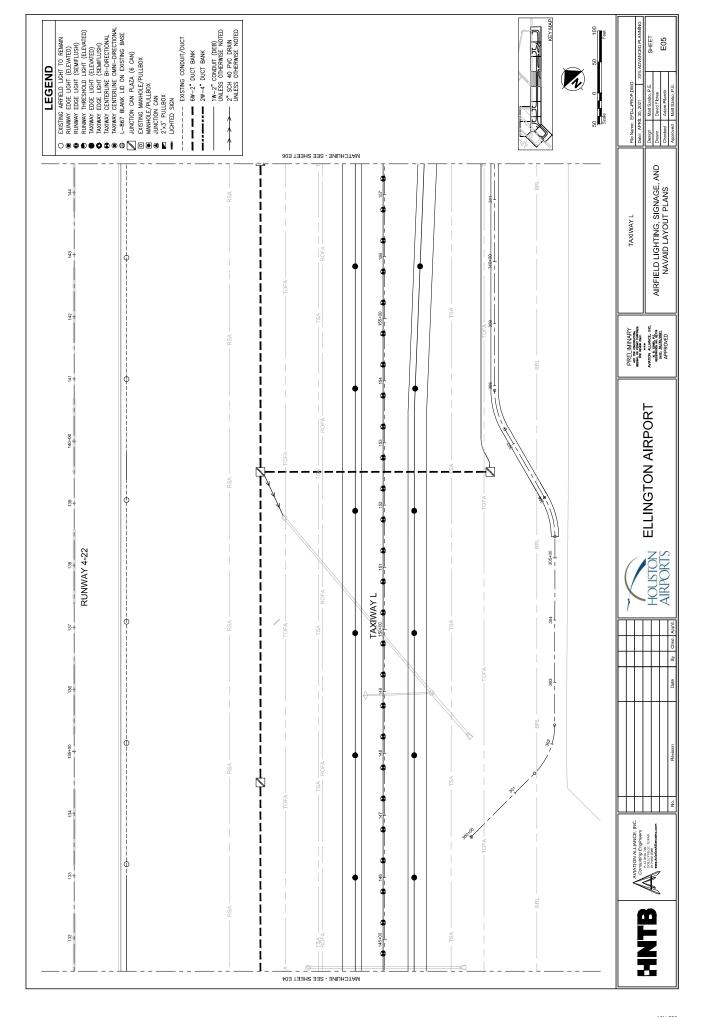


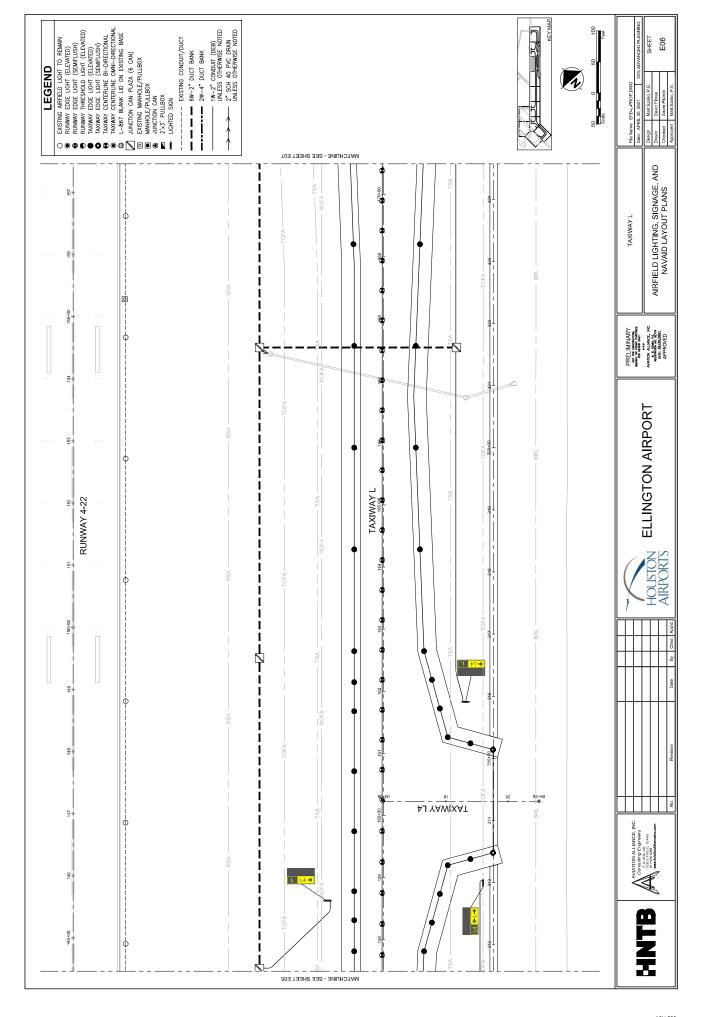


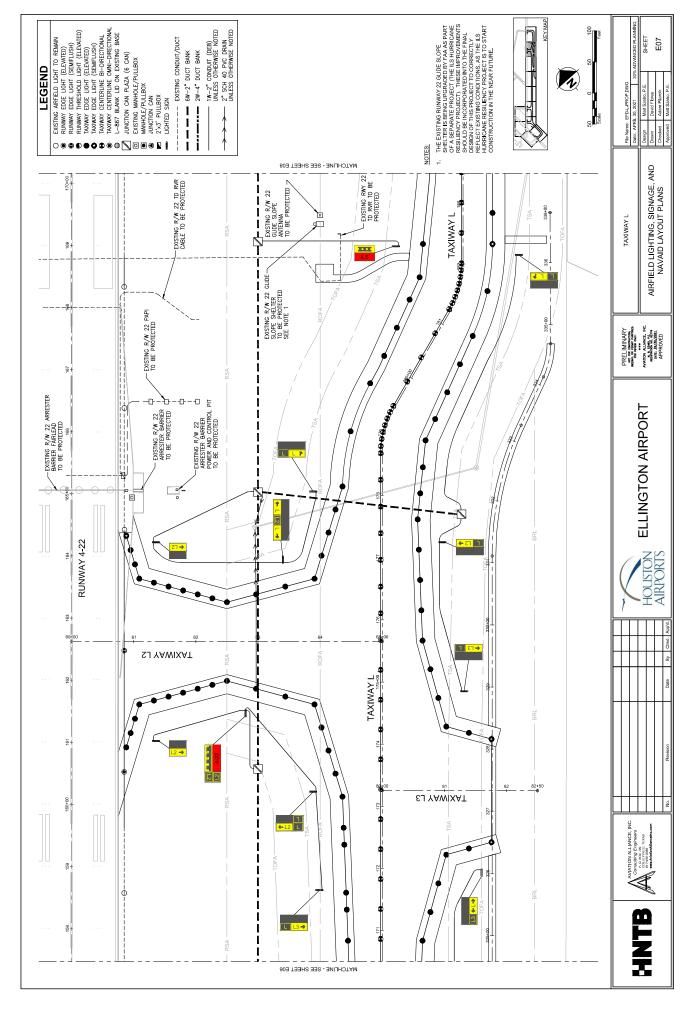
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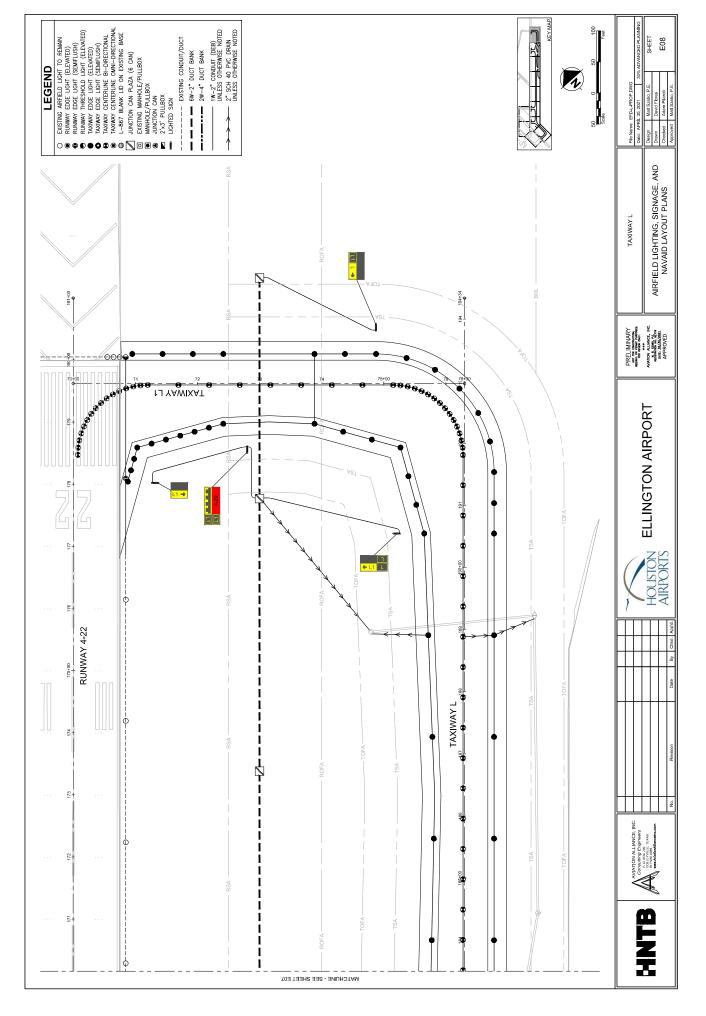


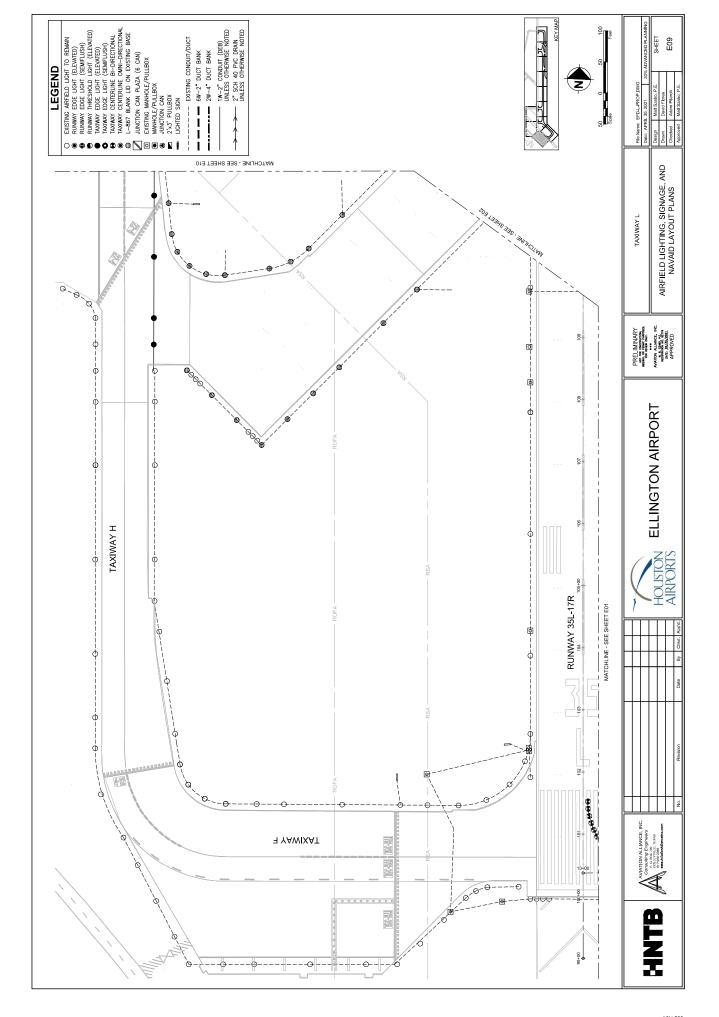


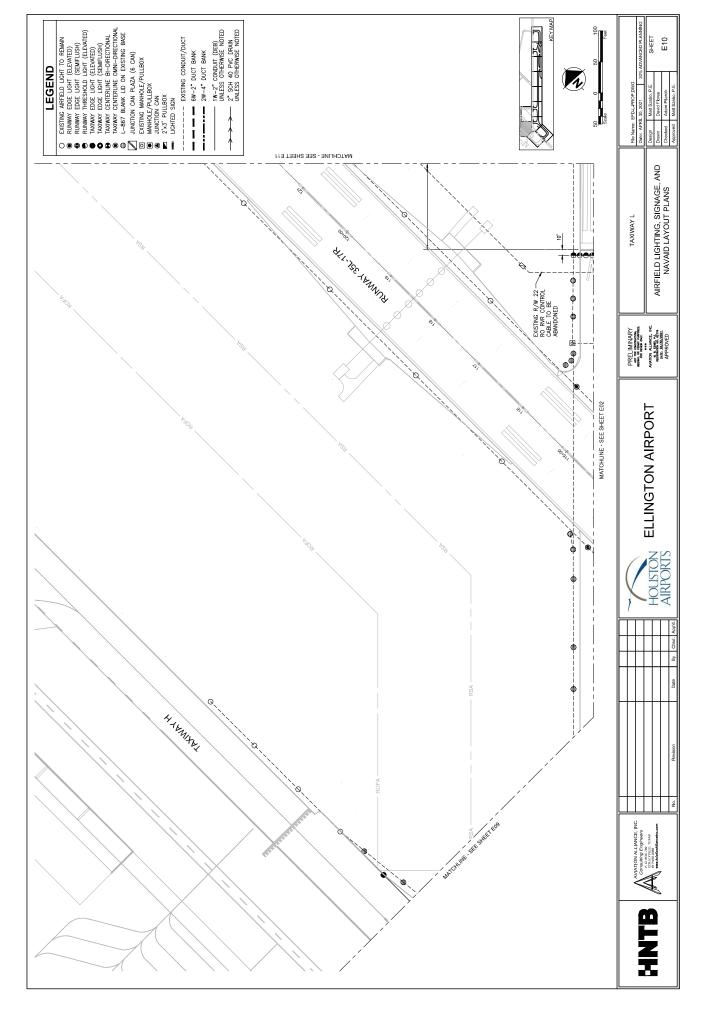


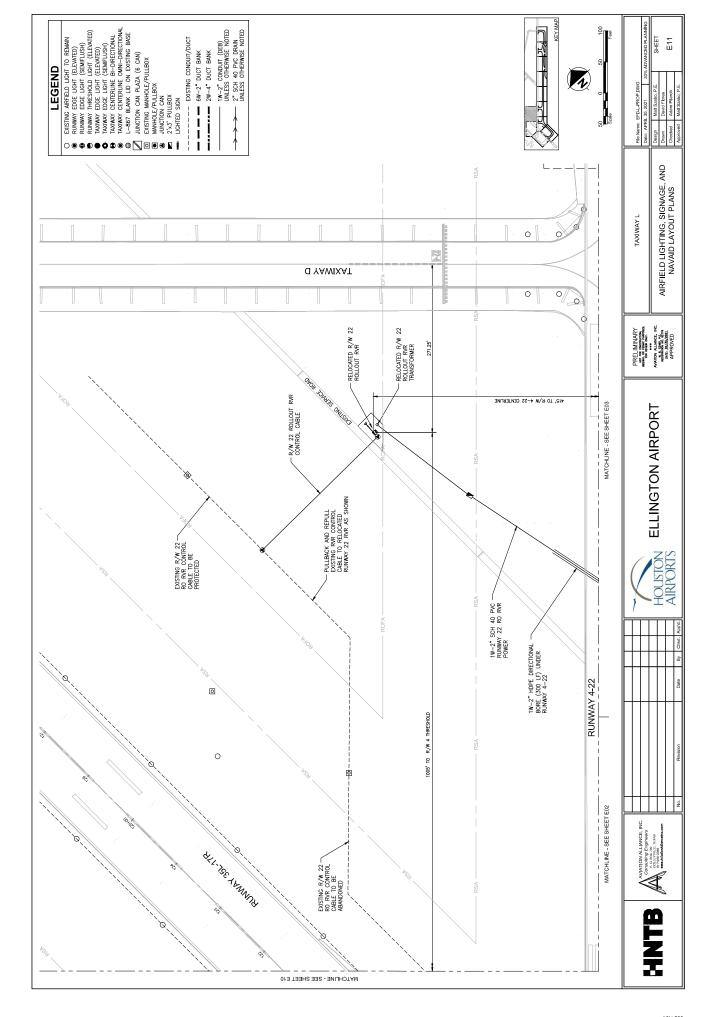












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V. List of Construction Specifications

Specification Number	Specification Title
C-100	Contractor Quality Control Program (CQCP)
C-102	Temporary Air and Water Pollution, Soil Erosion, and Siltation Control
C-105	Mobilization
C-110	Method of Estimating Percentage of Material Within Specification Limits (PWL)
P-101	Preparation/Removal of Existing Pavements
P-151	Clearing and Grubbing
P-152	Excavation, Subgrade, and Embankment
P-155	Lime-Treated Subgrade
P-209	Crushed Aggregate Base Course
P-306	Lean Concrete Base Course
P-401	Asphalt Mix Pavement
P-501	Cement Concrete Pavement
P-604	Compression Joint Seals for Concrete Pavements
P-605	Joint Sealants for Pavements
P-620	Runway and Taxiway Marking
D-701	Pipe for Storm Drains and Culverts
D-705	Pipe Underdrains for Airports
D-751	Manholes, Catch Basins, Inlets and Inspection Holes
T-901	Seeding
T-904	Sodding
Т-908	Mulching
L-107	Airport Wind Cones
L-108	Underground Power Cable for Airports
L-109	Airport Transformer Vault and Vault Equipment
L-110	Airport Underground Electrical Duct Banks and Conduits
L-111	Airfield Electrical Installation Testing
L-115	Electrical Manholes and Junction Structures
L-125	Installation of Airport Lighting Systems
L-1005	Aggregate Cover



November 29, 2021

Mr. John Verburg, P.E. Atkins North America, Inc. 200 Westlake Park Blvd, Suite 1100 Houston, Texas 77079

Re: Geotechnical Investigation - Addendum Lime-stabilized CBR Test Results Houston Airport System Taxiway L Geotechnical Investigation At Ellington Airport (EFD) Houston, Texas AEC Job No.: G103-21A

Dear Mr. Verburg,

This letter report is an addendum to Aviles Engineering Corporation's (AEC) Geotechnical Investigation Report G103-21 (dated October 22, 2021) for the Houston Airport System's (HAS) Taxiway L project, located at Ellington Airport (IATA Airport Code: EFD), in Houston, Texas. The contents of this letter should only be used in conjunction with AEC's original report, G103-21.

The purpose of this letter is to: (i) provide the results of optimum lime content (Tex 121E), lime-stabilized Modified Proctor (ASTM D 1557), and lime-stabilized California Bearing Ratio (CBR, ASTM D 1883) tests on soil recovered from four sample pits excavated along the Taxiway L alignment; and (ii) to provide maps from available literature (that were referenced in AEC Report G103-21) that show the approximate locations of geologic faults in the project area.

Lime-Stabilized Soil Test Results

<u>Optimum Lime Content</u>: AEC performed optimum lime content tests on composite samples from the test pits (collected from the ground surface to a depth of 4 feet) in accordance with Texas Department of Transportation (TxDOT) Test Method Tex 121E. The optimum lime content is the percentage of lime (by dry soil weight) that will achieve a pH of 12.4. The results of our optimum lime content tests are summarized on Table 1 and are presented on Plates A-1 through A-4, in Appendix A.

Sample ID and Description	Optimum Lime Content (pH = 12.4)	
B-8, 0'-4', Fat Clay (CH)	10%	
B-19, 0'-4', Fat Clay (CH)	8%	
B-31, 0'-4', Lean Clay with Sand (CL)	8%	
B-44, 0'-4', Lean Clay (CL)	8%	

Table 1.	Optimum	Lime Content	Results (Гех 121E)
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Based on the test results presented in Table 1, AEC recommends that a lime-stabilization rate of 8 percent be considered for pavement and taxiway subgrade stabilization purposes for this project.

5790 Windfern • Houston, Texas 77041 • (713) 895-7645 • Fax (713) 895-7943



<u>Compaction and CBR</u>: Soil (from the ground surface to a depth of 4 feet below grade) recovered from the sample pits was mixed and split in general accordance with ASTM C 702. After splitting, the samples were stabilized with 8 or 10 percent lime (by dry soil weight) and were molded and compacted in accordance with ASTM D 1557 (Modified Proctor). After the samples were compacted, there were allowed to cure for 72 hours in a moist state and then soaked for a period of 96 hours (total cure period of 7 days) and a CBR (ASTM D 1883) test was performed.

Modified Proctor compaction test results on soils stabilized with 8 or 10 percent lime (by dry soil weight) are presented on Plates A-5 through A-8, in Appendix A. CBR test results on soils stabilized with 8 or 10 percent lime (by dry soil weight) are presented on Plates A-9 through A-16, in Appendix A. A summary of the Modified Proctor and CBR test results on lime-stabilized soils are presented on Table 2 and Table 3, respectively.

Sample ID and Description	ASTM D 1557 Maximum Dry Density (pcf)	ASTM D 1557 Optimum Moisture Content (%)
B-8, 0'-4', Fat Clay (CH) with 10% lime	104.2	15.8
B-19, 0'-4', Fat Clay (CH) with 8% lime	112.0	12.8
B-31, 0'-4', Lean Clay with Sand (CL) with 8% lime	118.5	11.8
B-44, 0'-4', Lean Clay (CL) with 8% lime	115.7	13.7

Table 2. Lime-stabilized Modified Proctor Results (ASTM D 1557)

Table 3. California Bearing Ratio Test Results (ASTM D 1883)

Sample ID	Percent Compaction (%), ASTM D 1557	Dry Density (pcf)	CBR (%)
	100	104.2	97.55
B-8, 0'-4', Fat Clay (CH)	95	99.0	40.60
with 10% lime	90	93.8	31.20
	85	88.6	<24.40
	100	112.0	100.25
B-19, 0'-4', Fat Clay (CH) with 8% lime	95	106.4	74.00
	90	100.8	46.20
	85	95.2	<31.25
	100	118.5	151.91
B-31, 0'-4', Lean Clay with Sand (CL) with 8% lime	95	112.6	87.7
	90	106.7	<51.47
	100	115.7	240.56
B-44, 0'-4', Lean Clay (CL) with 8% lime	95	109.9	171.50
	90	104.1	107.60
	85	98.3	<58.47

Geologic Fault Maps

Discussion of geologic faults in the project area is presented in Section 4.4 of AEC Report G103-21. As



requested by HAS, AEC has included the fault maps discussed in AEC Report G103-21. The fault map from "Principal Surface Faults in the Central Houston Metropolitan Area (after O' Neill, Van Siclen, with additions by C. Norman, May 13, 2004)" is presented on Plate B-1, in Appendix B, while "Active Faults in Southeastern Harris County, Texas", Geo I, pages 149 - 154, by Clanton, U.S. and Amsbury, D.L. is presented on Plate B-2, in Appendix B.

Limitations

This investigation was performed using the standard level of care and diligence normally practiced by recognized geotechnical engineering firms in this area, presently performing similar services under similar circumstances. This letter report is intended to be used in its entirety. The report has been prepared exclusively for the project and location described in this report. If pertinent project details change or otherwise differ from those described herein, AEC should be notified immediately and retained to evaluate the effect of the changes on the recommendations presented in this report, and revise the recommendations if necessary. The recommendations presented in this report should not be used for other structures located along these alignments or similar structures located elsewhere, without additional evaluation and/or investigation.

AVILES ENGINEERING CORPORATION (TBPELS Firm Registration F-42)

Wilber L. Wang, P.E. Senior Engineer 11/29/21

Attachments: Appendix <u>A</u>	
Plates A-1 to A-4	Optimum Lime Content Test Results
Plates A-5 to A-8	Lime-stabilized Modified Proctor Test Results
Plates A-9 to A-16	Lime-stabilized California Bearing Ratio (CBR) Test Results
Appendix B	
Plate B-1	"Principal Surface Faults of the Houston Central Metropolitan Area"
Plate B-2	"Active Faults in Southeastern Harris County, Texas"



APPENDIX A

Plates A-1 to A-4	Optimum Lime Content Test Results
Plates A-5 to A-8	Lime-stabilized Modified Proctor Test Results
Plates A-9 to A-16	Lime-stabilized California Bearing Ratio (CBR) Test Results

Tex-121E Soil-Lime pH Curve

Project: Sample ID:	103-21 B-8	Date:	10/12/2021
Moisture Content of air	dried material:		
Tare ID:	G50		
Tare Wt (g):	82.22		
Wet + Tare (g):	92.36		

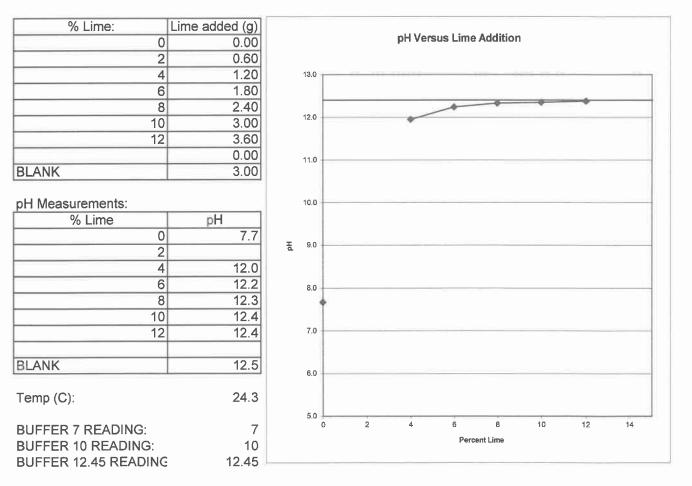
3.79 Mass of material equivalent to 30g oven-dried material: 31.14

91.99

Lime Additions:

Dry + Tare (g):

W=



0

Optimum Stabilization (% Lime):



Tex-121E Soil-Lime pH Curve

Project:		103-21	Date:	10/12/2021
Sample ID:	B-19			

 Moisture Content of air dried material:

 Tare ID:
 G49

 Tare Wt (g):
 83.2

 Wet + Tare (g):
 93.94

 Dry + Tare (g):
 93.71

 W=
 2.19

Mass of material equivalent to 30g oven-dried material:

0 30.66

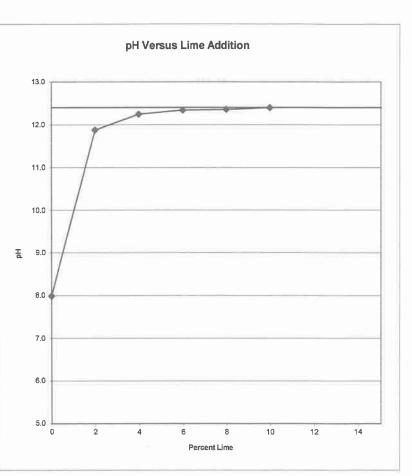
Lime Additions:

% Lime:		Lime added (g)
	0	0.00
	2	0.60
	4	1.20
	6	1.80
	8	2.40
	10	3.00
		0.00
		0.00
BLANK		3.00

% Lime	pН
0	8.0
2	
4	12.3
6	12.3
8	12.4
10	12.4
	12.3 12.4 12.4 12.4
BLANK	12.5

Temp (C):

BUFFER 7 READING: BUFFER 10 READING: BUFFER 12.45 READING



Optimum Stabilization (% Lime):



23.5

7

10

12.45

Tex-121E Soil-Lime pH Curve

Project:		103-21		Date:	10/11/2021
Sample ID:	B-31		,	1	

Moisture Content of air dried material: Tare ID: G49

Tare Wt (g):	83.21
Wet + Tare (g):	93.4
Dry + Tare (g):	93.25
W=	1.49

Mass of material equivalent to 30g oven-dried material:

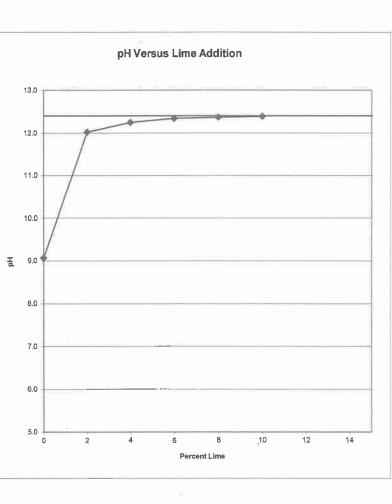
Lime Additions:

% Lime:		Lime added (g)
	0	0.00
	2	0.60
	4	1.20
	6	1.80
	8	2.40
	10	3.00
		0.00
		0.00
BLANK		3.00

pH Measurements:	
% Lime	pН
0	9.1
2	12.0
4	12.3
6	12.3
8	
10	12.4
BLANK	12.5

Temp (C):

BUFFER 7 READING: BUFFER 10 READING: BUFFER 12.45 READING



0

30.45

Optimum Stabilization (% Lime):

8

23.6

7

10

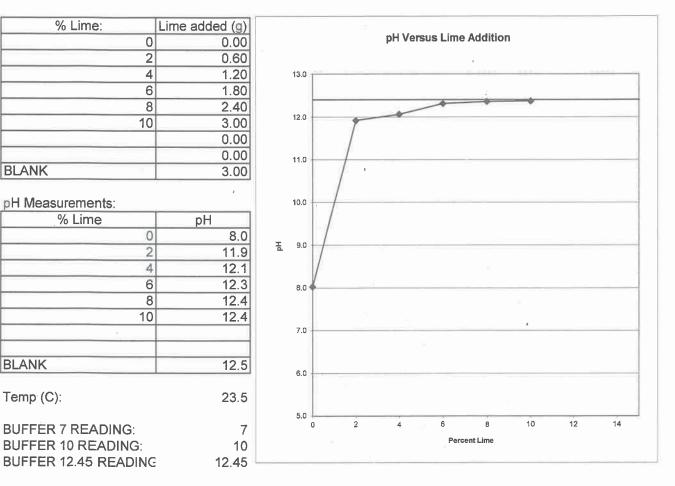
12.45

Tex-121E Soil-Lime pH Curve

Project: Sample ID:	B-44	103-21	I	Date:	10/11	1/2021
Moisture Content of ai	r dried mat	erial:		1		
Tare ID:		G50				
Tare Wt (g):		82.21				
Wet + Tare (g):		92.64				
Dry + Tare (g):		92.42				
W=		2.15				0
Mass of material equiv	alent to 30	g oven-drie	ed materia	l:		30.65

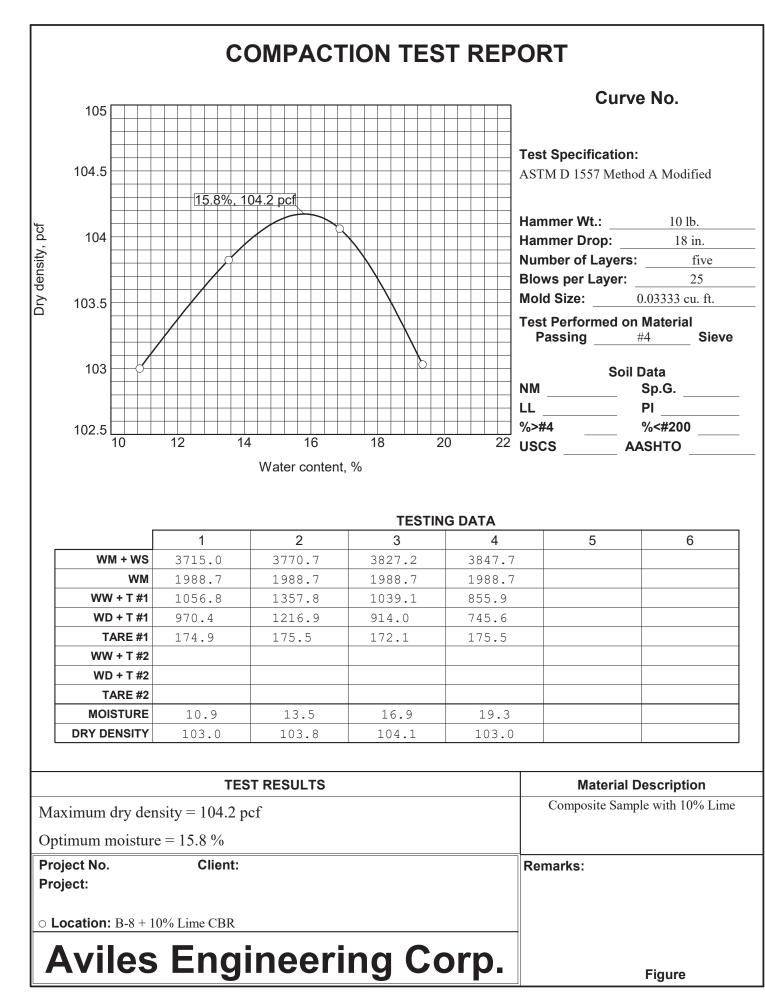
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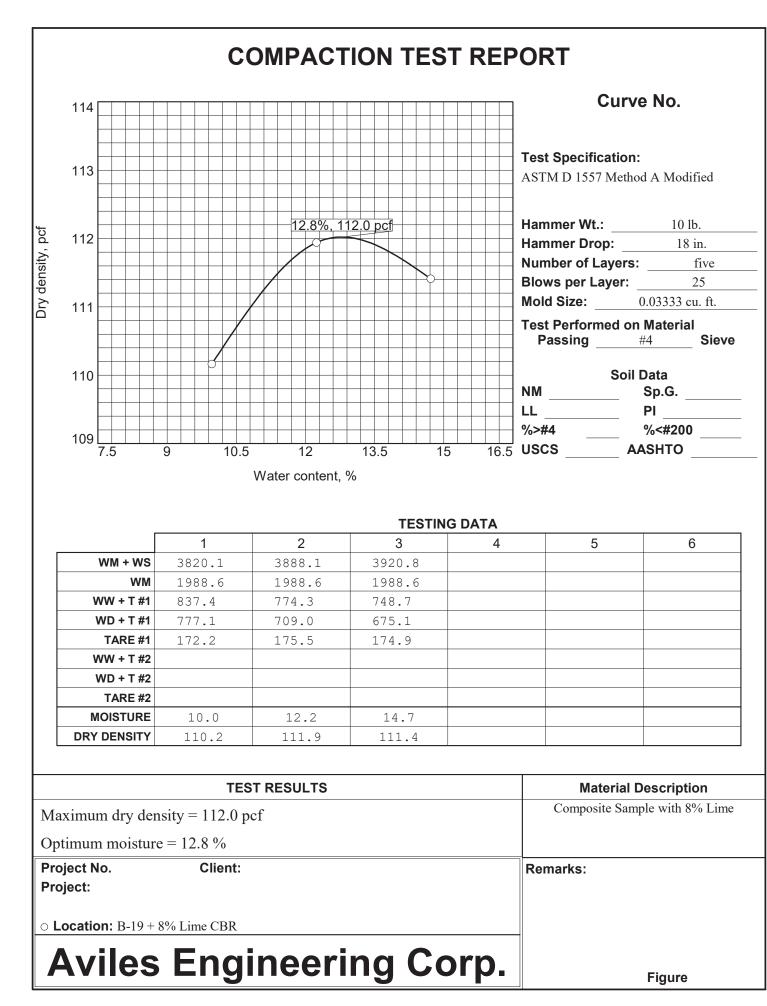
Lime Additions:

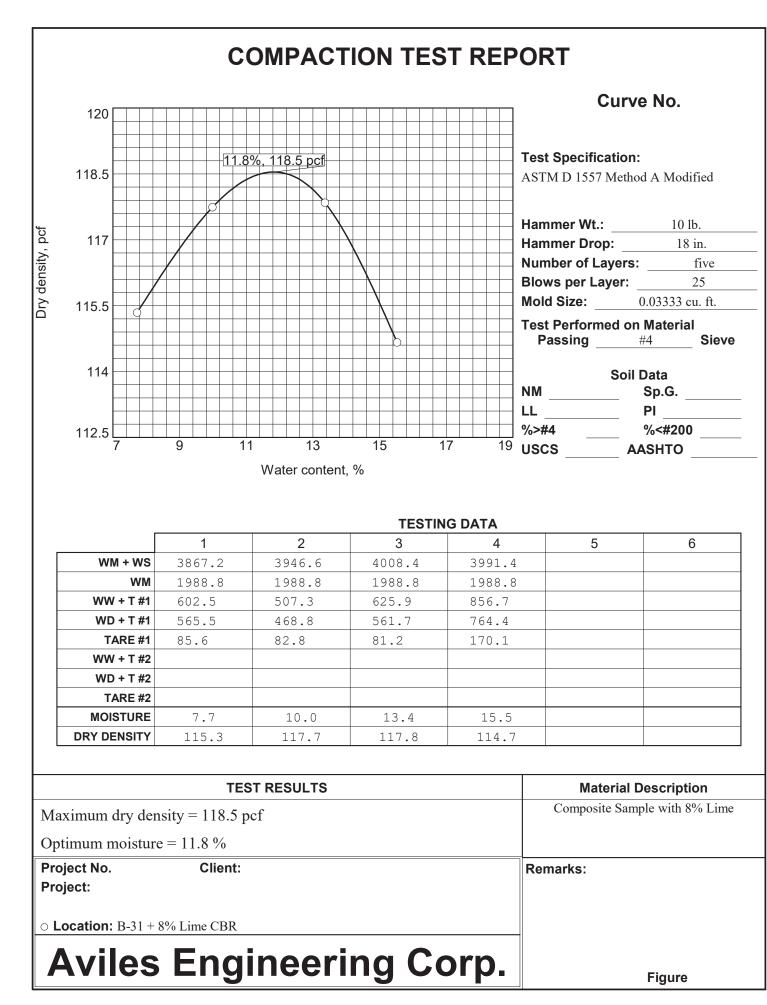


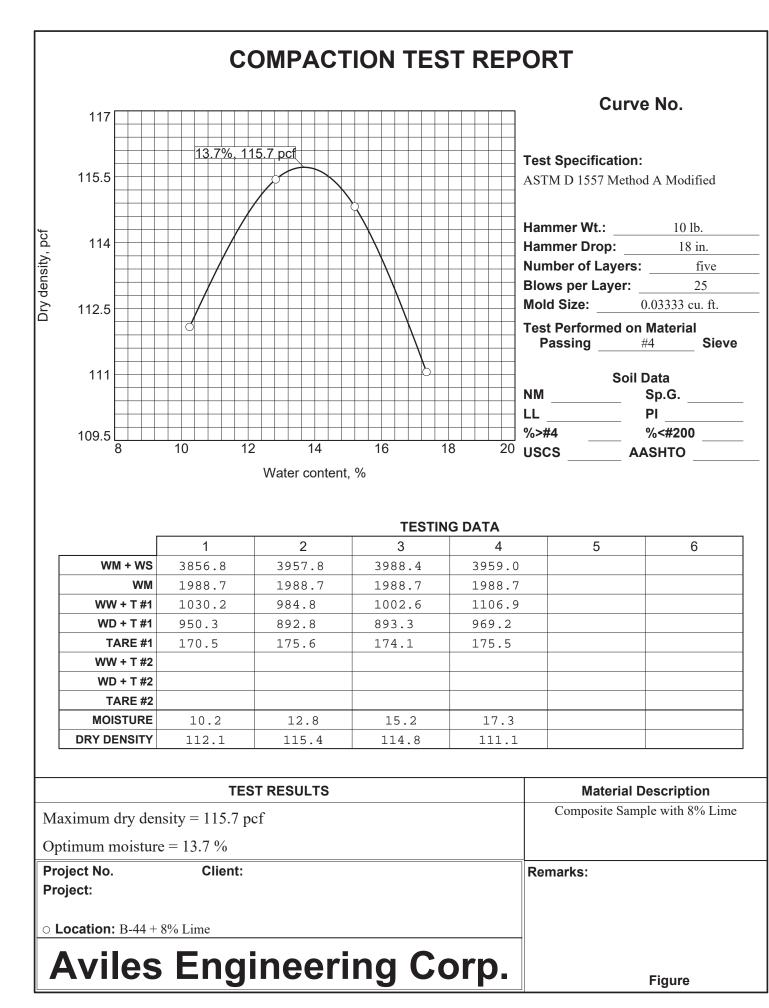
Optimum Stabilization (% Lime):

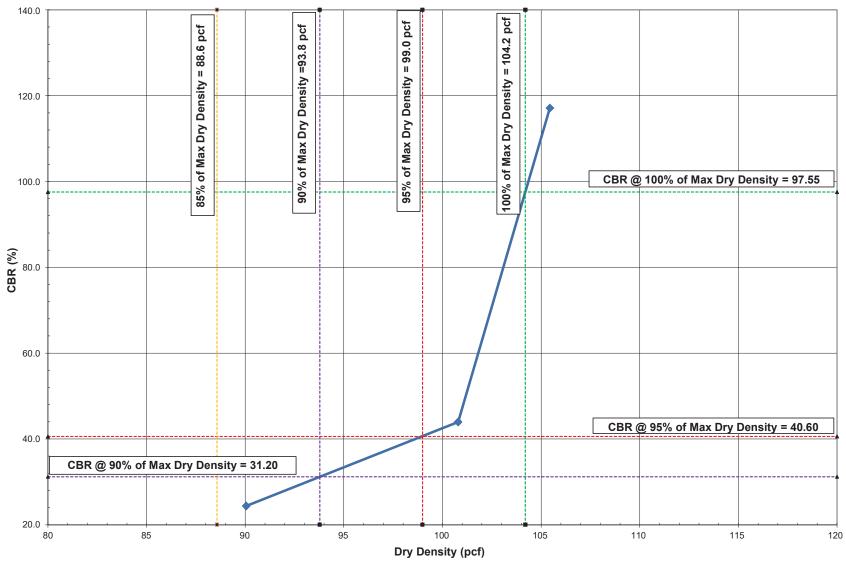
8



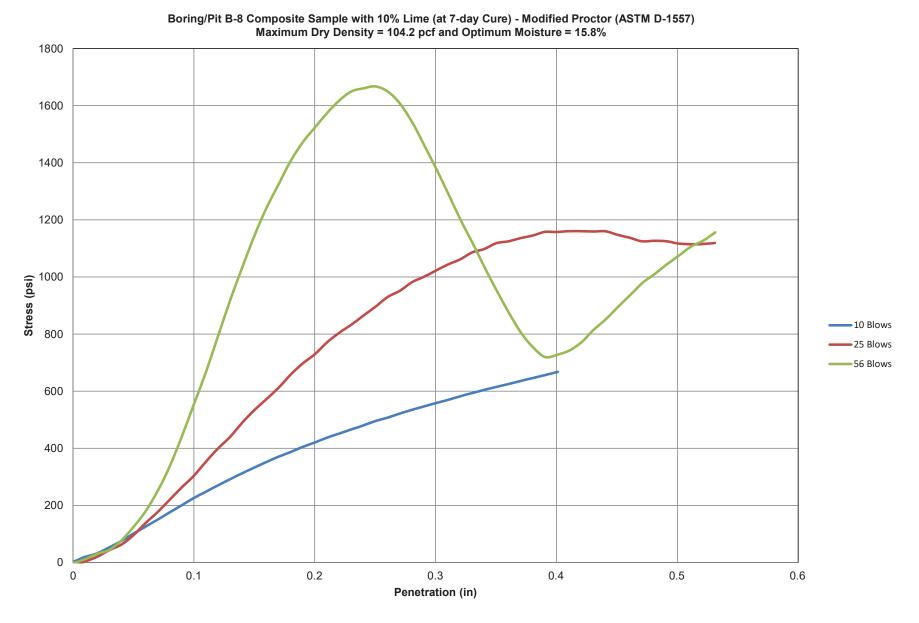


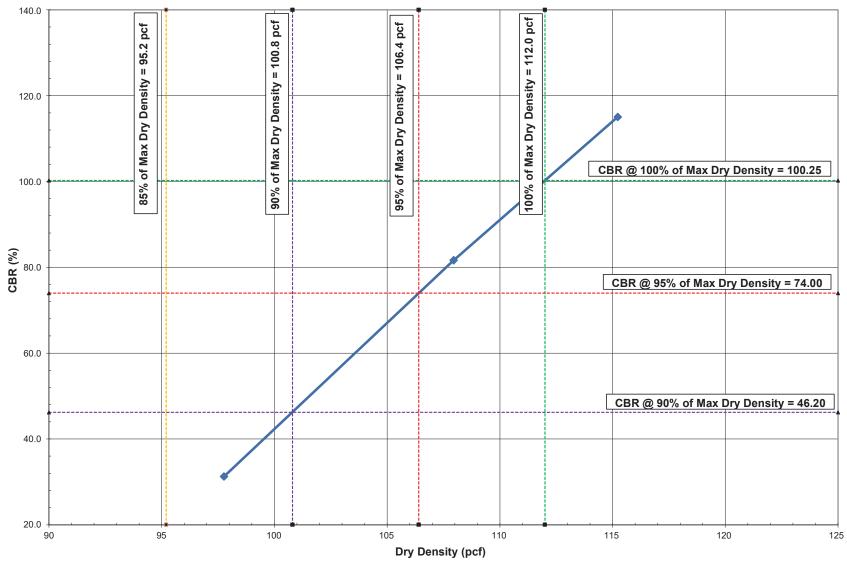




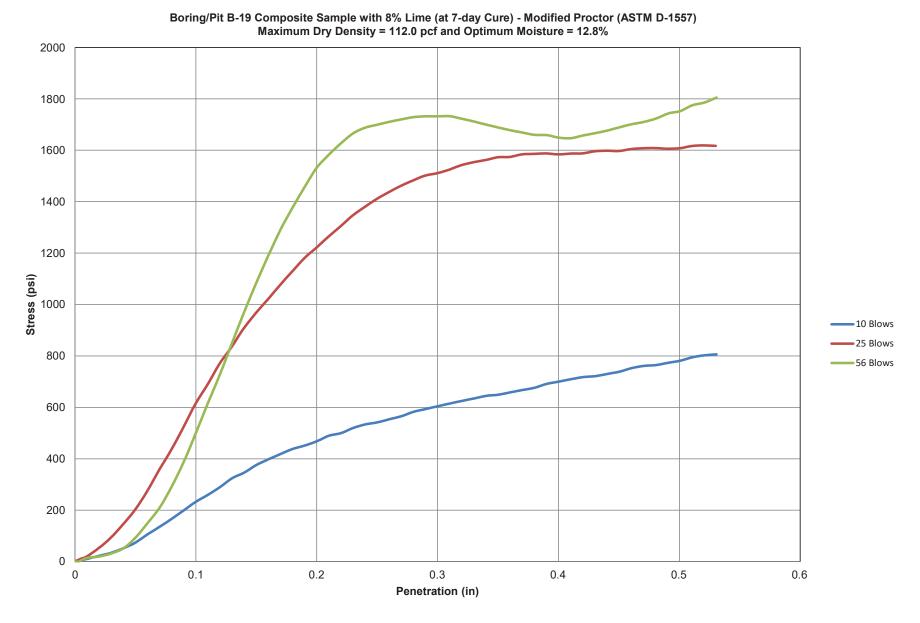


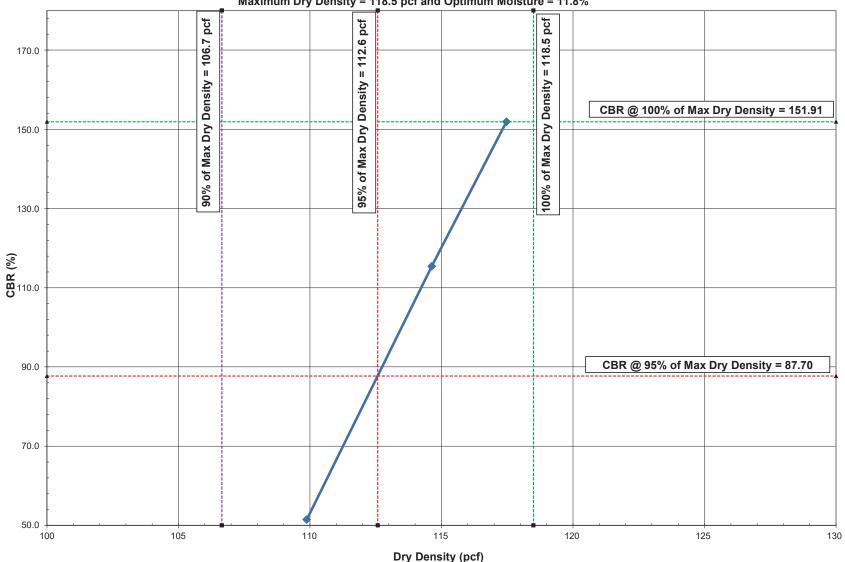
Boring/Pit B-8 Composite Sample with 10% Lime (at 7-day Cure) - Modified Proctor (ASTM D-1557) Maximum Dry Density = 104.2 pcf and Optimum Moisture = 15.8%



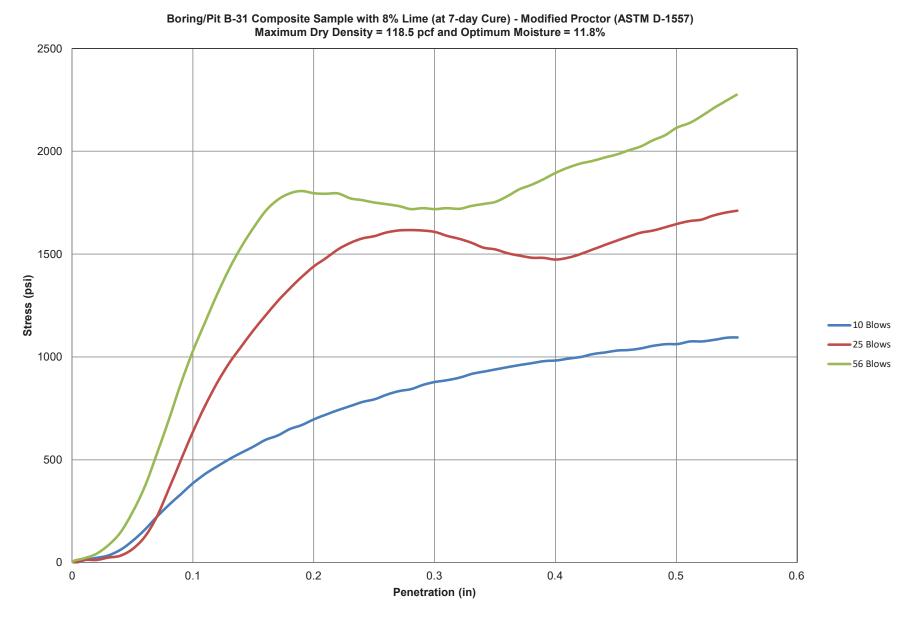


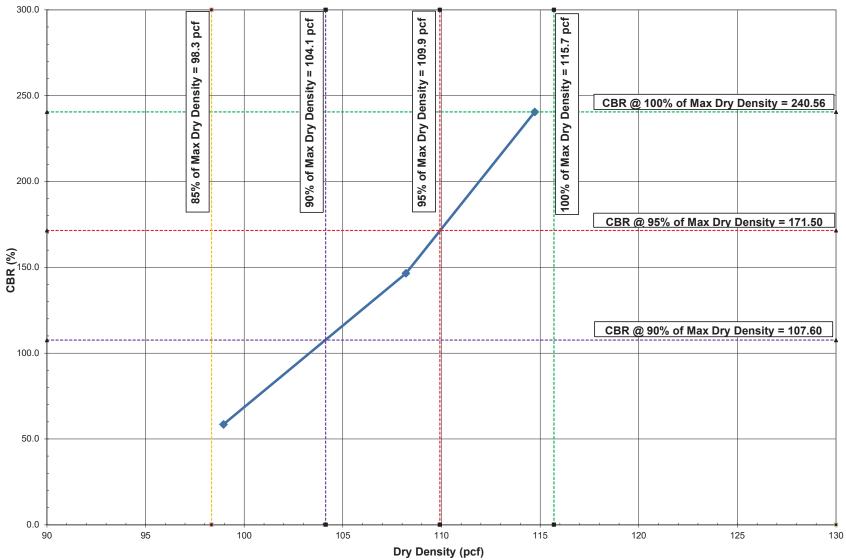
Boring/Pit B-19 Composite Sample with 8% Lime (at 7-day Cure) - Modified Proctor (ASTM D-1557) Maximum Dry Density = 112.0 pcf and Optimum Moisture = 12.8%



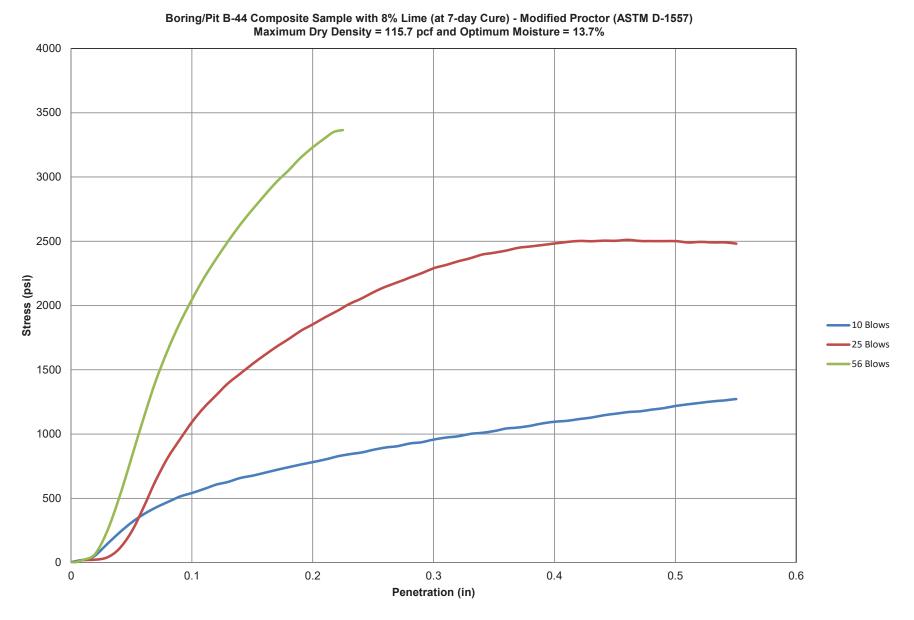


G103-21 HAS Taxiway L Geotechnical Investigation California Bearing Ratio (ASTM D-1883) Boring/Pit B-31 Composite Sample with 8% Lime (at 7-day Cure) - Modified Proctor (ASTM D-1557) Maximum Dry Density = 118.5 pcf and Optimum Moisture = 11.8%





Boring/Pit B-44 Composite Sample with 8% Lime (at 7-day Cure) - Modified Proctor (ASTM D-1557) Maximum Dry Density = 115.7 pcf and Optimum Moisture = 13.7%



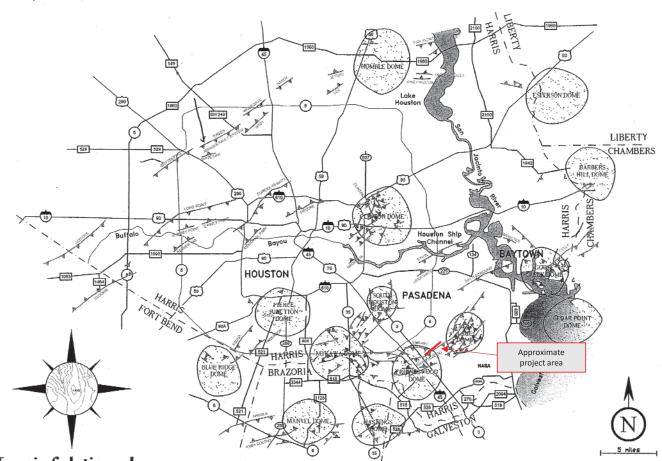


APPENDIX B

Plate B-1	"Principal Surface Faults of the Houston Central Metropolitan Area"
Plate B-2	"Active Faults in Southeastern Harris County, Texas"

G103-21 Ellington Field Taxiways L, E and D

Fault Study 12/19/2021

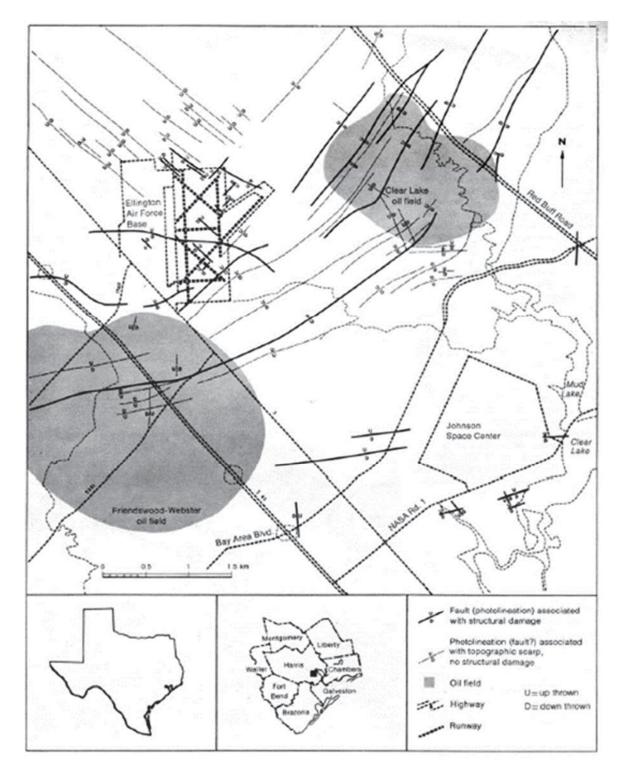


Terrain Solutions, Inc.

Principal Surface Faults of the Houston Central Metropolitan Area (After O'Neill & Van Siclen with additions by C. Norman)

PLATE B-1

Rev. 05/13/04



"Active Faults in Southeastern Harris County, Texas", Geo I, pages 151, by Clanton, U.S. and Amsbury, D.L.